



DRAFT

VOLUME II: APPENDICES

**RCRA FACILITY INVESTIGATION
FOR SOLID WASTE MANAGEMENT
UNITS 17, 31, 48, AND 54
AT RADFORD ARMY AMMUNITION
PLANT, VIRGINIA**

PREPARED FOR:

**U. S. ARMY
ENVIRONMENTAL CENTER**

Aberdeen Proving Ground, Maryland

PREPARED BY:

PARSONS ENGINEERING SCIENCE, INC.

**10521 Rosehaven Street
Fairfax, Virginia 22030**

JANUARY 1996

**RCRA FACILITY INVESTIGATION REPORT
VOLUME II
RADFORD ARMY AMMUNITION PLANT
RADFORD, VIRGINIA**

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APPENDIX A
ACRONYMS AND ABBREVIATIONS

LIST OF ACRONYMS AND ABBREVIATIONS

ACD	Air Curtain Destructor
ACL	Alternate Concentration Limit
ACO	Administrative Contracting Officer
ARARs	Applicable or Relevant and Appropriate Requirements
ASTM	American Society for Testing and Materials
atm-m ³ /mole	Atmosphere - cubic meter per mole
BCF	Bioconcentration Factor
BCM	Betz-Converse-Murdock, Inc.
bgs	Below Ground Surface
BTU	British Thermal Unit
CAA	Clean Air Act
CBC	Complete Blood Count
CL	Silty Clay
CIH	Certified Industrial Hygienist
CMS	Corrective Measures Study
COC	Chain of Custody
COD	Chemical Oxygen Demand
CRAVE	Carcinogenic Risk Assessment Verification Endeavor
CTM	Charles T. Main of Virginia, Inc.
CWA	Clean Water Act
dBA	Decibel
DCL	Data Chem Laboratories
DNT	Dinitrotoluene
E	Exposure Level
EM	Electromagnetic
EP	Extract Procedure
FAL	Fly Ash Landfill
FLFA	Former Lead Furnace Area
Fm.	Formation
FVC	Forced Vial Capacity
FWQC	Federal Water Quality Criteria
GCMS	Gas Chromatograph Mass Spectrometer
GM	Silty Gravel
GOCO	Government-owned, Contractor-operated
GW	Groundwater
HBN	Health-based Number
HEAST	Health Effects Assessment Summary Tables
HI	Hazard Index
HMX	High melting point explosive
HSP	Health and Safety Plan
HSWA	Hazardous and Solid Waste Amendments
ID	Identification Number
IR	Installation Restoration
IRDMIS	Installation Restoration Data Management Information System
IRFDS	Inhalation Reference Doses
ISF	Inhalation Slope Factor
IVR	Inhalation Unit Risks
KCl	Potassium Chloride
KoC	Organic Carbon (soils) Partition Coefficient
KoW	Octanol/water Partition Coefficient
LQAC	Laboratory QA Coordinator
MCL	Maximum Contaminant Level
MCLG	Maximum Contaminant Level Goals
MDL	Method Detection Limits
mg/kg	Milligrams Per Kilogram
mg/L	Milligrams Per Liter

LIST OF ACRONYMS AND ABBREVIATIONS

mgd	Million Gallons Per Day
ML	Sandy Silt
mm-Hg	Millimeters of Mercury
mph	Miles Per Hour
MSDS	Material Safety Data Sheet
msl	Mean Sea Level
MTBE	Methyl Tertiary Butyl Ether
MW	Monitoring Well
NBS	National Bureau of Standards
NC	Nitrocellulose
ND	Nondetect
NEIC	National Enforcement Investigation Center
NG	Nitroglycerin
NIST	National Institute of Standards and Technology
NROW	New River Ordnance Works
NRVPCD	New River Valley Planning District Commission
Parsons ES	Parsons Engineering Science, Inc.
PAHs	Polynuclear Aromatic Hydrocarbons
PC	Personal Computer
PEF	Particulate Emission Factor
PID	Photoionization Detector
PNA	Polynuclear Aromatic Hydrocarbons
PPE	Personal Protective Equipment
PQL	Practical Quantification Limit
psi	Pounds per Square Inch
PVC	Polyvinyl Chloride
QA	Quality Assurance
QAP	Quality Assurance Plan
QAPP	Quality Assurance Project Plan
QC	Quality Control
RAAP	Radford Army Ammunition Plant
RAGS	Risk Assessment Guidance for Superfund
RBC	Risk Based Concentration
RCRA	Resource Conservation and Recovery Act
RfC	Reference Concentration
RfD	Reference Dose
RFI	RCRA Facility Investigation
RL	Reporting Limit
RME	Reasonable Maximum Exposure
ROW	Radford Ordnance Works
RPD	Relative Percent Difference
RW	Drilling/Rinse Water
SB	Soil Boring
SCS	Soil Conservation Service
SE	Sediment
SES	Safety and Environmental Service
SF	Slope Factor
SM	Silty Sand
SO	Soil
SOP	Standard Operating Procedure
SS	Surface Soil
SVOC	Semivolatile Organic Compound
SW	Surface Water
SWMU	Solid Waste Management Unit
TAL	Target Analyte List

LIST OF ACRONYMS AND ABBREVIATIONS

TBC	To Be Considered
TBD	To Be Determined
TCE	Trichloroethene
TCLP	Toxic Characteristic Leaching Procedure
TEFs	Toxicity Equivalency Factors
TIC	Tentatively Identified Compound
TNT	Trinitrotoluene
TOC	Top of Well Casing or Total Organic Carbon
TOX	Total Organic Halogens
TPH	Total Petroleum Hydrocarbon
μg/g	Micrograms Per Gram
μg/L	Micrograms Per Liter
USAEC	U.S. Army Environmental Center
USAEHA	U.S. Army Environmental Hygiene Agency
USATHAMA	U.S. Army Toxic and Hazardous Materials Agency
USCS	Unified Soil Classification System
USDOT	U.S. Department of Transportation
USEPA	U.S. Environmental Protection Agency
UST	Underground Storage Tank
VDMR	Virginia Division of Mineral Resources
VI	Verification Investigation
VOC	Volatile Organic Compound
VPI&SU	Virginia Polytechnic Institute and State University
WQC	Water Quality Criteria

APPENDIX B

GROUNDWATER USAGE - WELL INVENTORY

**PROPERTY OWNERS WITHIN 1 MILE OF RAAP
WITH PRIVATE WATER WELL SUPPLIES**

LONGSHOP-McCOY AREA RESIDENTS

Michael Graham*
Route 3, Box 1304-A
Blacksburg, VA 24060

Steve Graham*
4513 Mount Zion Road
Blacksburg, VA 24060

Richard Hinkson*
2065 Aviation Yacht Club Road
Mechanicsville, MD 20659
(residence at 4918 McCoy Road)

Mode A. Johnson
609 N. Main Street, #1
Blacksburg, VA 24060

Ronnie and Ella Roop*
1500 Staples Street
Radford, VA 24141
(owners of Prices Fork property)

Charles R. Sheppard
Route 2, Box 341
Blacksburg, VA 24060

Douglas H. Frey
Route 3, Box 488
Blacksburg, VA 24060

Edward A. Mullins
Route 2, Box 329
Blacksburg, VA 24060

David S. Rowe
3198 Mathews Lane
Blacksburg, VA 24060

Charles E. Snow*
Route 2, Box 551
Blacksburg, VA 24060

Vivian Vyule
4760 Prices Fork Road
Blacksburg, VA 24060

Freddie L. Oliver
3611 McCoy Road
Blacksburg, VA 24060

Carmon M. Smith
3928 McCoy Road
Blacksburg, VA 24060

Ira Long
3870 Prices Fork Road
Blacksburg, VA 24060

James V. Noonkester
Route 2, Box 450
Blacksburg, VA 24060

* GW-2 Waterwell Completion reports available.

**PROPERTY OWNERS WITHIN 1 MILE OF RAAP
WITH PRIVATE WATER WELL SUPPLIES (Continued)**

RIVER BLUFFS SUBDIVISION RESIDENTS

Kenneth R. Church P.O. Box 3279 Radford, VA 24143	Section III, Lot 6
J.R. and Judy Willoughly Route 2, Box 366 Radford, VA 24143	Section II, Lot 40
Clanston Tickle Route 2, Box 261 Radford, VA 24143	Section II, Lot 45
Cheryl Austin Route 2 Radford, VA 24143	Section III, Lot 17 (extended)
Philip Mabe Route 2 Radford, VA 24143	Section II, Lot 51A
Gary Hughes Route 2 Radford, VA 24143	Section II, Lot 43
D.L. Dalton Route 2, Box 356 Radford, VA 24143	Section II, Lot 55
Terry St. Clair Route 2 Radford, VA 24143	Section II, Lots 21, 22
David Wright Route 2 Radford, VA 24143	Section II, Lot 42
Jo Ann Bingham Route 2 Radford, VA 24143	Section I, Lot 1

**PROPERTY OWNERS WITHIN 1 MILE OF RAAP
WITH PRIVATE WATER WELL SUPPLIES (Continued)**

RIVER BLUFFS SUBDIVISION RESIDENTS

Perry and Norma Boone Route 2 Radford, VA 24143	Section II, Lot 54
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Roger D. King Route 2 Radford, VA 24143	Section II, Lot 56
---	--------------------

Allen Wiley Route 2 Radford, VA 24143	Section II, Lot 32
---	--------------------

Curtis Lawson Route 2 Radford, VA 24143	Section I, Lot 7
---	------------------

Ronnie Dalton Route 2 Radford, VA 24143	Section II, Lot 16
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Jessee White Route 2 Radford, VA 24143	Section II, Lot 5
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Benton Miller Route 2 Radford, VA 24143	Section II, Lot 8 (extended)
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Lloyd Loftas Route 2 Radford, VA 24143	Section II, Lot 10
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**PROPERTY OWNERS WITHIN 1 MILE OF RAAP
WITH PRIVATE WATER WELL SUPPLIES (Continued)**

GATE TEN ROAD RESIDENTS

Robert Pannell
Route 2
Radford, VA 24143

Ms. Thaddus Lee
Route 2
Radford, VA 24143

Bob Hosp
Route 2
Radford, VA 24143

**PUBLIC WATER SUPPLY WELLS
IN THE VICINITY OF RAAP**

PULASKI COUNTY

Location	Description	Number of Public Wells
Eagleview Trailer Park	1 1/2 miles SW of RAAP; along Route 600	2
Trigg Trailer Park	2 1/2 miles SW of RAAP; near town of New River	2
River Bend Subdivision	1/2 mile SW of RAAP; west of Pepper, VA, along Route 114	1
Sunset Terrace Apartment Complex	3/4 mile SW of RAAP; west of Pepper, VA, along Route 114	1
River Bend Trailer Park	1 mile SW of RAAP; west of Pepper, VA, along Route 114	2
Polyester Trailer Park	2 miles south of RAAP; in meander loop of New River	2

**PUBLIC WATER SUPPLY WELLS
IN THE VICINITY OF RAAP (Continued)**

MONTGOMERY COUNTY

Location	Description	Number of Public Wells
Phillips Acres Subdivision	2 1/2 miles east of RAAP; 1 mile east of Prices Fork	1
Prices Fork Area	1 1/2 miles east of RAAP; 1/2 mile south of Prices Fork	2
Vicker Heights Subdivision	3 miles east of RAAP; 1/4 mile south of Route 114	1

APPENDIX C
LITHOLOGIC LOGS/WELL CONSTRUCTION RECORDS

CONTRACTOR: CT & E GEOLOGIST: BACHOVCHIN/GLENNIE DRILLING METHOD: HSA DTW FROM TOC: NA DATE/TIME: NA	PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO.: 17ASB1 LOCATION: SWMU 17A WEATHER: COLD, 30° F DATE/TIME START: 12/12/94 1800 DATE/TIME FINISH: 12/12/94 1800
	PROJECT NAME: RAAP CLIENT: US AEC PROJECT NO.: 722843	

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
1								SAND AND SILT (FILL), BLACK, DRY		SURFACE ELEVATION 1872.4' (MSL)	1
2											2
3											3
4											4
5											5
6	1A*	30	5/6 7/10	0.0	SS	SS 5'-7'	SM				6
7											7
8											8
9	2*	50	6/4 3/2	0.0	SS	SS 8'-10'					9
10											10
11											11
12											12
13								SILT, SOME CLAY, LITTLE SAND, YELLOW-BROWN, QUARTZ PEBBLES, GRAVEL, WET AT 15 FEET		13	
14	3*	80	7/10 15/17	0.0	SS	SS 13'-15'	ML			14	
15										15	
16										16	
17								CLAY, SOME SILT, YELLOW-BROWN, GRAVEL		17	
18										18	
19	4*	65	15/19 14/13	0.0	SS	SS 18'-20'	CL			19	
20								GRADING INTO TAN DOLOMITE AT 21.5 FEET (REFUSAL)		20	
21	5*	50	15/15 REF.	0.0	SS	SS 21'-22'				21	
22								END OF BORING AT 22 FEET			22
23											23
24											24
25											25
26											26

HSA = HOLLOW STEM AUGER CAL = CALIBRATION USCS = UNIFIED SOIL CLASS. SYS.	SS = SPLIT SPOON A = AUGER CUTTINGS * = LAB SAMPLE	BH = BORE HOLE GS = GRAB SAMPLE ♁ = WATER LEVEL
COMMENTS: 4 INCH DIAMETER BORING GROUTED TO SURFACE		

CONTRACTOR: CT & E	PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO.: 17ASB2
GEOLOGIST: BACHOVCHIN/GLENNIE		LOCATION: SWMU 17A
DRILLING METHOD: HSA		WEATHER: COLD, 20° F
DTW FROM TOC: NA		DATE/TIME START: 12/13/94 0840
DATE/TIME: NA	PROJECT NAME: RAAP	DATE/TIME FINISH: 12/13/94 1000
	CLIENT: US AEC	
	PROJECT NO.: 722843	

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
1								SILT, SOME CLAY, TRACE SAND, YELLOW-BROWN		SURFACE ELEVATION 1874.4' (MSL)	1
2											2
3											3
4	1*	75	6/16 18/30	0.0	SS	SS 3'-5'					4
5											5
6											6
7											7
8											8
9	2*	85	10/16 20/25	0.7	SS	SS 8'-10'	ML				9
10				0.3	BH						10
11											11
12											12
13											13
14	3*	90	13/15 7/4	0.0	SS	SS 13'-15'					14
15				1.4	HS			CLAY, SOME SILT, LIGHT BROWN, DAMP			15
16											16
17											17
18											18
19											19
20											20
21	4A*	50	4/6 7/8	1.2	HS	SS 20'-22'	CL				21
22											22
23											23
24	5*	90	3/6 12/18	1.3	HS	SS 23'-25'	DLMT	DOLOMITE, TAN, REFUSAL			24
25								END OF BORING AT 25 FEET			25
26											26

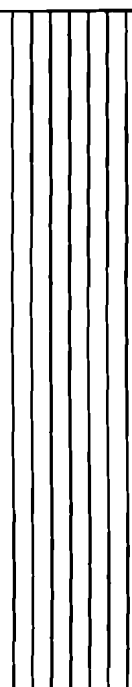
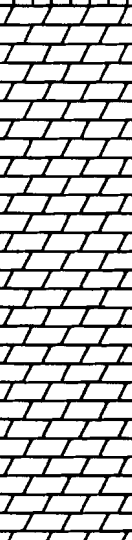
HSA = HOLLOW STEM AUGER
 CAL = CALIBRATION
 USCS = UNIFIED SOIL CLASS. SYS.

SS = SPLIT SPOON
 A = AUGER CUTTINGS
 * = LAB SAMPLE

BH = BORE HOLE
 GS = GRAB SAMPLE
 ▽ = WATER LEVEL

COMMENTS:
 4 INCH DIAMETER BORING
 GROUTED TO SURFACE

CONTRACTOR: CT & E GEOLOGIST: BACHOVCHIN/GLENNIE DRILLING METHOD: HSA DTW FROM TOC: NA DATE/TIME: NA	PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO: 17ASB3 LOCATION: SWMU 17A WEATHER: COLD, 20° F DATE/TIME START: 12/13/94 1030 DATE/TIME FINISH: 12/13/94 1130
	PROJECT NAME: RAAP CLIENT: US AEC PROJECT NO.: 722843	

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
1								SILT AND CLAY, DARK YELLOW-BROWN		↑ SURFACE ELEVATION 1873.9' (MSL) ↓	1
2											2
3											3
4	1*	80	4/3 4/12	2.0	SS	SS 3'-5'					4
5											5
6											6
7											7
8											8
9	2*	90	5/6 5/5	0.0	HS	SS 8'-10'	ML				9
10											10
11											11
12											12
13											13
14	3*	85	24/16 6/50	0.0	HS	SS 13'-15'		DAMP CLAY AT 13 FEET		14	
15								15			
16								16			
17								17			
18								18			
19	4*	25	80/ 6"	0.0	HS	SS 18'-20'	DLMT	19			
20								20			
21								21			
22								22			
23								23			
24	5*	25	100/ 6"	0.0	HS	SS 23'-25'		24			
25								25			
26								END OF BORING AT 25 FEET		26	

HSA = HOLLOW STEM AUGER CAL = CALIBRATION USCS = UNIFIED SOIL CLASS. SYS.	SS = SPLIT SPOON BH = BORE HOLE HS = HEADSPACE A = AUGER CUTTINGS GS = GRAB SAMPLE * = LAB SAMPLE	⚡ = WATER LEVEL COMMENTS: 4 INCH DIAMETER BORING GROUTED TO SURFACE
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CONTRACTOR: CT & E		PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO: 17CSB1
GEOLOGIST: BACHOVCHIN/GLENNIE			LOCATION: SWMU 17C
DRILLING METHOD: HSA			WEATHER: COLD, 20° F
DTW FROM TOC: NA			DATE/TIME START: 12/13/94 1250
DATE/TIME: NA		PROJECT NAME: RAAP	DATE/TIME FINISH: 12/13/94 1330
		CLIENT: US AEC	
		PROJECT NO.: 722843	

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
1							GM	GRAVEL AND SILT (FILL)			1
2								SILT AND CLAY, ORANGE-BROWN, SOME FILL			2
3											3
4	1*	85	6/16 25/36	0.0	HS	SS 3'-5'	ML				4
5											5
6											6
7											7
8											8
9	2*	65	6/6 6/6	0.0	HS	SS 8'-10'	CL	CLAY AND SILT, DARK YELLOW-BROWN			9
10											10
11											11
12	3*	40	100/6	0.0	HS	SS 13'-13'	DLMT	DOLOMITE, GRAY, WEATHERED			12
13								END OF BORING AT 12.7 FEET			13
14											14
15											15
16											16
17											17
18											18
19											19
20											20
21											21
22											22
23											23
24											24
25											25
26											26

HSA = HOLLOW STEM AUGER CAL = CALIBRATION USCS = UNIFIED SOIL CLASS. SYS.	SS = SPLIT SPOON A = AUGER CUTTINGS * = LAB SAMPLE	BH = BORE HOLE GS = GRAB SAMPLE ♀ = WATER LEVEL	COMMENTS: 4 INCH DIAMETER BORING GROUTED TO SURFACE
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CONTRACTOR: CT & E		PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO: 17CSB2
GEOLOGIST: BACHOVCHIN/GLENNIE			LOCATION: SWMU 17C
DRILLING METHOD: HSA			WEATHER: COLD, 20° F
DTW FROM TOC: NA			DATE/TIME START: 12/13/94 1340
DATE/TIME: NA		PROJECT NAME: RAAP	DATE/TIME FINISH: 12/13/94 1415
		CLIENT: US AEC	
		PROJECT NO.: 722843	

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
1							GM	GRAVEL (FILL)			1
2								SILT AND CLAY, YELLOW-BROWN			2
3											3
4	1*	65	6/17 19/20	0.4	HS	SS 3'-5'					4
5											5
6							ML				6
7											7
8											8
9	2*	80	3/5 10/19	0.0	HS	SS 8'-10'					9
10											10
11								DOLOMITE, GRAY, WEATHERED			11
12							DLMT				12
13	3*	15	100/4	0.0	SS	SS 13'-14'					13
14								END OF BORING AT 13.5 FEET			14
15											15
16											16
17											17
18											18
19											19
20											20
21											21
22											22
23											23
24											24
25											25
26											26

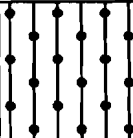
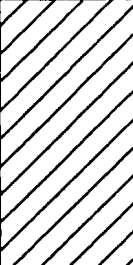
HSA = HOLLOW STEM AUGER
CAL = CALIBRATION
USCS = UNIFIED SOIL CLASS. SYS.

SS = SPLIT SPOON
A = AUGER CUTTINGS
* = LAB SAMPLE

BH = BORE HOLE
GS = GRAB SAMPLE
W = WATER LEVEL

COMMENTS:
4 INCH DIAMETER BORING
GROUTED TO SURFACE

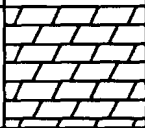
CONTRACTOR: <u>CT & E</u> GEOLOGIST: <u>BACHOVCHIN/GLENNIE</u> DRILLING METHOD: <u>HSA</u> DTW FROM TOC: <u>NA</u> DATE/TIME: <u>NA</u>			PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD			BORING NO: <u>17DSB1</u> LOCATION: <u>SWMU 17D</u> WEATHER: <u>COLD, 25° F</u> DATE/TIME START: <u>12/13/94 1555</u> DATE/TIME FINISH: <u>12/13/94 1720</u>		
			PROJECT NAME: <u>RAAP</u>					
			CLIENT: <u>US AEC</u>					
			PROJECT NO.: <u>722843</u>					

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
1								GRAVEL, SOME SILT (FILL)		SURFACE ELEVATION 1866.3' (MSL)	1
2							GM				2
3											3
4	1*	100	4,6 8,11	0.7	HS	SS 3'-5'		CLAY AND SILT, GRAY (FILL), THEN FILL ENDING AT APPROXIMATELY 8 FEET			4
5											5
6											6
7											7
8											8
9	2*	100	10,11 12,16	2.6	SS	SS 8'-10'					9
10											10
11											11
12							CL				12
13											13
14	3*	100	9,9 10,16	5.0	SS	SS 13'-15'					14
15											15
16											16
17											17
18											18
19	4*	100	5,5 9,8	2.2	SS	SS 18'-20'					19
20											20
21											21
22											22
23											23
24	5*	100	3,3 6,8	1.1	SS	SS 23'-25'					24
25											25
26	6*	100	2,3	2.2	HS	SS	DLMT	DOLOMITE, GRAY, ARGILLACEOUS, WEATHERED, INTERLAYERED YELLOW CLAY		26	

HSA = HOLLOW STEM AUGER CAL = CALIBRATION USCS = UNIFIED SOIL CLASS. SYS.	SS = SPLIT SPOON A = AUGER CUTTINGS * = LAB SAMPLE	BH = BORE HOLE GS = GRAB SAMPLE ¶ = WATER LEVEL
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COMMENTS: 4 INCH DIAMETER BORING GROUTED TO SURFACE
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CONTRACTOR: <u>CT & E</u>	PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO: <u>17DSB1</u>
GEOLOGIST: <u>BACHOVCHIN/GLENNIE</u>		LOCATION: <u>SMMU 17D</u>
DRILLING METHOD: <u>HSA</u>		WEATHER: <u>COLD, 25° F</u>
DTW FROM TOC: <u>NA</u>		DATE/TIME START: <u>12/13/94 1555</u>
DATE/TIME: <u>NA</u>	PROJECT NAME: <u>RAAP</u>	DATE/TIME FINISH: <u>12/13/94 1720</u>
	CLIENT: <u>US AEC</u>	
	PROJECT NO.: <u>722843</u>	

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
27			3,4			25'-27'					27
28								END OF BORING AT 28.5 FEET			28
29											29
30											30
31											31
32											32
33											33
34											34
35											35
36											36
37											37
38											38
39											39
40											40
41											41
42											42
43											43
44											44
45											45
46											46
47											47
48											48
49											49
50											50
51											51
52											52

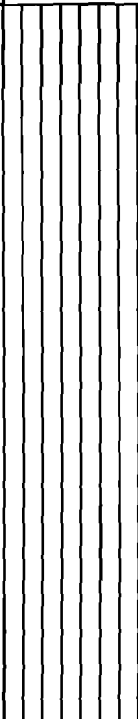
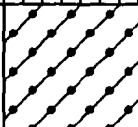
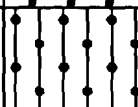
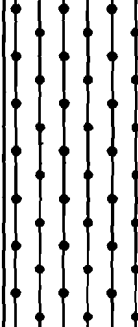
HSA = HOLLOW STEM AUGER CAL = CALIBRATION USCS = UNIFIED SOIL CLASS. SYS.	SS = SPLIT SPOON A = AUGER CUTTINGS * = LAB SAMPLE	BH = BORE HOLE GS = GRAB SAMPLE W = WATER LEVEL	COMMENTS: 4 INCH DIAMETER BORING GROUTED TO SURFACE
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CONTRACTOR: CT & E		PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO: 17DSB2
GEOLOGIST: BACHOVCHIN/GLENNIE			LOCATION: SWMU 17D
DRILLING METHOD: HSA			WEATHER: COLD, 25° F
DTW FROM TOC: NA			DATE/TIME START: 12/13/94 1430
DATE/TIME: NA		PROJECT NAME: RAAP	DATE/TIME FINISH: 12/13/94 1530
		CLIENT: US AEC	
		PROJECT NO.: 722843	

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	P10 (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
1								GRAVEL, (FILL)		SURFACE ELEVATION 1867.3' (MSL)	1
2							GM				2
3											3
4	1*	90	6,11 11,10	0.8	SS	SS 3'-5'		SILT, SOME CLAY, GRAY, DARK YELLOW, MOIST			4
5											5
6											6
7							ML				7
8											8
9	2*	90	4,14 17,23	2.0	SS	SS 8'-10'					9
10											10
11											11
12											12
13											13
14	3*	90	3,4 4,5	0.9	HS	SS 13'-15'		CLAY AND SILT, ORANGE-BROWN, MOIST			14
15											15
16							CL				16
17											17
18											18
19	4*	100	2,3 9,16	0.0	HS	SS 18'-20'					19
20											20
21											21
22							DLMT	DOLOMITE, TAN, ARGILLACEOUS, WEATHERED			22
23											23
24	5*	80	3,8 8,38	0.0	HS	SS 23'-25'					24
25											25
26								END OF BORING AT 25.5 FEET			26

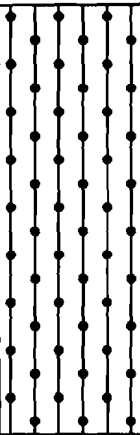
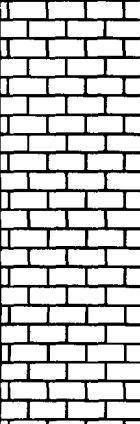
HSA = HOLLOW STEM AUGER CAL = CALIBRATION USCS = UNIFIED SOIL CLASS. SYS.	SS = SPLIT SPOON A = AUGER CUTTINGS * = LAB SAMPLE	BH = BORE HOLE GS = GRAB SAMPLE ▽ = WATER LEVEL	HS = HEADSPACE COMMENTS: 4 INCH DIAMETER BORING GROUTED TO SURFACE
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CONTRACTOR: <u>CT & E</u>	PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO: <u>31MW1</u>
GEOLOGIST: <u>BACHOVCHIN/GLENNIE</u>		LOCATION: <u>SWMU 31</u> <u>UPGRADIENT OF LAGOONS</u>
DRILLING METHOD: <u>HSA</u>		WEATHER: <u>COLD, 35° F</u>
DTW FROM TOC: <u>42 FT (FROM SURFACE)</u>		DATE/TIME START: <u>12/15/94 1500</u>
DATE/TIME: <u>12/16/94 1600</u>		DATE/TIME FINISH: <u>12/16/94 1630</u>
	PROJECT NAME: <u>RAAP</u>	
	CLIENT: <u>US AEC</u>	
	PROJECT NO.: <u>722843</u>	

DEPTH (FT)	S, MPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
1								SILT AND CLAY, DARK BROWN		TOC 1715.04' 1.6' STICK UP	1
2											2
3											3
4											4
5											5
6	1	50	5.5	0.0	HS	SS	ML				6
7			5.5			5'-7'					7
8											8
9											9
10											10
11								11			
12								12			
13								13			
14								14			
15								15			
16								16			
17								SAND, SOME SILT, PINK-ORANGE, GRAVEL		GROUT TO SURFACE	17
18	2	50	7, 100/5	7.9	SS	SS	SM				18
19	3	25	100/6	4.3	SS	SS		AUGER REFUSAL DUE TO GRAVEL, SWITCHED TO AIR ROTARY DRILLING AT 20 FEET			19
20						19'-20'					20
21								SAND AND GRAVEL, SOME SILT, LIGHT GRAY CUTTINGS			21
22											22
23											23
24											24
25											25
26	*						GM/SM				26
27										27	
28										28	
29										29	
30										30	

HSA = HOLLOW STEM AUGER CAL = CALIBRATION USCS = UNIFIED SOIL CLASS. SYS.	SS = SPLIT SPOON A = AUGER CUTTINGS * = LAB SAMPLE	BH = BORE HOLE GS = GRAB SAMPLE ▽ = WATER LEVEL	COMMENTS: 4 INCH ID PVC, SCH 40 0.01 INCH SLOT SCREEN
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CONTRACTOR: CT & E	PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO: 31MW1
GEOLOGIST: BACHOVCHIN/GLENNIE		LOCATION: SWMU 31 UPGRADIENT OF LAGOONS
DRILLING METHOD: HSA		WEATHER: COLD, 35° F
DTW FROM TOC: 42 FT (FROM SURFACE)	PROJECT NAME: RAAP	DATE/TIME START: 12/15/94 1500
DATE/TIME: 12/16/94 1600	CLIENT: US AEC	DATE/TIME FINISH: 12/16/94 1630
	PROJECT NO.: 722843	

DEPTH (FT)	SAMPLE ID	RECOVERY %	BL'W COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
31								SAND, BECOMING WEATHERED, CUTTINGS CHANGE COLOR TO GREEN-BROWN AT 35 FEET		GROUT TO SURFACE ↓ BENTONITE SEAL ↓ TOP OF SAND PACK AT 38', SCREEN FROM 40' TO 50' ↓	31
32											32
33											33
34											34
35											35
36	*					GM/SM					36
37											37
38								LIMESTONE, GRAY, WEATHERED WET AT 45 FEET DRILLING RATE (1 FOOT/2 MINUTES)		TOP OF SAND PACK AT 38', SCREEN FROM 40' TO 50' ↓	38
39											39
40											40
41											41
42											42
43											43
44											44
45						LMSN					45
46											46
47											47
48											48
49											49
50								END OF BORING AT 50 FEET			50
51											51
52											52
53											53
54											54
55											55
56											56
57											57
58											58
59											59
60											60

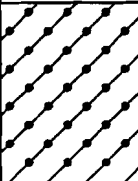
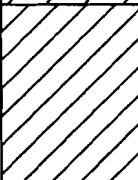
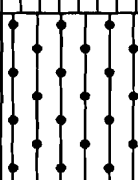
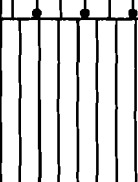
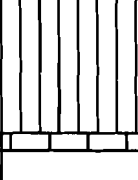
HSA = HOLLOW STEM AUGER
 CAL = CALIBRATION
 USCS = UNIFIED SOIL CLASS. SYS.

SS = SPLIT SPOON
 A = AUGER CUTTINGS
 * = LAB SAMPLE

BH = BORE HOLE
 GS = GRAB SAMPLE
 HS = HEADSPACE
 ♁ = WATER LEVEL

COMMENTS:
 4 INCH ID PVC, SCH 40
 0.01 INCH SLOT SCREEN

CONTRACTOR: <u>CT & E</u> GEOLOGIST: <u>BACHOVCHIN/GLENNIE</u> DRILLING METHOD: <u>HSA</u> DTW FROM TOC: <u>25 FT</u> DATE/TIME: <u>12/14/94 1530</u>	PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO: <u>31MW2</u> LOCATION: <u>SWMU 31 NEAR EAST LAGOON</u> WEATHER: <u>SHOWERS, 35° F</u> DATE/TIME START: <u>12/14/94 0920</u> DATE/TIME FINISH: <u>12/14/94 1100</u>
	PROJECT NAME: <u>RAAP</u> CLIENT: <u>US AEC</u> PROJECT NO.: <u>722843</u>	

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PTD (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
1								SAND AND SILT, DARK BROWN		TOC 1699.05' 1.5' STICK UP ↑ GROUT TO SURFACE ↓ BENTONITE SEAL ↓ TOP OF SAND PACK AT 16.5', SCREEN FROM 18.5' TO 28.5' ↓	1
2							SM				2
3											3
4											4
5											5
6	1	70	3,3 6,7	1.9	HS	SS 5'-7'	CL	CLAY, SOME SILT, BROWN			6
7										7	
8										8	
9										9	
10										10	
11	2*	90	5,7 6,9	4.4	HS	SS 10'-12'	ML	SILT, SOME SAND, LITTLE CLAY, BROWN-GRAY			11
12										12	
13										13	
14										14	
15										15	
16	3	25	12,11 10,9	2.8	HS	SS 15'-17'	GM/SM	SAND AND SILT, DARK BROWN, LIMESTONE PEBBLES			16
17										17	
18										18	
19										19	
20										20	
21	4*	10	6,4 4,2	2.8	HS	SS 20'-22'		SILT, SOME CLAY, DARK BROWN-GRAY			21
22										22	
23										23	
24							ML			24	
25								WET AT 25 FEET		25	
26	5	10	6,13 11,10	5.0	HS	SS 25'-27'					26
27										27	
28										28	
29							LM/SN	LIMESTONE, GRAY, WEATHERED			29
30								END OF BORING AT 28.5 FEET			30
31											31
32											32
33											33
34											34
35											35

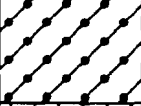
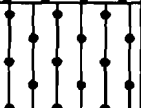
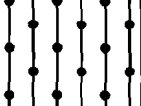
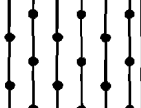
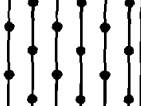
HSA = HOLLOW STEM AUGER
 CAL = CALIBRATION
 USCS = UNIFIED SOIL CLASS. SYS.

SS = SPLIT SPOON
 A = AUGER CUTTINGS
 * = LAB SAMPLE

BH = BORE HOLE
 GS = GRAB SAMPLE
 HS = HEADSPACE
 W = WATER LEVEL

COMMENTS:
 4 INCH ID PVC, SCH 40
 0.01 INCH SLOT SCREEN

CONTRACTOR: CT & E	PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO: 31MW3
GEOLOGIST: BACHOVCHIN/GLENNIE		LOCATION: SWMU 31 MIDDLE LAGOON
DRILLING METHOD: HSA		WEATHER: SHOWERS, 35° F
DTW FROM TOC: 23.18 FT		DATE/TIME START: 12/14/94 1330
DATE/TIME: 12/15/94 0820		DATE/TIME FINISH: 12/14/94 1700
PROJECT NAME: RAAP		
CLIENT: US AEC		
PROJECT NO.: 722843		

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
1								SILT, SOME SAND, LITTLE CLAY, MICACEOUS, DARK BROWN		TOC 1688.8' 1.6' STICK UP	1
2							SM				2
3	1	90	NA	8.1	HS	MOSS SPOON	GM	SILT, GRAVEL, GRAY			3
4											4
5											5
6								SAND AND SILT, BROWN, MICACEOUS, GRAVEL		GROUT TO SURFACE	6
7											7
8	2*	50	NA	4.1	HS	MOSS SPOON	GM/SM	STAINING AT 9-10 FEET			8
9											9
10											10
11								SILT, SOME SAND, LITTLE CLAY, BROWN, MICACEOUS, GRAVEL, LIMESTONE PEBBLES		BENTONITE SEAL	11
12	3	50	NA	9.5	HS	MOSS SPOON	GM/ML				12
13											13
14											14
15											15
16											16
17	4*	5	NA	11.1	HS	MOSS SPOON				TOP OF SAND PACK AT 18.6', SCREEN FROM 20.6' TO 30.6'	17
18											18
19											19
20											20
21											21
22											22
23											23
24											24
25											25
26	5	65	10,11 20,27	12.3	HS	SS 25'-27'	ML	SILT, SOME CLAY, BROWN, WET			26
27											27
28	6	5	100/2				LM/SN	LIMESTONE, GRAY, WEATHERED			28
29											29
30											30
31								END OF BORING AT 30.6 FEET			31
32											32
33											33
34											34
35											35

HSA = HOLLOW STEM AUGER CAL = CALIBRATION USCS = UNIFIED SOIL CLASS. SYS.	SS = SPLIT SPOON A = AUGER CUTTINGS * = LAB SAMPLE	BH = BORE HOLE GS = GRAB SAMPLE ∇ = WATER LEVEL	HS = HEADSPACE COMMENTS: 4 INCH ID PVC, SCH 40 0.01 INCH SLOT SCREEN
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CONTRACTOR: CT & E		PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO.: 31MW4
GEOLOGIST: BACHOVCHIN/GLENNIE			LOCATION: SWMU 31 WEST LAGOON
DRILLING METHOD: HSA/AIR ROTARY			WEATHER: SHOWERS, 40° F
DTW FROM TOC: 23.8 FT			DATE/TIME START: 12/15/94 0840
DATE/TIME: 12/15/94 1320		PROJECT NAME: RAAP	DATE/TIME FINISH: 12/15/94 1200
		CLIENT: US AEC	
		PROJECT NO.: 722843	

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
1								SILT, SOME CLAY, LITTLE SAND, DARK BROWN		TOC 1698.6'	1
2										1.4'	2
3							ML			STICK UP	3
4											4
5											5
6	1	80	5,8	0.8	HS	SS					6
7			7,7			5'-7'					7
8								SILT AND CLAY, BROWN, MUCH GRAVEL			8
9											9
10											10
11	2*	75	37,8	1.8	HS	SS	GM/ML			GROUT TO SURFACE	11
12			8,7			10'-12'					12
13											13
14											14
15											15
16	3	80	11,5	1.9	HS	SS				BENTONITE SEAL	16
17			6,5			15'-17'					17
18											18
19											19
20											20
21	4*	5	11,10	3.3	HS	SS					21
22			28,34			20'-22'				TOP OF SAND PACK AT 17', SCREEN FROM 18' TO 29'	22
23							GM	GRAVEL, SOME SILT, GRAY			23
24								AUGER REFUSAL AT 25 FEET, SWITCHED TO AIR ROTARY			24
25											25
26	5	5	100/5	0.0	SS	SS	LMSN	WET AT 25 FEET			26
27						25'-27'		LIMESTONE, GRAY, WEATHERED			27
28											28
29											29
30								END OF BORING AT 30 FEET			30
31											31
32											32
33											33
34											34
35											35

HSA = HOLLOW STEM AUGER
 CAL = CALIBRATION
 USCS = UNIFIED SOIL CLASS. SYS.

SS = SPLIT SPOON
 A = AUGER CUTTINGS
 * = LAB SAMPLE

BH = BORE HOLE
 GS = GRAB SAMPLE
 ↓ = WATER LEVEL

COMMENTS:
 4 INCH ID PVC, SCH 40
 0.01 INCH SLOT SCREEN

CONTRACTOR: CT & E	PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO: 48SB4
GEOLOGIST: BACHOVCHIN/GLENNIE		LOCATION: SWMU 48 UPPER DISPOSAL AREA
DRILLING METHOD: HSA		WEATHER: DAMP, 40° F
DTW FROM TOC: NA		DATE/TIME START: 12/17/94 0850
DATE/TIME: NA	PROJECT NAME: RAAP	DATE/TIME FINISH: 12/17/94 1050
	CLIENT: US AEC	
	PROJECT NO.: 722843	

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
1							GM	GRAVEL AND ASH, SOME SILT, BLACK		SURFACE ELEVATION 1830.4' (MSL)	1
2											2
3	1	100	NA	1.2	HS	MOSS SPOON		CLAY AND SILT, LITTLE SAND, BROWN-ORANGE, MICACEOUS AT 9 FEET			3
4							CL				4
5											5
6											6
7											7
8	2	100	NA	2.9	HS	MOSS SPOON					8
9											9
10											10
11								SAND AND SILT, LITTLE CLAY, ORANGE-BROWN			11
12	3*	75	NA	3.8	HS	MOSS SPOON	SM				12
13								HARD DRILLING AT 14 FEET DUE TO GRAVEL			13
14											14
15	4	10	100 4"	0.0	HS	SS 14'-16'	GM/SM	GRAVEL, SAND AND SILT, BROWN, PEBBLE TO COBBLE SIZE GRAVEL			15
16											16
17	5	0	100 2"			SS 16'-18'					17
18											18
19	6	0	46, 100 5"			SS 18'-19'					19
20											20
21	7*	10	37,64 100 3"	2.0	SS	SS 20'-21'	ML	SILT, SOME SAND AND CLAY, YELLOW-BROWN			21
22								END OF BORING AT 21 FEET			22
23											23
24											24
25											25

HSA = HOLLOW STEM AUGER
CAL = CALIBRATION
USCS = UNIFIED SOIL CLASS. SYS.

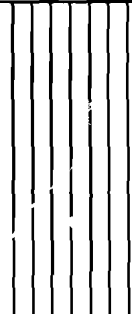
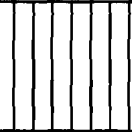
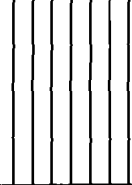
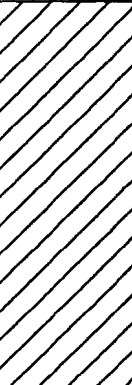
SS = SPLIT SPOON
A = AUGER CUTTINGS
* = LAB SAMPLE

BH = BORE HOLE
GS = GRAB SAMPLE

HS = HEADSPACE
▽ = WATER LEVEL

COMMENTS:
4 INCH DIAMETER BORING
GROUTED TO SURFACE

CONTRACTOR: CT & E	PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO: 48SB5
GEOLOGIST: BACHOVCHIN/GLENNIE		LOCATION: SWMU 48 LOWER DISPOSAL AREA
DRILLING METHOD: HSA		WEATHER: DAMP, 45° F
DTW FROM TOC: NA	PROJECT NAME: RAAP	DATE/TIME START: 12/17/94 1140
DATE/TIME: NA	CLIENT: US AEC	DATE/TIME FINISH: 12/17/94 1510
	PROJECT NO.: 722843	

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
1								SILT, SOME SAND, SOME CLAY, DARK ORANGE-BROWN		SURFACE ELEVATION 1823.5' (MSL)	1
2											2
3	1	100	NA	2.6	HS	MOSS SPOON	ML				3
4											4
5											5
6											6
7	2	75	NA	2.9	HS	MOSS SPOON			7		
8									8		
9									9		
10	3	25	NA	10	HS	MOSS SPOON	GM/SM	SILT AND SAND, GRAVEL, ORANGE-BROWN, HYDROCARBON ODOR AT 10.5 FEET			10
11	4	10	30	1.9	HS	SS					11'-12'
12			100								12
13			3"								13
14	5	35	75,60	131	HS	SS	ML	SILT AND CLAY, SOME SAND, LIGHT BROWN, STRONG HYDROCARBON ODOR, SOME GRAVEL			14
15			19,18								13'-15'
16	6	0	38,74	—	—	SS					16
17			100								17
18	7*	50	2"	213	SS	SS	GM/ML	SILT AND SAND, YELLOW-BROWN, GRAVEL, STRONG HYDROCARBON ODOR			18
19			43,56								17'-19'
20	8	75	18,12	125	HS	SS	ML	SILT, SOME SAND, LITTLE CLAY, WEATHERED GREEN SILTSTONE, STRONG HYDROCARBON ODOR			20
21			20,12								19'-21'
22			9,11								22
23											23
24											24
25											25
26	9	95	5,10	201	HS	SS		CLAY AND SILT, ORANGE, INTERBEDDED WEATHERED SILTSTONE, HYDROCARBON ODOR DECREASING TO BOTTOM, MORE COMPETENT SILTSTONE, GREEN AT 35 FEET			26
27			15,30								25'-27'
28											28
29											29
30											30
31	10	95	7,12	180	HS	SS	CL				31
32			12,14								30'-32'
33											33
34											34
35										35	
36	11*	95	20,31	3.4	HS	SS				36	
37			42,42							37	
38								END OF BORING AT 37 FEET		38	
39										39	
40										40	

HSA = HOLLOW STEM AUGER
 CAL = CALIBRATION
 USCS = UNIFIED SOIL CLASS. SYS.

SS = SPLIT SPOON
 A = AUGER CUTTINGS
 * = LAB SAMPLE

BH = BORE HOLE
 GS = GRAB SAMPLE
 HS = HEADSPACE
 † = WATER LEVEL

COMMENTS:
 4 INCH DIAMETER BORING
 GROUTED TO SURFACE

CONTRACTOR: CT & E	PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO.: 48MW1
GEOLOGIST: BACHOVCHIN/GLENNIE		LOCATION: SWMU 48 NW OF LOWER DISPOSAL AREA
DRILLING METHOD: HSA/AIR ROTARY		WEATHER: DAMP, 45° F
DTW FROM TOC: 122 FT (FROM SURFACE)		DATE/TIME START: 12/17/94 1545
DATE/TIME: 12/19/94 1200	PROJECT NAME: RAAP	DATE/TIME FINISH: 12/19/94 1255
	CLIENT: US AEC	
	PROJECT NO.: 722843	

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
1								SILT, SOME CLAY, SOME SAND, ORANGE-BROWN			1
2											2
3											3
4											4
5											5
6	1	100	11,9	3.4	SS	SS	ML				6
7			7,14			5'-7'					7
8											8
9											9
10								SILT AND SAND, GRAVEL, ORANGE-BROWN, SLIGHT ODOR			10
11	2	100	3,3	3.5	HS	SS	GM/SM				11
12			4,6			10'-12'					12
13								SILT AND CLAY, ORANGE-BROWN TO YELLOW-BROWN			13
14											14
15											15
16											16
17											17
18								SILT BECOMING MORE COMPETENT, MORE RED, WEATHERED, LAYERED			18
19											19
20											20
21	3*	95	11,8	4.0	HS	SS	ML				21
22			7,10			20'-22'					22
23											23
24											24
25											25
26	4	95	8,7	1.1	HS	SS					26
27			8,10			25'-27'					27
28											28
29											29
30											30
31	5	80	13,9	0.0	HS	SS					31
32			10,11			30'-32'					32
33											33
34											34
35											35
36	6	75	9,12	4.0	HS	SS					36
37			9,9			35'-37'					37
38											38
39											39
40											40
41	7	95	7,9	0.0	HS	SS					41
42			10,9			40'-42'					42
43											43
44											44
45											45

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SS = SPLIT SPOON

A = AUGER CUTTINGS

* = LAB SAMPLE

BH = BORE HOLE

GS = GRAB SAMPLE

HS = HEADSPACE

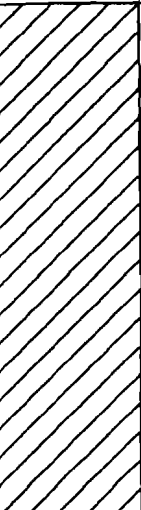
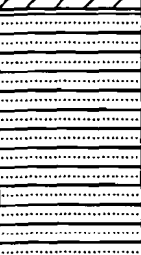
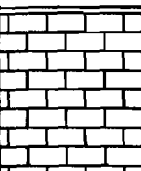
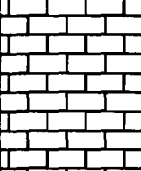
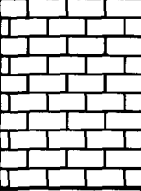
‡ = WATER LEVEL

COMMENTS:

4 INCH ID PVC, SCH 40

0.01 INCH SLOT SCREEN

CONTRACTOR: <u>CT & E</u> GEOLOGIST: <u>BACHOVCHIN/GLENNIE</u> DRILLING METHOD: <u>HSA/AIR ROTARY</u> DTW FROM TOC: <u>122 FT (FROM SURFACE)</u> DATE/TIME: <u>12/19/94 1200</u>			PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD			BORING NO: <u>48MWI</u> LOCATION: <u>SWMU 48</u> WEATHER: <u>DAMP, 45° F</u> DATE/TIME START: <u>12/17/94 1545</u> DATE/TIME FINISH: <u>12/19/94 1255</u>		
			PROJECT NAME: <u>RAAP</u> CLIENT: <u>US AEC</u> PROJECT NO.: <u>722843</u>					

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
46	8	100	9,70	2.8	HS	SS		CLAY AND SILT, TRACE SAND, BROWN, SLIGHTLY DAMP AT 52 FEET, WEATHERED		GROUT TO SURFACE	46
47			17,18			SS					47
48											48
49											49
50											50
51	9	75	9,9	6.0	HS	SS	CL	SWITCHED TO AIR ROTARY DRILLING AT 60 FEET		GROUT TO SURFACE	51
52			9,9			SS					52
53	10*	75	16,8	6.0	HS	SS					53
54			9,8			SS					54
55											55
56											56
57											57
58											58
59											59
60											60
61	11	60	10,10	4.5	HS	SS		SILTSTONE, GREEN-BROWN, WEATHERED, VERY DAMP AT 66 FEET		GROUT TO SURFACE	61
62			10,10			SS					62
63											63
64											64
65											65
66	12	100	12,28	3.9	HS	SS	SLSN	DISTINCT CHANGE AT 72 FEET		GROUT TO SURFACE	66
67			31,75			SS					67
68											68
69											69
70											70
71											71
72								LIMESTONE, DARK BROWN CUTTINGS, ARGILLACEOUS		BENTONITE SEAL	72
73											73
74											74
75											75
76											76
77											77
78											78
79											79
80							LMSN				80
81											81
82											82
83											83
84											84
85											85
86											86
87											87
88											88
89											89
90											90

HSA = HOLLOW STEM AUGER CAL = CALIBRATION USCS = UNIFIED SOIL CLASS. SYS.	SS = SPLIT SPOON A = AUGER CUTTINGS * = LAB SAMPLE	BH = BORE HOLE GS = GRAB SAMPLE ♀ = WATER LEVEL
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COMMENTS: 4 INCH ID PVC, SCH 40 0.01 INCH SLOT SCREEN
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CONTRACTOR: CT & E

GEOLOGIST: BACHOVCHIN/GLENNIE

DRILLING METHOD: HSA/AIR ROTARY

DTW FROM TOC: 122 FT (FROM SURFACE)

DATE/TIME: 12/19/94 1200

**PARSONS
ENGINEERING-SCIENCE, INC.
DRILLING RECORD**

BORING NO: 48MW1

LOCATION: SWMU 48

WEATHER: DAMP, 45° F

DATE/TIME START: 12/17/94 1545

DATE/TIME FINISH: 12/19/94 1255

PROJECT NAME: RAAP

CLIENT: US AEC

PROJECT NO.: 722843

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
91								LIMESTONE, DARK BROWN CUTTINGS, ARGILLACEOUS			91
92											92
93											93
94							LMSN	STOPPED OVERNIGHT AT 94 FEET, NO WATER IN HOLE 12-19-94			94
95											95
96											96
97											97
98											98
99								DRILLING RATE IS APPROXIMATELY 1 FOOT/1.5 MINUTES			99
100											100
101								DOLOMITE, GRAY, WEATHERED, SOFT			101
102											102
103											103
104											104
105											105
106											106
107											107
108											108
109								DRILLING RATE IS APPROXIMATELY 1 FOOT/2.5 MINUTES			109
110											110
111											111
112											112
113											113
114											114
115											115
116											116
117											117
118											118
119											119
120							DLMT				120
121											121
122											122
123											123
124											124
125											125
126											126
127											127
128											128
129											129
130											130
131											131
132											132
133											133
134											134
135											135

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 GS = GRAB SAMPLE

HS = HEADSPACE
 ♡ = WATER LEVEL

COMMENTS:
 4 INCH 10 PVC, SCH 40
 0.01 INCH SLOT SCREEN

CONTRACTOR: CT & E	PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO: 48MW1
GEOLOGIST: BACHOVCHIN/GLENNIE		LOCATION: SWMU 48
DRILLING METHOD: HSA/AIR ROTARY		WEATHER: DAMP, 45° F
DTW FROM TOC: 122 FT (FROM SURFACE)		DATE/TIME START: 12/17/94 1545
DATE/TIME: 12/18/94 1200	PROJECT NAME: RAAP	DATE/TIME FINISH: 12/19/94 1255
	CLIENT: US AEC	
	PROJECT NO.: 722843	

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
136								DOLOMITE, GRAY, WEATHERED, SOFT			136
137											137
138											138
139											139
140											140
141											141
142											142
143											143
144											144
145											145
146											146
147											147
148											148
149											149
150											150
151											151
152											152
153											153
154											154
155								END OF BORING AT 154 FEET			155
156											156
157											157
158											158
159											159
160											160
161											161
162											162
163											163
164											164
165											165
166											166
167											167
168											168
169											169
170											170
171											171
172											172
173											173
174											174
175											175
176											176
177											177
178											178
179											179
180											180

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 A = AUGER CUTTINGS
 * = LAB SAMPLE

BH = BORE HOLE
 GS = GRAB SAMPLE
 ▽ = WATER LEVEL

COMMENTS:
 4 INCH ID PVC, SCH 40
 0.01 INCH SLOT SCREEN

24

CONTRACTOR: CT & E		PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO: 48MW2
GEOLOGIST: BACHOVCHIN/GLENNIE			LOCATION: SWMU 48 SW OF LOWER DISPOSAL AREA
DRILLING METHOD: HSA/AIR ROTARY			WEATHER: CLEAR, 25° F
DTW FROM TOC: 126 FT (FROM SURFACE)			DATE/TIME START: 12/19/94 1630
DATE/TIME: 1/07/95 0830		PROJECT NAME: RAAP	DATE/TIME FINISH: 1/07/95 1200
		CLIENT: US AEC	
		PROJECT NO.: 722843	

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
1								SILT, SOME SAND AND CLAY, RED-BROWN		TOC 1818.88' 1.3' STICK UP 	1
2											2
3											3
4											4
5											5
6	1	60	8,12 15,16	0.0	HS	SS 5'-7'	ML				6
7											7
8											8
9											9
10											10
11	2	75	7,5 5,4	0.0	HS	SS 10'-12'	SM	SILT AND SAND, BROWN			11
12											12
13											13
14											14
15											15
16											16
17								VERY HARD DRILLING AT 17 FEET (GRAVEL)			17
18											18
19											19
20											20
21	3	5	100/ 2.5	0.0	HS	SS 20'-22'	GM/ML	SILT AND CLAY, SOME SAND, LIGHT BROWN, GRAVEL		GROUT TO SURFACE 	21
22											22
23											23
24											24
25											25
26											26
27											27
28											28
29											29
30											30
31	4	30	10,8 5,4	0.0	HS	SS 30'-32'					31
32											32
33											33
34											34
35											35
36											36
37											37
38											38
39											39
40											40
41	5*	90	18,25 25,28			SS 40'-42'	DLMT	DOLOMITE, WEATHERED, LIGHT GRAY, ARGILLACEOUS, INTERBEDDED SILTSTONE			41
42											42
43											43
44											44
45	6*	5	100/1			SS 44'-46'		SWITCHED TO AIR HAMMER AT 44 FT			45
46											46

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SS = SPLIT SPOON
 A = AUGER CUTTINGS
 * = LAB SAMPLE

BH = BORE HOLE
 GS = GRAB SAMPLE

HS = HEADSPACE
 ♡ = WATER LEVEL

COMMENTS:
 2 INCH ID PVC, SCH 40
 0.01 INCH SLOT SCREEN

CONTRACTOR: CT & E		PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO: 48MW2
GEOLOGIST: BACHOVCHIN/GLENNIE			LOCATION: SWMU 48
DRILLING METHOD: HSA/AIR ROTARY			WEATHER: CLEAR, 25° F
DTW FROM TOC: 128 FT (FROM SURFACE)		PROJECT NAME: RAAP	DATE/TIME START: 12/19/94 1830
DATE/TIME: 1/07/95 0830		CLIENT: US AEC	DATE/TIME FINISH: 1/07/95 1200
		PROJECT NO.: 722843	

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PTD (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
47								DOLOMITE, WEATHERED, LIGHT GRAY			47
48											48
49											49
50							SLSN	SILTSTONE, LIGHT BROWN, WEATHERED, INTERBEDDED GRAY DOLOMITE			50
51											51
52											52
53											53
54								DRILLING RATE (1 FOOT/3 MINUTES)			54
55											55
56											56
57											57
58											58
59											59
60											60
61								DOLOMITE, WEATHERED, LIGHT GRAY, ARGILLACEOUS			61
62											62
63											63
64							DLMT				64
65								DRILLING RATE (1 FOOT/2.3 MINUTES)			65
66											66
67											67
68											68
69											69
70											70
71								NOTE: SOFT FORMATION NOT RETURNING CUTTINGS UP HOLE. MUST SET TEMPORARY CASING. HOLE IS STOPPED AT 80 FEET OVER HOLIDAY, RESUME DRILLING ON 1-5-95.		GROUT TO SURFACE	71
72											72
73											73
74											74
75											75
76											76
77											77
78											78
79											79
80								LIMESTONE, WEATHERED, GRAY-BROWN			80
81											81
82											82
83							LMSN				83
84											84
85											85
86											86
87											87
88											88
89											89
90											90
91											91
92											92

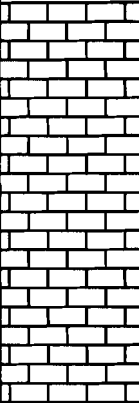
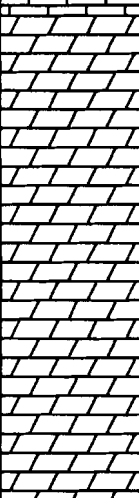
HSA = HOLLOW STEM AUGER CAL = CALIBRATION USCS = UNIFIED SOIL CLASS. SYS.	SS = SPLIT SPOON A = AUGER CUTTINGS * = LAB SAMPLE	BH = BORE HOLE GS = GRAB SAMPLE ∇ = WATER LEVEL	HS = HEADSPACE COMMENTS: 2 INCH ID PVC, SCH 40 0.01 INCH SLOT SCREEN
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CONTRACTOR: CT & E	PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO: 48MW2
GEOLOGIST: BACHOVCHIN/GLENNIE		LOCATION: SWMU 48
DRILLING METHOD: HSA/AIR ROTARY		WEATHER: CLEAR, 25' F
DTW FROM TOC: 128 FT (FROM SURFACE)		DATE/TIME START: 12/19/94 1630
DATE/TIME: 1/07/95 0830	PROJECT NAME: RAAP	DATE/TIME FINISH: 1/07/95 1200
	CLIENT: US AEC	
	PROJECT NO.: 722843	

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
93							LMSN	LIMESTONE, WEATHERED, GRAY-BROWN			93
94											94
95								DRILLING RATE (1 FOOT/1.7 MINUTES)		GROUT TO SURFACE	95
96											96
97											97
98											98
99											99
100											100
101										BENTONITE SEAL	101
102											102
103											103
104											104
105											105
106											106
107											107
108											108
109											109
110							DLMT	DOLOMITE, LIGHT GRAY, WEATHERED, ALTERNATING HARD AND SOFT, GRAY AND BROWN, LAYERS			110
111											111
112											112
113											113
114											114
115											115
116											116
117										TOP OF SAND PACK AT 104', SCREEN FROM 113.7' TO 133.7'	117
118											118
119											119
120											120
121											121
122											122
123											123
124											124
125								DRILLING RATE (1 FOOT/3.3 MINUTES)			125
126											126
127											127
128											128
129											129
130											130
131											131
132											132
133											133
134								END OF BORING AT 133.7 FEET			134
135											135
136											136
137											137
138											138

HSA = HOLLOW STEM AUGER CAL = CALIBRATION USCS = UNIFIED SOIL CLASS. SYS.	SS = SPLIT SPOON A = AUGER CUTTINGS * = LAB SAMPLE	BH = BORE HOLE GS = GRAB SAMPLE ∇ = WATER LEVEL	HS = HEADSPACE COMMENTS: 2 INCH ID PVC, SCH 40 0.01 INCH SLOT SCREEN
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CONTRACTOR: <u>CT & E</u>	PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO: <u>48MW3</u>
GEOLOGIST: <u>BACHOVCHIN/GLENNIE</u>		LOCATION: <u>SWMU 48</u>
DRILLING METHOD: <u>HSA/AIR ROTARY</u>		WEATHER: <u>WET, COLD, 40° F</u>
DTW FROM TOC: <u>119 FT (FROM SURFACE)</u>	PROJECT NAME: <u>RAAP</u>	DATE/TIME START: <u>1/07/95 1237</u>
DATE/TIME: <u>1/08/95 1430</u>	CLIENT: <u>US AEC</u>	DATE/TIME FINISH: <u>1/08/95 1430</u>
	PROJECT NO.: <u>722843</u>	

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
91							LMSN	LIMESTONE, LIGHT GRAY, DRILLING RATE (1 FOOT/4 MINUTES)		↑ TOP OF SAND PACK AT 90', SCREEN FROM 100' TO 120' ↓ 	91
92											92
93											93
94											94
95											95
96											96
97											97
98											98
99											99
100											100
101							101				
102							102				
103							103				
104							104				
105							DLMT	DOLOMITE, LIGHT GRAY, POSSIBLE WET ZONE AT 112 FEET DRILLING RATE (1 FOOT/3.5 MINUTES)			105
106											106
107											107
108											108
109											109
110											110
111											111
112										112	
113										113	
114										114	
115							115				
116							116				
117							117				
118							118				
119							119				
120							120				
121							121				
122							122				
123								END OF BORING AT 122 FEET		123	
124										124	
125										125	
126										126	
127										127	
128										128	
129										129	
130										130	
131										131	
132										132	
133										133	
134										134	
135										135	

HSA = HOLLOW STEM AUGER

CAL = CALIBRATION

USCS = UNIFIED SOIL CLASS. SYS.

SS = SPLIT SPOON

A = AUGER CUTTINGS

* = LAB SAMPLE

BH = BORE HOLE

GS = GRAB SAMPLE

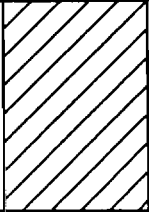
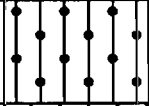
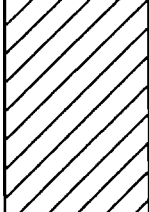
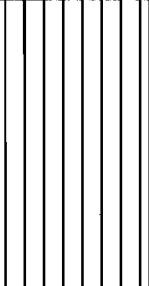
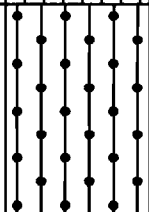
HS = HEADSPACE

W = WATER LEVEL

COMMENTS:

4 INCH ID PVC, SCH 40
0.01 INCH SLOT SCREEN

CONTRACTOR: <u>CT & E</u>	PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO: <u>48MW4</u>
GEOLOGIST: <u>BACHOVCHIN/GLENNIE</u>		LOCATION: <u>SWMU 48</u> <u>CENTER OF UPPER DISPOSAL AREA</u>
DRILLING METHOD: <u>HSA/AIR ROTARY</u>		WEATHER: <u>RAIN, 85° F</u>
DTW FROM TOC: <u>78.19 FT</u>		DATE/TIME START: <u>7/18/95 1100</u>
DATE/TIME: <u>7/22/95 1200</u>	PROJECT NAME: <u>RAAP</u>	DATE/TIME FINISH: <u>7/20/95 1830</u>
	CLIENT: <u>US AEC</u>	
	PROJECT NO.: <u>722843</u>	

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
1								CLAY AND SILT, LITTLE SAND, RED-BROWN		TOC 1832.6 2.06' STICK UP ↑	1
2											2
3				0.1	BH		CL				3
4											4
5										↑ GROUT TO SURFACE	5
6											6
7											7
8											8
9				0.0	BH		GM	SILT AND GRAVEL, LITTLE SAND, ORANGE-BROWN			9
10											10
11											11
12											12
13								CLAY AND SILT, LITTLE SAND, RED-BROWN, MOIST			13
14											14
15											15
16											16
17				0.0	BH		CL				17
18											18
19											19
20											20
21											21
22											22
23											23
24											24
25				0.0	BH						25
26											26
27											27
28											28
29											29
30											30
31											31
32											32
33				0.0	BH		ML	SILT AND CLAY, ORANGE-BROWN, MOIST ZONE AT 40-41 FEET			33
34											34
35											35
36											36
37											37
38											38
39											39
40											40
41											41
42											42
43											43
44											44
45				0.0	BH		GM	SAND AND GRAVEL, SOME SILT, BROWN, MOIST, GRAVEL LAYER AT 49 FEET			45
46											46
47											47
48											48
49											49

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SS = SPLIT SPOON
 A = AUGER CUTTINGS
 * = LAB SAMPLE

BH = BORE HOLE
 GS = GRAB SAMPLE
 HS = HEADSPACE
 ♣ = WATER LEVEL

COMMENTS:
 4 INCH ID PVC, SCH 40
 0.01 INCH SLOT SCREEN

CONTRACTOR: <u>CT & E</u>	PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO.: <u>48MW4</u>
GEOLOGIST: <u>BACHOVCHIN/GLENNIE</u>		LOCATION: <u>SWMU 48</u>
DRILLING METHOD: <u>HSA/AIR ROTARY</u>		WEATHER: <u>RAIN, 85° F</u>
DTW FROM TOC: <u>78.19 FT</u>	PROJECT NAME: <u>RAAP</u>	DATE/TIME START: <u>7/18/95 1100</u>
DATE/TIME: <u>7/22/95 1200</u>	CLIENT: <u>US AEC</u>	DATE/TIME FINISH: <u>7/20/95 1830</u>
	PROJECT NO.: <u>722843</u>	

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
50								SILT, BROWN, BECOMING MORE COMPETENT, SWITCHED TO AIR ROTARY DRILLING AT 55 FEET			50
51											51
52				0.0	BH		ML				52
53											53
54											54
55											55
56											56
57											57
58											58
59											59
60				0.0	BH		SLSN				60
61											61
62											62
63											63
64											64
65											65
66											66
67											67
68											68
69											69
70											70
71				0.0	BH						71
72											72
73											73
74											74
75											75
76											76
77											77
78											78
79											79
80											80
81											81
82											82
83											83
84				0.0	BH						84
85											85
86											86
87											87
88											88
89											89
90											90
91											91
92											92
93											93
94				0.0	BH		DLMT				94
95											95
96											96
97											97
98											98

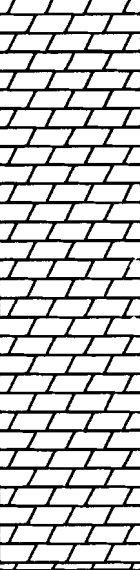
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SS = SPLIT SPOON
 A = AUGER CUTTINGS
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BH = BORE HOLE
 GS = GRAB SAMPLE
 HS = HEADSPACE
 ∇ = WATER LEVEL

COMMENTS:
 4 INCH ID PVC, SCH 40
 0.01 INCH SLOT SCREEN

CONTRACTOR: <u>CT & E</u> GEOLOGIST: <u>BACHOVCHIN/GLENNIE</u> DRILLING METHOD: <u>HSA/AIR ROTARY</u> DTW FROM TOC: <u>78.19 FT</u> DATE/TIME: <u>7/22/95 1200</u>			PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD				BORING NO: <u>48MW4</u> LOCATION: <u>SWMU 48</u> WEATHER: <u>RAIN, 85° F</u> DATE/TIME START: <u>7/18/95 1100</u> DATE/TIME FINISH: <u>7/20/95 1830</u>		
			PROJECT NAME: <u>RAAP</u> CLIENT: <u>US AEC</u> PROJECT NO.: <u>722843</u>						

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
99								DOLOMITE, GREEN-GRAY, AND INTERBEDDED DARK GRAY SILTSTONE, SOFT ZONE AT 100-108 FEET (WATER?)		SAND PACK TO 120'	99
100											100
101											101
102											102
103											103
104											104
105											105
106											106
107											107
108				0.0	BH		DLMT				108
109								109			
110								110			
111								111			
112								112			
113								113			
114								114			
115								115			
116								116			
117								117			
118								118			
119								119			
120								END OF BORING AT 120 FEET			120
121											121
122											122
123											123
124											124
125											125
126											126
127											127
128											128
129											129
130											130
131											131
132											132
133											133
134											134
135											135
136											136
137											137
138											138
139											139
140											140
141											141
142											142
143											143
144											144
145											145
146											146
147											147

HSA = HOLLOW STEM AUGER CAL = CALIBRATION USCS = UNIFIED SOIL CLASS. SYS.	SS = SPLIT SPOON A = AUGER CUTTINGS * = LAB SAMPLE	BH = BORE HOLE GS = GRAB SAMPLE ▽ = WATER LEVEL
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COMMENTS:
 4 INCH ID PVC, SCH 40
 0.01 INCH SLOT SCREEN

CONTRACTOR: CT & E	PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO: 54SB1
GEOLOGIST: BACHOVCHIN/GLENNIE		LOCATION: SWMU 54 SOUTH OF LOWER MOUND
DRILLING METHOD: HSA		WEATHER: COLD, 30° F
DTW FROM TOC: NA		DATE/TIME START: 12/20/94 1610
DATE/TIME: NA	PROJECT NAME: RAAP	DATE/TIME FINISH: 12/20/94 1700
	CLIENT: US AEC	
	PROJECT NO.: 722843	

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
1	1*	65	3,5	5.9	SS	SS	ML	SILT, SOME CLAY, LITTLE SAND, DARK BROWN, POSSIBLE ASH OR STAINING AT 2 FEET		SURFACE ELEVATION 1697.3' (MSL)	1
2			6,6			0-2'					2
3	2	60	4,6	5.8	SS	SS					3
4			9,9			2-4'					4
5											5
6	3	85	6,7	5.3	SS	SS					6
7			7,9			5-7'					7
8											8
9											9
10											10
11	4	90	4,5	5.2	SS	SS	SM	SAND, SOME SILT, DARK BROWN, MOIST			11
12			7,8			10-12'					12
13											13
14											14
15											15
16	5	90	10,7	4.9	HS	SS					16
17			37,32			15-17'					17
18											18
19											19
20											20
21	6*	90	28,40	6.0	HS	SS	LMSN	LIMESTONE, WEATHERED, GREEN-GRAY			21
22			100/5			20-22'					22
23											23
24											24
25											25
26											26

HSA = HOLLOW STEM AUGER
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SS = SPLIT SPOON
A = AUGER CUTTINGS
* = LAB SAMPLE

BH = BORE HOLE
GS = GRAB SAMPLE
g = WATER LEVEL

COMMENTS:
4 INCH DIAMETER BORING
GROUTED TO SURFACE

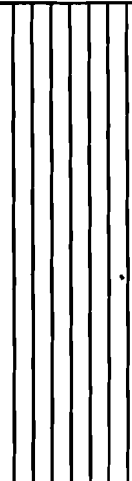
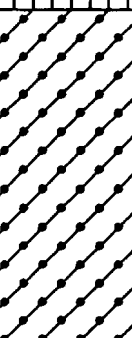
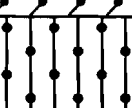
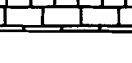
CONTRACTOR: CT & E		PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD				BORING NO: 54SB2			
GEOLOGIST: BACHOVCHIN/GLENNIE						LOCATION: SWMU 54 SOUTH OF LOWER MOUND			
DRILLING METHOD: HSA						WEATHER: COLD, 30° F			
DTW FROM TOC: NA						DATE/TIME START: 12/21/94 0945			
DATE/TIME: NA		PROJECT NAME: RAAP				DATE/TIME FINISH: 12/21/94 1030			
		CLIENT: US AEC							
		PROJECT NO.: 722843							

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PTD (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)			
1	1*	50	6,4 4,9	7.0	HS	SS 0-2'	ML	SILT, SOME CLAY, LITTLE SAND, DARK BROWN		SURFACE ELEVATION 1000.1' (MSL)	1			
2														2
3	2	70	10,5 8,10	7.9	SS	SS 2-4'								3
4														4
5														5
6	3	90	2,3 4,3	8.7	SS	SS 5-7'								6
7														7
8														8
9														9
10														10
11	4	90	3,6 8,5	8.9	SS	SS 10-12'								11
12														12
13														13
14														14
15														15
16	5*	90	1,2 2,1	8.2	SS	SS 15-17'								16
17										17				
18										18				
19										19				
20										20				
21	6	60	22,38 35 50/2	4.8	SS	SS 20-22'	GM	GRAVEL, SOME SILT, WET			21			
22							SLSN	SILTSTONE, WEATHERED, GRAY			22			
23								END OF BORING AT 22 FEET			23			
24											24			
25											25			
26											26			

HSA = HOLLOW STEM AUGER CAL = CALIBRATION USCS = UNIFIED SOIL CLASS. SYS.	SS = SPLIT SPOON A = AUGER CUTTINGS * = LAB SAMPLE	BH = BORE HOLE GS = GRAB SAMPLE ♯ = WATER LEVEL
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COMMENTS:
 4 INCH DIAMETER BORING
 GROUTED TO SURFACE

CONTRACTOR: CT & E GEOLOGIST: BACHOVCHIN/GLENNIE DRILLING METHOD: HSA DTW FROM TOC: NA DATE/TIME: NA	PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO.: 54SB3 LOCATION: SWMU 54 WEST OF LOWER MOUND WEATHER: COLD, 30° F. DATE/TIME START: 12/21/94 1036 DATE/TIME FINISH: 12/21/94 1110
PROJECT NAME: RAAP CLIENT: US AEC PROJECT NO.: 722843		

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)		
1	1*	75	5,6 6,6	1.6	HS	SS 0-2'	ML	SILT, SOME CLAY, DARK BROWN		SURFACE ELEVATION 1698.6' (MSL)	1		
2													2
3	2	75	6,6 6,4	1.5	HS	SS 2-4'							3
4													4
5											5		
6	3	70	2,3 3,5	1.9	HS	SS 5-7'					6		
7											7		
8											8		
9											9		
10											10		
11	4	95	8,10 11,5	1.9	HS	SS 10-12'	SM	SILT AND SAND, LITTLE CLAY, BROWN			11		
12													12
13													13
14											14		
15											15		
16	5*	40	5,13 24,32	2.0	HS	SS 15-17'					16		
17											17		
18							GM	GRAVEL, SOME SILT, WET			18		
19	6	60	45,52 REF.	9.8	SS	SS 18-19'	LMSN	LIMESTONE, WEATHERED, GREEN-GRAY, WET			19		
20								END OF BORING AT 19.5 FEET			20		
21											21		
22											22		
23											23		
24											24		
25											25		
26											26		

HSA = HOLLOW STEM AUGER CAL = CALIBRATION USCS = UNIFIED SOIL CLASS. SYS.	SS = SPLIT SPOON A = AUGER CUTTINGS * = LAB SAMPLE	BH = BORE HOLE GS = GRAB SAMPLE HS = HEADSPACE W = WATER LEVEL	COMMENTS: 4 INCH DIAMETER BORING GROUTED TO SURFACE
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CONTRACTOR: CT & E	PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO: 54SB4
GEOLOGIST: BACHOVCHIN/GLENNIE		LOCATION: SNMU 54 WEST OF LOWER MOUND
DRILLING METHOD: HSA		WEATHER: COLD, 35° F
DTW FROM TOC: NA		DATE/TIME START: 12/21/94 1120
DATE/TIME: NA		DATE/TIME FINISH: 12/21/94 1152
PROJECT NAME: RAAP		
CLIENT: US AEC		
PROJECT NO.: 722843		

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
1	1*	90	3,4	3.4	HS	SS		SILT AND CLAY, LITTLE SAND, DARK BROWN		SURFACE ELEVATION 1697.0' (MSL)	1
2			5,4			0-2'					2
3	2	95	4,5	3.2	HS	SS	ML				3
4			8,6			2-4'					4
5											5
6	3	95	6,7	4.8	HS	SS		CLAY AND SILT, SOME SAND, LIGHT BROWN			6
7			7,9			5-7'					7
8							CL/ML				8
9											9
10											10
11	4	90	2,3	4.9	HS	SS		SAND, LITTLE SILT, BROWN, MEDIUM COARSE			11
12			2,2			10-12'					12
13							SW				13
14											14
15											15
16	5*	60	2,2	4.0	HS	SS	SM	SAND AND SILT, SOME CLAY, MOIST, BROWN			16
17			3,8			15-17'					17
18	6	10	50/2	2.1	SS	SS	GM	GRAVEL, OVER WEATHERED, GREEN-GRAY LIMESTONE, WET			18
19						18-19'					19
20								END OF BORING AT 18.5 FEET			20
21											21
22											22
23											23
24											24
25											25
26											26

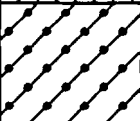
HSA = HOLLOW STEM AUGER
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SS = SPLIT SPOON
A = AUGER CUTTINGS
* = LAB SAMPLE

BH = BORE HOLE
GS = GRAB SAMPLE
v = WATER LEVEL

COMMENTS:
4 INCH DIAMETER BORING
GROUTED TO SURFACE

CONTRACTOR: <u>CT & E</u> GEOLOGIST: <u>BACHOVCHIN/GLENNIE</u> DRILLING METHOD: <u>HSA</u> DTW FROM TOC: <u>NA</u> DATE/TIME: <u>NA</u>	PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO.: <u>54SB5</u> LOCATION: <u>SWMU 54</u> <u>N. CENTER OF LOWER MOUND</u> WEATHER: <u>COLD, 35° F</u> DATE/TIME START: <u>12/21/94 1204</u> DATE/TIME FINISH: <u>12/21/94 1225</u>
PROJECT NAME: <u>RAAP</u> CLIENT: <u>US AEC</u> PROJECT NO.: <u>722843</u>		

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
1	1*	100	3.2 3.4	9.7	HS	SS 0-2'		SILT, SOME CLAY, LITTLE SAND, DARK BROWN		SURFACE ELEVATION 1897.0' (MSL) 	1
2											2
3											3
4											4
5											5
6	2	90	4.4 7.8	4.7	HS	SS 5-7'					6
7											7
8							ML				8
9											9
10											10
11	3	95	9.3 4.6	6.5	HS	SS 10-12'					11
12											12
13											13
14											14
15											15
16	4*	90	4.3 2.3	5.3	HS	SS 15-17'	SM	SILT AND SAND, BROWN			16
17											17
18							GM	GRAVEL, WET			18
19								END OF BORING AT 18 FEET			19
20											20
21											21
22											22
23											23
24											24
25											25
26											26

HSA = HOLLOW STEM AUGER CAL = CALIBRATION USCS = UNIFIED SOIL CLASS. SYS.	SS = SPLIT SPOON A = AUGER CUTTINGS * = LAB SAMPLE	BH = BORE HOLE GS = GRAB SAMPLE g = WATER LEVEL	HS = HEADSPACE	COMMENTS: 4 INCH DIAMETER BORING GROUTED TO SURFACE
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CONTRACTOR: CT & E

GEOLOGIST: BACHOVCHIN/GLENNIE

DRILLING METHOD: HSA

DTW FROM TOC: NA

DATE/TIME: NA

**PARSONS
ENGINEERING-SCIENCE, INC.
DRILLING RECORD**

BORING NO: 54SB6

LOCATION: SWMU 54
CENTER OF LOWER MOUND

WEATHER: CLOUDY, 45° F

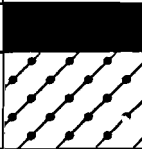
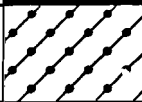
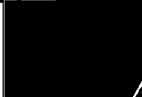
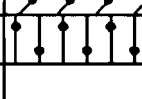
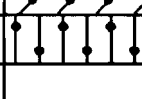
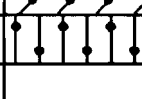
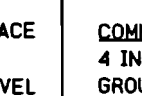
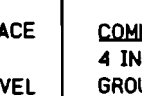
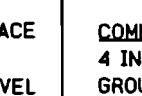
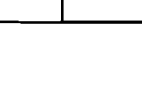
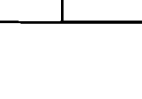
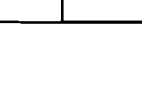
DATE/TIME START: 12/22/94 1100

DATE/TIME FINISH: 12/22/94 1200

PROJECT NAME: RAAP

CLIENT: US AEC

PROJECT NO.: 722843

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)	
1	1*	50	NA	32.0	HS	MOSS SPOON 0-5'	ASH	ASH, GLASSY, BLACK		SURFACE ELEVATION 1700.9' (MSL)	1	
2							SM	SILT AND SAND, LITTLE CLAY, BROWN				2
3							ASH	ASH, GLASSY, BLACK				3
4	2	50	NA	6.0	HS	MOSS SPOON 5-10'	ASH	ASH, GLASSY, BLACK			4	
5							SM	SILT AND SAND, RED-BROWN				5
6							ASH	ASH, GLASSY, BLACK-BROWN				6
7	3*	90	NA	6.5	HS	MOSS SPOON 10-15'	ASH	ASH, GLASSY, BLACK-BROWN			7	
8							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				8
9							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				9
10	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			10	
11							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				11
12							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				12
13	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			13	
14							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				14
15							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				15
16	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			16	
17							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				17
18							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				18
19	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			19	
20							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				20
21							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				21
22	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			22	
23							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				23
24							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				24
25	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			25	
26							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				26
27							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				27
28	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			28	
29							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				29
30							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				30
31	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			31	
32							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				32
33							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				33
34	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			34	
35							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				35
36							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				36
37	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			37	
38							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				38
39							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				39
40	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			40	
41							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				41
42							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				42
43	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			43	
44							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				44
45							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				45
46	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			46	
47							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				47
48							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				48
49	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			49	
50							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				50
51							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				51
52	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			52	
53							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				53
54							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				54
55	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			55	
56							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				56
57							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				57
58	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			58	
59							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				59
60							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				60
61	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			61	
62							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				62
63							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				63
64	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			64	
65							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				65
66							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				66
67	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			67	
68							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				68
69							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				69
70	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			70	
71							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				71
72							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				72
73	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			73	
74							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				74
75							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				75
76	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			76	
77							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				77
78							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				78
79	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			79	
80							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				80
81							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				81
82	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			82	
83							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				83
84							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				84
85	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			85	
86							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				86
87							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				87
88	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			88	
89							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				89
90							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				90
91	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			91	
92							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				92
93							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				93
94	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			94	
95							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				95
96							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				96
97	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			97	
98							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				98
99							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				99
100	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			100	
101							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				101
102							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				102
103	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			103	
104							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				104
105							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				105
106	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			106	
107							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				107
108							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				108
109	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST			109	
110							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				110
111							SM	SILT AND SAND, SOME CLAY, DARK BROWN, LESS CLAY AT BOTTOM, MOIST				111
112	4	75	NA	5.0	HS	MOSS SPOON 15-20'	SM	SILT AND SAND				

CONTRACTOR: <u>CT & E</u> GEOLOGIST: <u>BACHOVCHIN/GLENNIE</u> DRILLING METHOD: <u>HSA</u> DTW FROM TOC: <u>NA</u> DATE/TIME: <u>NA</u>	PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO: <u>54SB7</u> LOCATION: <u>SWMU 54</u> <u>EAST OF LOWER MOUND</u> WEATHER: <u>WARM, 50° F</u> DATE/TIME START: <u>12/22/94 1215</u> DATE/TIME FINISH: <u>12/22/94 1255</u>
	PROJECT NAME: <u>RAAP</u> CLIENT: <u>US AEC</u> PROJECT NO.: <u>722843</u>	

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
1	1*	90	2,3	0.0	HS	SS		SILT, SOME SAND, LITTLE CLAY, DARK BROWN		SURFACE ELEVATION 1700.1' (MSL)	1
2			4,7			0-2'					2
3							ML				3
4											4
5											5
6	2	95	7,4	0.0	HS	SS		SAND AND SILT, LITTLE CLAY, BROWN, MORE CLAY TOWARD 16 FEET			6
7			4,2			5-7'					7
8							SM				8
9											9
10											10
11	3	90	4,8	5.0	SS	SS					11
12			9,7			10-12'					12
13											13
14											14
15											15
16	4*	80	1,1	2.5	SS	SS					16
17			2,3			15-17'		SILT AND CLAY, SOME SAND, DARK BROWN			17
18							ML				18
19											19
20											20
21	5	90	4,10	0.2	SS	SS	SW	SAND, LITTLE SILT, BROWN, MEDIUM COARSE			21
22			19,15			20-22'	GM	GRAVEL, SAND AND SILT, WET			22
23											23
24							LMSN	LIMESTONE, WEATHERED, GRAY			24
25								END OF BORING AT 24 FEET			25
26											26

HSA = HOLLOW STEM AUGER
 CAL = CALIBRATION
 USCS = UNIFIED SOIL CLASS. SYS.

SS = SPLIT SPOON
 A = AUGER CUTTINGS
 * = LAB SAMPLE

BH = BORE HOLE
 GS = GRAB SAMPLE
 HS = HEADSPACE
 W = WATER LEVEL

COMMENTS:
 4 INCH DIAMETER BORING
 GROUTED TO SURFACE

CONTRACTOR: CT & E

GEOLOGIST: BACHOVCHIN/GLENNIE

DRILLING METHOD: HSA

DTW FROM TOC: NA

DATE/TIME: NA

PARSONS

ENGINEERING-SCIENCE, INC.

DRILLING RECORD

BORING NO: 54SB8

LOCATION: SWMU 54
EAST OF LOWER MOUND

WEATHER: WARM, 50' F

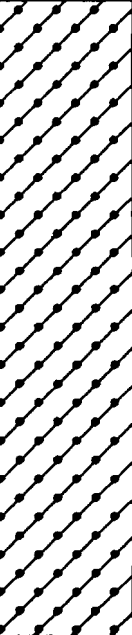
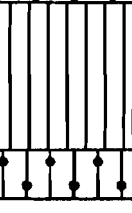
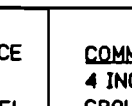
DATE/TIME START: 12/22/94 1320

DATE/TIME FINISH: 12/22/94 1355

PROJECT NAME: RAAP

CLIENT: US AEC

PROJECT NO.: 722843

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
1	1*	60	2,2	9.0	HS	SS	ML	SILT, SOME CLAY, DARK BROWN		SURFACE ELEVATION 1699.4' (MSL)	1
2			3,3			0-2'					2
3											3
4											4
5							SM	SILT AND SAND, LITTLE CLAY, BROWN, MOIST, MORE SAND WITH DEPTH			5
6	2	90	5,5	2.1	HS	SS					6
7			4,2			5-7'					7
8											8
9											9
10											10
11	3	90	1,2	4.8	HS	SS	GM				11
12			2,2			10-12'					12
13											13
14											14
15											15
16	4*	100	6,5	5.9	SS	SS					16
17			6,5			15-17'					17
18							ML	SILT AND CLAY, DARK BROWN, MOIST			18
19											19
20							GM				20
21	5	50	15,11	2.5	SS	SS					21
22			11, 50/2			20-22'					22
23								END OF BORING AT 22 FEET			23
24											24
25											25
26											26

HSA = HOLLOW STEM AUGER

CAL = CALIBRATION

USCS = UNIFIED SOIL CLASS. SYS.

SS = SPLIT SPOON

A = AUGER CUTTINGS

* = LAB SAMPLE

BH = BORE HOLE

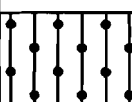
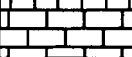
GS = GRAB SAMPLE

g = WATER LEVEL

COMMENTS:

4 INCH DIAMETER BORING GROUTED TO SURFACE

CONTRACTOR: <u>CT & E</u> GEOLOGIST: <u>BACHOVCHIN/GLENNIE</u> DRILLING METHOD: <u>HSA</u> DTW FROM TOC: <u>NA</u> DATE/TIME: <u>NA</u>	PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO: <u>54SB9</u> LOCATION: <u>SWMU 54</u> <u>NORTH OF LOWER MOUND</u> WEATHER: <u>COLD, 30° F</u> DATE/TIME START: <u>12/21/94 1235</u> DATE/TIME FINISH: <u>12/21/94 1305</u>
	PROJECT NAME: <u>RAAP</u> CLIENT: <u>US AEC</u> PROJECT NO.: <u>722843</u>	

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
1	1	90	3,4	4.2	SS	SS 0-2'	ML	SILT AND CLAY, SOME SAND, BLACK-BROWN (ASH?)		SURFACE ELEVATION 1697.9' (MSL) 	1
2			6,5								2
3											3
4											4
5											5
6	2*	85	2,3	48.0	HS	SS 5-7'					6
7			4,4								7
8											8
9											9
10											10
11	3	50	1,2	0.0	HS	SS 10-12'					11
12			2,4								12
13											13
14											14
15											15
16	4*	90	2,3	0.0	HS	SS 15-17'					16
17			3,3				SW	SAND, BROWN, MEDIUM COARSE			17
18							GM	GRAVEL, SILT, WET			18
19											19
20	5	10	50/2	0.0	HS	SS 20-21'	LMSN	LIMESTONE, WEATHERED, GREEN-GRAY			20
21								END OF BORING AT 21 FEET			21
22											22
23											23
24											24
25											25
26											26

HSA = HOLLOW STEM AUGER
 CAL = CALIBRATION
 USCS = UNIFIED SOIL CLASS. SYS.

SS = SPLIT SPOON BH = BORE HOLE HS = HEADSPACE
 A = AUGER CUTTINGS GS = GRAB SAMPLE
 * = LAB SAMPLE ¶ = WATER LEVEL

COMMENTS:
 4 INCH DIAMETER BORING
 GROUTED TO SURFACE

CONTRACTOR: CT & E	PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO.: 54SB10
GEOLOGIST: BACHOVCHIN/GLENNIE		LOCATION: SWMU 54 WEST OF UPPER MOUND
DRILLING METHOD: HSA		WEATHER: COLD, 30° F
DTW FROM TOC: NA		DATE/TIME START: 12/21/94 1310
DATE/TIME: NA	PROJECT NAME: RAAP	DATE/TIME FINISH: 12/21/94 1340
	CLIENT: US AEC	
	PROJECT NO.: 722843	

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
1	1	50	2,4 6,8	0.0	HS	SS 0-2'	ML	SILT, SOME CLAY, DARK-BROWN		SURFACE ELEVATION 1696.6' (MSL)	1
2											2
3											3
4											4
5											5
6	2*	90	6,7 7,6	0.0	HS	SS 5-7'	SM				6
7											7
8											8
9											9
10											10
11	3	75	2,6 7,9	0.2	HS	SS 10-12'	SM	SAND, LITTLE SILT, BROWN			11
12											12
13											13
14											14
15											15
16	4*	75	2,3 6,13	0.0	HS	SS 15-17'	GM				16
17											17
18											18
19											19
20											20
21							LMSN				21
22											22
23											23
24											24
25											25
26											26
								GRAVEL, SILT			
								LIMESTONE, WEATHERED, GRAY, WET			
								END OF BORING AT 19 FEET			

HSA = HOLLOW STEM AUGER CAL = CALIBRATION USCS = UNIFIED SOIL CLASS. SYS.	SS = SPLIT SPOON A = AUGER CUTTINGS * = LAB SAMPLE	BH = BORE HOLE GS = GRAB SAMPLE ♀ = WATER LEVEL	HS = HEADSPACE COMMENTS: 4 INCH DIAMETER BORING GROUTED TO SURFACE
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CONTRACTOR: <u>CT & E</u> GEOLOGIST: <u>BACHOVCHIN/GLENNIE</u> DRILLING METHOD: <u>HSA</u> DTW FROM TOC: <u>NA</u> DATE/TIME: <u>NA</u>	PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO: <u>54SB11</u> LOCATION: <u>SWMU 54</u> <u>WEST OF UPPER MOUND</u> WEATHER: <u>COLD, 35° F</u> DATE/TIME START: <u>12/21/94 1350</u> DATE/TIME FINISH: <u>12/21/94 1418</u>
	PROJECT NAME: <u>RAAP</u> CLIENT: <u>US AEC</u> PROJECT NO.: <u>722843</u>	

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)		
1	1*	70	2,2 3,2	2.8	HS	SS 0-2'	ML	SILT, SOME CLAY, LITTLE SAND, DARK-BROWN		SURFACE ELEVATION 1897.3' (MSL) 	1		
2													2
3	2	90	2,4 5,4	0.0	HS	SS 2-4'							3
4													4
5							SM	</					

HSA = HOLLOW STEM AUGER CAL = CALIBRATION USCS = UNIFIED SOIL CLASS. SYS.	SS = SPLIT SPOON A = AUGER CUTTINGS * = LAB SAMPLE	BH = BORE HOLE GS = GRAB SAMPLE HS = HEADSPACE v = WATER LEVEL	COMMENTS: 4 INCH DIAMETER BORING GROUTED TO SURFACE
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CONTRACTOR: CT & E	PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO.: 54SB12
GEOLOGIST: BACHOVCHIN/GLENNIE		LOCATION: SWMU 54 NORTHWEST OF UPPER MOUND
DRILLING METHOD: HSA		WEATHER: COLD, 35° F
DTW FROM TOC: NA		DATE/TIME START: 12/21/94 1500
DATE/TIME: NA	PROJECT NAME: RAAP	DATE/TIME FINISH: 12/21/94 1540
	CLIENT: US AEC	
	PROJECT NO.: 722843	

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
1	1*	90	2.2	2.8	HS	SS 0-2'	ML	SILT AND CLAY, DARK-BROWN		SURFACE ELEVATION 1698.8' (MSL)	1
2			3.2								2
3	2	100	3.5	1.7	HS	SS 2-4'					3
4			7.6								4
5											5
6	3	90	3.6	0.8	HS	SS 5-7'	CL/ML	CLAY AND SILT, DARK BROWN, MOIST AT 16 FEET			6
7			5.5								7
8											8
9											9
10											10
11	4	95	2.2	0.8	HS	SS 10-12'					11
12			2.2								12
13											13
14											14
15											15
16	5*	90	2.3	0.0	HS	SS 15-17'	SM	SAND AND SILT, LIGHT BROWN			16
17			3.5								17
18							GM	GRAVEL OVER LIMESTONE, WET			18
19											19
20	6	10	100/6	0.0	HS	SS 18-19'		AUGER REFUSAL AT 18 FEET			20
21											21
22											22
23											23
24											24
25											25
26											26

HSA = HOLLOW STEM AUGER
CAL = CALIBRATION
USCS = UNIFIED SOIL CLASS. SYS.

SS = SPLIT SPOON
A = AUGER CUTTINGS
* = LAB SAMPLE

BH = BORE HOLE
GS = GRAB SAMPLE

HS = HEADSPACE
g = WATER LEVEL

COMMENTS:
4 INCH DIAMETER BORING
GROUTED TO SURFACE

CONTRACTOR: CT & E	PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO: 54SB13
GEOLOGIST: BACHOVCHIN/GLENNIE		LOCATION: SWMU 54 EAST OF UPPER MOUND
DRILLING METHOD: HSA		WEATHER: COLD, 35° F
DTW FROM TOC: NA		DATE/TIME START: 12/21/94 1550
DATE/TIME: NA		DATE/TIME FINISH: 12/21/94 1845
PROJECT NAME: RAAP CLIENT: US AEC PROJECT NO.: 722843		

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	F'D (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
1	1*	85	2,2	0.0	HS	SS 0-2'	ML	SILT, SOME CLAY, LITTLE SAND, DARK-BROWN		SURFACE ELEVATION 1700.0' (MSL) 	1
2			2,3								2
3	2	80	2,4	0.0	HS	SS 2-4'					3
4			4,3								4
5											5
6	3	90	4,6	0.0	HS	SS 5-7'	SM	SILT AND SAND, LITTLE CLAY, BROWN			6
7			7,6								7
8											8
9											9
10											10
11	4	90	1,1	0.0	HS	SS 10-12'	CL/ML	SILT AND CLAY, LITTLE SAND, DARK BROWN			11
12			1,1								12
13											13
14											14
15											15
16	5	85	2,5	0.0	HS	SS 15-17'	ML	SILT, SOME CLAY AND SAND, BROWN			16
17			5,4								17
18											18
19											19
20											20
21	6*	80	2,2	0.0	HS	SS 20-22'	SM	SAND AND SILT, BROWN, MOIST			21
22			13,8								22
23	7	50	19,13	0.0	HS	SS 22-24'	GM	GRAVEL, WET			23
24			52/2				LMSN	LIMESTONE, WEATHERED, GREEN-GRAY			24
25								END OF BORING AT 24 FEET			25
26											26

HSA = HOLLOW STEM AUGER
 CAL = CALIBRATION
 USCS = UNIFIED SOIL CLASS. SYS.

SS = SPLIT SPOON
 A = AUGER CUTTINGS
 * = LAB SAMPLE

BH = BORE HOLE
 GS = GRAB SAMPLE
 HS = HEADSPACE
 ▽ = WATER LEVEL

COMMENTS:
 4 INCH DIAMETER BORING
 GROUTED TO SURFACE

CONTRACTOR: CT & E	PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO: 54SB14
GEOLOGIST: BACHOVCHIN/GLENNIE		LOCATION: SWMU 54 NORTHEAST OF UPPER MOUND
DRILLING METHOD: HSA		WEATHER: WARM, 40° F
DTW FROM TOC: NA		DATE/TIME START: 12/22/94 0830
DATE/TIME: NA	PROJECT NAME: RAAP	DATE/TIME FINISH: 12/22/94 0910
	CLIENT: US AEC	
	PROJECT NO.: 722843	

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PTD (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
1								SILT, SOME SAND, LITTLE CLAY, DARK-BROWN		SURFACE ELEVATION 1699.6' (MSL)	1
2											2
3	1*	55	NA	1.7	HS	MOSS SPOON 0-5'	ML				3
4											4
5								SAND AND SILT, LITTLE CLAY, BROWN			5
6											6
7											7
8	2	95	NA	6.0	HS	MOSS SPOON 5-10'	SM				8
9											9
10											10
11											11
12											12
13	3*	75	NA	5.6	HS	MOSS SPOON 10-15'					13
14											14
15											15
16											16
17											17
18	4	5	NA	1.4	HS	MOSS SPOON 15-20'					18
19											19
20											20
21							GM	GRAVEL OVER LIMESTONE, WET			21
22								AUGER REFUSAL AT 21 FEET			22
23											23
24											24
25											25
26											26

HSA = HOLLOW STEM AUGER
 CAL = CALIBRATION
 USCS = UNIFIED SOIL CLASS. SYS.

SS = SPLIT SPOON
 A = AUGER CUTTINGS
 * = LAB SAMPLE

BH = BORE HOLE
 GS = GRAB SAMPLE
 HS = HEADSPACE
 ♡ = WATER LEVEL

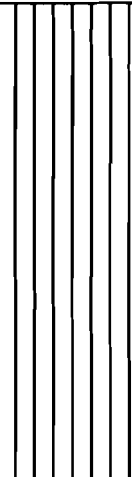
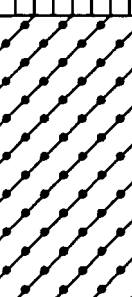
COMMENTS:
 4 INCH DIAMETER BORING
 GROUTED TO SURFACE

CONTRACTOR: CT & E	PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD	BORING NO: 54SB15
GEOLOGIST: BACHOVCHIN/GLENNIE		LOCATION: SWMU 54 CENTER OF UPPER MOUND
DRILLING METHOD: HAND AUGERED		WEATHER: WARM, 40° F
DTW FROM TOC: NA		DATE/TIME START: 12/22/94 1100
DATE/TIME: NA	PROJECT NAME: RAAP	DATE/TIME FINISH: 12/22/94 1130
	CLIENT: US AEC	
	PROJECT NO.: 722843	

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)
1							ML	SILT, LITTLE CLAY, BROWN		SURFACE ELEVATION 1704.5' (MSL)	1
2											2
3											3
4							ASH	ASH, GLASSY BLACK, AND BROWN SILT			4
5											5
6							ML	SILT, LITTLE CLAY, BROWN			6
7											7
8											8
9								END OF BORING AT 8 FEET			9
10								* 4-6 FEET INTERVAL SUBMITTED TO LAB			10
11											11
12											12
13											13
14								NOTE: NO PID READINGS ABOVE BACKGROUND RECORDED			14
15											15
16											16
17											17
18											18
19											19
20											20
21											21
22											22
23											23
24											24
25											25
26											26

HSA = HOLLOW STEM AUGER CAL = CALIBRATION USCS = UNIFIED SOIL CLASS. SYS.	SS = SPLIT SPOON A = AUGER CUTTINGS * = LAB SAMPLE	BH = BORE HOLE GS = GRAB SAMPLE ∇ = WATER LEVEL	HS = HEADSPACE COMMENTS: HAND AUGERED GROUTED TO SURFACE
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CONTRACTOR: <u>CT & E</u> GEOLOGIST: <u>BACHOVCHIN/GLENNIE</u> DRILLING METHOD: <u>HSA</u> DTW FROM TOC: <u>NA</u> DATE/TIME: <u>NA</u>			PARSONS ENGINEERING-SCIENCE, INC. DRILLING RECORD				BORING NO: <u>54SB16</u> LOCATION: <u>SWMU 54</u> <u>N. OF UPPER MOUND (BACKGROUND)</u> WEATHER: <u>WARM, 45° F</u> DATE/TIME START: <u>12/22/94 0940</u> DATE/TIME FINISH: <u>12/22/94 1005</u>				
			PROJECT NAME: <u>RAAP</u>			CLIENT: <u>US AEC</u>			PROJECT NO.: <u>722843</u>		

DEPTH (FT)	SAMPLE ID	RECOVERY %	BLOW COUNT	PID (ppm)	READING AT	SAMPLE TYPE	USCS	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FT)			
1	1*	90	2,2	27.1	HS	SS	ML	SILT, SOME CLAY, LITTLE SAND, DARK-BROWN		SURFACE ELEVATION 1697.0' (MSL)	1			
2			2,3											2
3														3
4														4
5														5
6	2	80	3,3	7.4	SS	SS					6			
7			4,6			5-7'								7
8														8
9														9
10														10
11	3*	80	4,6	15.9	HS	SS	SM	SAND AND SILT, LITTLE CLAY, MEDIUM BROWN			11			
12			7,6			10-12'								12
13														13
14														14
15														15
16	4	90	1,1	2.8	SS	SS	ML	SILT AND CLAY, DARK BROWN			16			
17			2,4			15-17'							17	
18								GM			GRAVEL, SOME SILT, WET		18	
19											AUGER REFUSAL AT 18 FEET		19	
20											20			
21											21			
22											22			
23											23			
24											24			
25											25			
26											26			

HSA = HOLLOW STEM AUGER CAL = CALIBRATION USCS = UNIFIED SOIL CLASS. SYS.	SS = SPLIT SPOON A = AUGER CUTTINGS * = LAB SAMPLE	BH = BORE HOLE GS = GRAB SAMPLE g = WATER LEVEL
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COMMENTS:
 4 INCH DIAMETER BORING
 GROUTED TO SURFACE

DRILLING CONTRACTOR: CT & E

DRILLER: DAVE DOLAN

GEOLOGIST: S. GLENNIE

RIG TYPE: BB0/92

DRILLING METHOD: HSA

ENGINEERING-SCIENCE DRILLING RECORD

BORING NO. BG1 UC

SHEET 1 OF 1

LOCATION: FIRE TRAIL
#5W4A - NEAR ROAD

BORING SITE DESCRIPTION

WATER LEVEL MEASUREMENTS

MP			
DTW FROM MP	<u>N/A</u>		
TIME			
DATE			

WEATHER Warm - Humid ~78°F

DATE/TIME START 7-19-95 / 1700

DATE/TIME FINISH 7-19-95 / 1710

DEPTH (FEET)	SAMPLE NUMBER	RECOVERY %	BLOW COUNTS	PTD READING	READING AT	USCS	SAMPLE TYPE	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FEET)
1			17, 9					Light Grey Dry Sand (1-2'). Lite Brown Sand with Clay (2-3')			1
2	18	100	11, 12	0.0	SS	SM	SS				2
3			14, 16, 20, 19					Light Brown Silt with Clay			3
4	N/A	75		0.0	SS	ML	SS				4
5								Light Brown Compact Clay, minor black oxides			5
6											6
7	1C	25		0.0	SS	CH	SS				7
8								E.O.B AT 8 Ft.			8
9											9
10											10
11											11
12											12
13											13
14											14
15											15
16											16
17											17
18											18
19											19
20								20			

LEGEND:

SAND & GRAVEL	CLAY	SILT & CLAY	SAND	SAND & SILT
SILT	BEDROCK	GRAVEL	SAPROLITE	WATER LEVEL

SPT = STANDARD PENETRATION TEST CAL = CALIBRATION BZ = BREATHING ZONE
 SS = SPLIT SPOON A = AUGER CUTTINGS C = CORE BH = BOREHOLE GS = GRAB SAMPLE

COMMENTS:

DRILLING CONTRACTOR: <u>CT & E</u> DRILLER: <u>DAVE DOLAN</u> GEOLOGIST: <u>S. GLENNIE</u> RIG TYPE: <u>BB0/92</u> DRILLING METHOD: <u>HSA</u>		ENGINEERING-SCIENCE DRILLING RECORD		BORING NO. <u>BG2 UC</u> SHEET <u>1</u> OF <u>1</u> LOCATION: <u>FIRE TRAIL</u> <u>*SW 4A - NEAR ROAD</u> BORING SITE DESCRIPTION <u>N 10' North of</u> <u>BG 1</u> <u>UNISON URBAN LAND</u> <u>COMPLEX</u>	
WATER LEVEL MEASUREMENTS MP _____ DTW _____ FROM MP <u>N/A</u> TIME _____ DATE _____		PROJECT NAME <u>RAAP</u> CLIENT <u>US AEC</u> PROJECT NO. <u>722B43</u> WEATHER <u>Warm Humid ~ 78°F</u> DATE/TIME START <u>7-19-95 / 1628</u> DATE/TIME FINISH <u>7-19-95 / 1650</u>			

DEPTH (FEET)	SAMPLE NUMBER	RECOVERY %	BLOW COUNTS	PIT READING	READING AT	USCS	SAMPLE TYPE	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FEET)
1											1
2	N/A	5	9,10 9,9	0.0	SS	SM	SS	Light Brown Silty Sand			2
3											3
4	2B	25	19,11 15,20	0.0	SS	CL	SS	Light Brown Silty with Clay			4
5											5
6	N/A	10	14,17 19,21	0.0	SS	CL	SS	Brown-red Clay, minor silt			6
7											7
8	N/A	100	21,15 19,21	0.0	SS	SM	SS	Light Brown Sand with silt, minor clay			8
9											9
10	2C	50	17,16 14,16	0.0	SS	CL	SS	Brown dense clay to sandy clay			10
11								E.O.B. @ 11 Ft			11
12											12
13											13
14											14
15											15
16											16
17											17
18											18
19											19
20											20

LEGEND:

SAND & GRAVEL	CLAY	SILT & CLAY	SAND	SAND & SILT
SILT	BEDROCK	GRAVEL	SAPROLITE	WATER LEVEL

SPT = STANDARD PENETRATION TEST CAL = CALIBRATION BT = BREATHING ZONE
 SS = SPLIT SPOON A = AUGER CUTTINGS C = CORED BS = BOREHOLE GS = GRAB SAMPLE

COMMENTS:

DRILLING CONTRACTOR: <u>CT & E</u>		ENGINEERING-SCIENCE DRILLING RECORD	BORING NO. <u>BG3UC</u>	
DRILLER: <u>DAVE DOLAN</u>			SHEET <u>1</u> OF <u>1</u>	
GEOLOGIST: <u>S. GLENNIE</u>			LOCATION: <u>EAST REGION OF</u> <u>MAIN MFG. AREA.</u>	
BIC TYPE: <u>BB0/92</u>			BORING SITE DESCRIPTION	
DRILLING METHOD: <u>HSA</u>		PROJECT NAME <u>RAAP</u>	SOIL TYPE:	
		CLIENT <u>US AEC</u>	<u>UNISON URBAN LAND</u> <u>COMPLEX</u>	
		PROJECT NO. <u>722B43</u>		
WATER LEVEL MEASUREMENTS		WEATHER <u>90°F - HUMID</u>		
MP				
DTW FROM MP	<u>N/A</u>			
TIME		DATE/TIME START <u>7-20-95 / 1610</u>		
DATE		DATE/TIME FINISH <u>7-20-95 / 1627</u>		

DEPTH (FEET)	SAMPLE NUMBER	RECOVERY %	BLOW COUNTS	PTD READING	READING AT	USCS	SAMPLE TYPE	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FEET)
1											1
2	38	75	6,6, 8,12	0.0	SS	CL	SS	DARK-RED SILT, SOME CLAY, MINOR SAND			2
3											3
4											4
5											5
6											6
7											7
8											8
9											9
10											10
11											11
12											12
13											13
14											14
15											15
16											16
17											17
18											18
19											19
20											20
21	30	3C	14,8, 14,38	0.0	SS	SM	SS	BROWN MED. GRAINED SAND, WITH MICACEOUS SILT.			21
22								C.O.B. @ 22 FT.			22

LEGEND:		SAND & GRAVEL	CLAY	SILT & CLAY	SAND	SAND & SILT
		SILT	BEDROCK	GRAVEL	SAPROLITE	WATER LEVEL
SPT = STANDARD PENETRATION TEST CAL = CALIBRATION BZ = BELLHOLE ZONE SS = SPLIT SPOON A = AUGER CUTTINGS C = CORED BB = BORED HOLE GS = GRAB SAMPLE						
COMMENTS:						

DRILLING CONTRACTOR: <u>CT & E</u> DRILLER: <u>DAVE DOLAN</u> GEOLOGIST: <u>S. GLENNIE</u> RIG TYPE: <u>BB0/92</u> DRILLING METHOD: <u>HSA</u>	ENGINEERING-SCIENCE DRILLING RECORD	BORING NO. <u>BG4UC</u> SHEET <u>1</u> OF <u>1</u> LOCATION: <u>EAST REGION OF</u> <u>MAIN MFG. AREA.</u> BORING SITE DESCRIPTION SOIL TYPE: <u>UNION URBAN LAND</u> <u>COMPLEX</u>
PROJECT NAME <u>RAAP</u> CLIENT <u>US AEC</u> PROJECT NO. <u>722843</u> WEATHER <u>90°F - HUMID</u> DATE/TIME START <u>7-20-95 / 1550</u> DATE/TIME FINISH <u>7-20-95 / 1600</u>		

DEPTH (FEET)	SAMPLE NUMBER	RECOVERY %	BLOW COUNTS	PID READING	READING AT	USCS	SAMPLE TYPE	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FEET)
1											1
2											2
3											3
4	4B	75	10,9, 10,8	0.0	SS	MH	SS	SANDY SILT, WITH CLAY MINOR GRAVEL (2-3mm). HEAVY MOTTLING. FILL?			4
5											5
6											6
7											7
8											8
9											9
10											10
11											11
12											12
13											13
14											14
15								BROWN MICACEOUS SILT, MINOR CLAY. SOME RED SHALE PIECES.			15
16	4C	50	8,6, 7,10	0.0	SS	ML	SS				16
17								E.O.B. @ 17 Ft.			17
18											18
19											19
20											20

LEGEND: SAND & GRAVEL SILT CLAY BEDROCK SILT & CLAY GRAVEL SAND SAPROLITE SAND & SILT WATER LEVEL	SPT = STANDARD PENETRATION TEST CAL = CALIBRATION BZ = BULWYING ZONE SS = SPLIT SPOON A = AUGER CUTTINGS C = COAL BH = BOREHOLE GS = GRAB SAMPLE
COMMENTS:	

DRILLING CONTRACTOR: <u>CT & E</u>			ENGINEERING-SCIENCE DRILLING RECORD			BORING NO. <u>BG7 UC</u>					
DRILLER: <u>DAVE DOLAN</u>						SHEET <u>1</u> OF <u>1</u>					
GEOLOGIST: <u>S. GLENNIE</u>			PROJECT NAME <u>RAAP</u>			LOCATION: <u>NW REGION of</u>					
RIG TYPE: <u>BBO/92</u>			CLIENT <u>US AEC</u>			<u>RAAP</u>					
DRILLING METHOD: <u>HSA</u>			PROJECT NO. <u>722843</u>			BORING SITE DESCRIPTION					
WATER LEVEL MEASUREMENTS			WEATHER			40' EAST of					
MP						BG 6					
DTW FROM MP <u>N/A</u>						Soil: UNISON URBAN LAND					
TIME			DATE/TIME START <u>7-19-95 / 1836</u>			COMPLEX					
DATE			DATE/TIME FINISH <u>7-19-95 / 1905</u>								
DEPTH (FEET)	SAMPLE NUMBER	RECOVERY %	BLOW COUNTS	PTD READING	READING AT	USCS	SAMPLE TYPE	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FEET)
1											1
2	N/A	0%						No Recovery From a split spoons			2
3											3
4	7B	75	5.5, 6.6	0.0	SS	CH	SS	Light BROWN CLAY, Some RED STREAKS, Approx 15% OXIDES MOIST			4
5											5
6											6
7											7
8											8
9											9
10											10
11											11
12											12
13											13
14											14
15											15
16											16
17											17
18											18
19											19
20	7C	25	8.4, 100/5"	0.0	SS	CH	SS	BROWN CLAY WITH MINOR OXIDE STAINING. LIMESTONE at 21.5 Feet			20
21								E.O.B @ 21.5 Ft			21

LEGEND: SAND & GRAVEL CLAY SILT & CLAY SAND SAND & SILT
 SILT BEDROCK GRAVEL SAPROLITE WATER LEVEL

SPT = STANDARD PENETRATION TEST CAL = CALIBRATION BZ = BREATHER ZONE
SS = SPLIT SPOON A = AUGER CUTTINGS C = CORED BH = BORED HOLE GS = GRAB SAMPLE

COMMENTS:

DRILLING CONTRACTOR: <u>CT & E</u> DRILLER: <u>DAVE DOLAN</u> GEOLOGIST: <u>S. GLENNIE</u> RIG TYPE: <u>BB0/92</u> DRILLING METHOD: <u>HSA</u>		ENGINEERING-SCIENCE DRILLING RECORD		BORING NO. <u>BGBUC</u> SHEET <u>1</u> OF <u>1</u> LOCATION: <u>NW CORNER of RAAP</u> BORING SITE DESCRIPTION <u>45' West of end of NW portion of GRAVEL ROAD</u> SWL: <u>UNISON URBAN LAND COMPLEX</u>	
PROJECT NAME <u>RAAP</u> CLIENT <u>US AEC</u> PROJECT NO. <u>722843</u>		WEATHER <u>WARM ~75°F</u> DATE/TIME START <u>7-19-95 / 195</u> DATE/TIME FINISH <u>7-19-95 / 1930</u>			
WATER LEVEL MEASUREMENTS MP _____ DTW FROM MP <u>N/A</u> TIME _____ DATE _____					

DEPTH (FEET)	SAMPLE NUMBER	RECOVERY %	BLOW COUNTS	PTD READING	READING AT	USCS	SAMPLE TYPE	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FEET)
1											1
2	N/A		9.7, 10, 10	0.0	SS	ML	SS	RED-BROWN SILT WITH CLAY; MUCOUS - DAMP			2
3											3
4	3B	100	12, 12, 12, 14	0.0	SS	SM/SC	SS	RED BROWN SAND AND SILT AND CLAY, SOME OXIDE STAINING			4
5											5
6											6
7											7
8											8
9	BC	75	15, 18, 7, 5	0.0	SS	GM	SS	BROWN SAND WITH MINOR CLAY AND GRAVEL			9
10											10
11								E.O.B. @ 10 Ft			11
12											12
13											13
14											14
15											15
16											16
17											17
18											18
19											19
20											20

LEGEND:
 SAND & GRAVEL
 CLAY
 SILT & CLAY
 SAND
 SAND & SILT
 SILT
 BEDROCK
 GRAVEL
 SAPROLITE
 WATER LEVEL

SPT = STANDARD PENETRATION TEST CAL = CALIBRATION SZ = SEALING ZONE
 BS = SPLIT SPOON A = AUGER CUTTINGS C = COLED BH = BOREHOLE GS = GRAB SAMPLE

COMMENTS:

DRILLING CONTRACTOR: <u>CT & E</u> DRILLER: <u>DAVE DOLAN</u> GEOLOGIST: <u>S. GLENNIE</u> RIG TYPE: <u>B80/92</u> DRILLING METHOD: <u>HSA</u>		ENGINEERING-SCIENCE DRILLING RECORD		BORING NO. <u>BG1WL</u> SHEET <u>1</u> OF <u>1</u> LOCATION: <u>NE REGION of RAAP</u> BORING SITE DESCRIPTION <u>SOIL TYPE:</u> <u>WHEELING SANDY LOAM.</u>	
WATER LEVEL MEASUREMENTS MP _____ DTW _____ FROM MP <u>N/A</u> TIME _____ DATE _____		PROJECT NAME <u>RAAP</u> CLIENT <u>US AEC</u> PROJECT NO. <u>722B43</u> WEATHER <u>WARM, HUMID ~80F</u> DATE/TIME START <u>7-20-95 / 0930</u> DATE/TIME FINISH <u>7-20-95 / 0940</u>			

DEPTH (FEET)	SAMPLE NUMBER	RECOVERY %	BLOW COUNTS	PTD READING	READING AT	USCS	SAMPLE TYPE	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FEET)
1											1
2	N/A	25	4,4 5,4	0.0	SS	SC	SS	BROWN SAND, WITH CLAY, SOME GRAVEL. RED STREAKS AND BLACK OXIDE STAINING.			2
3											3
4	1B	50	3,3 4,3	0.0	SS	CL	SS	BROWN CLAY WITH SAND.			4
5											5
6	1C	50	1,2 4,6	0.0	SS	CL	SS	BROWN SAND AND CLAY.			6
7											7
8	N/A	100	4,8 10,11	0.0	SS	CL	SS	(7-8'): BROWN SAND, SAME CLAY (8-9'): BROWN CLAY W/SAND			8
9								E.O.B. @ 9 Ft.			9
10											10
11											11
12											12
13											13
14											14
15											15
16											16
17											17
18											18
19											19
20											20

LEGEND:

SAND & GRAVEL	CLAY	SILT & CLAY	SAND	SAND & SILT
SILT	BEDROCK	GRAVEL	SAPROLITE	WATER LEVEL

SPT = STANDARD PENETRATION TEST CAL = CALIBRATION BZ = BREATHING ZONE
 SS = SPLIT SPOON A = AUGER CUTTINGS C = COLED BH = BOREHOLE GS = GRAB SAMPLE

COMMENTS:

DRILLING CONTRACTOR: CT & E DRILLER: DAVE DOLAN GEOLOGIST: S. GLENNIE RIG TYPE: BB0/92 DRILLING METHOD: HSA	ENGINEERING-SCIENCE DRILLING RECORD	BORING NO. BG2 WL SHEET 1 OF 1 LOCATION: NE REGION OF RAAP BORING SITE DESCRIPTION SOIL TYPE: WHEELING SANDY LOAM
PROJECT NAME RAAP CLIENT US AEC PROJECT NO. 722B43		
WATER LEVEL MEASUREMENTS MP _____ DTW FROM MP N/A TIME _____ DATE _____		WEATHER WARM, HUMID ~80°F DATE/TIME START 7-20-95 / 0940 DATE/TIME FINISH 7-20-95 / 0954

DEPTH (FEET)	SAMPLE NUMBER	RECOVERY %	BLOW COUNTS	PTD READING	READING AT	USCS	SAMPLE TYPE	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FEET)	
1			10, 2,					FILL MATERIAL: GRAVEL AND DARK GREY CLAY			1	
2	N/A	25	2, 3	0.0	SS	GC	SS				2	
3			3, 2,					BROWN CLAY AND SAND, MINOR BLACK OXIDE STAINING.				3
4	ZB	50	5, 5	0.0	SS	SC	SS				4	
5			1, 4,					BROWN CLAY, MINOR SAND				5
6	N/A	100	7, 7	0.0	SS	CL	SS				6	
7			5, 10					BROWN SAND AND SILT AND CLAY				7
8	N/A	100	9, 11	0.0	SS	SC- SM	SS				8	
9			10, 10					MIXED BROWN + GREY CLAY				9
10	N/A	50		0.0	SS	CH	SS				10	
11	2C	100	15, 14 12, 17	0.0	SS	CL	SS	RED-BROWN SAND SOME CLAY (10-11'): ALL SAND (11-12').				11
12								E.O.B. @ 12 Ft.				12
13									13			
14									14			
15									15			
16									16			
17									17			
18									18			
19									19			
20									20			

LEGEND:

SAND & GRAVEL	CLAY	SILT & CLAY	SAND	SAND & SILT
SILT	BEDROCK	GRAVEL	SAPROLITE	WATER LEVEL

SPT = STANDARD PENETRATION TEST CAL = CALIBRATION SZ = BREATHING ZONE
 SS = SPLIT SPOON A = AUGER CUTTINGS C = CORED BS = BOREHOLE GS = GRAB SAMPLE

COMMENTS:

DRILLING CONTRACTOR: <u>CT & E</u> DRILLER: <u>DAVE DOLAN</u> GEOLOGIST: <u>S. GLENNIE</u> RIG TYPE: <u>BBO/92</u> DRILLING METHOD: <u>HSA</u>	ENGINEERING-SCIENCE DRILLING RECORD	BORING NO. <u>BG3 WL</u> SHEET <u>1</u> OF <u>2</u> LOCATION: <u>NE CORNER</u> <u>AREA OF RAAP</u> BORING SITE DESCRIPTION SOIL TYPE: <u>WHEELING SANDY LOAM</u>																
PROJECT NAME <u>RAAP</u> CLIENT <u>US AEC</u> PROJECT NO. <u>722843</u> WEATHER <u>80F, Humid</u> DATE/TIME START <u>7-20-95 / 1005</u> DATE/TIME FINISH <u>7-20-95 / 1037</u>																		
WATER LEVEL MEASUREMENTS <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td>MP</td> <td></td> <td></td> <td></td> </tr> <tr> <td>DTW FROM MP</td> <td><u>N/A</u></td> <td></td> <td></td> </tr> <tr> <td>TIME</td> <td></td> <td></td> <td></td> </tr> <tr> <td>DATE</td> <td></td> <td></td> <td></td> </tr> </table>		MP				DTW FROM MP	<u>N/A</u>			TIME				DATE				
MP																		
DTW FROM MP	<u>N/A</u>																	
TIME																		
DATE																		

DEPTH (FEET)	SAMPLE NUMBER	RECOVERY %	BLOW COUNTS	PTD READING	READING AT	USCS	SAMPLE TYPE	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FEET)
1								BROWN SILT WITH SAND, MINOR CLAY  AIR DRILLING TO 20 FEET			1
2	38	25	2,4 5,2	0.0	SS	SM	SS				2
3											3
4											4
5											5
6											6
7											7
8											8
9											9
10											10
11											11
12											12
13											13
14											14
15											15
16											16
17											17
18											18
19											19
20	3C	75	9,8, 8,7	0.0	SS		SS	SEE FOLLOWING PAGE			20

LEGEND:
  SAND & GRAVEL
  CLAY
  SILT & CLAY
  SAND
  SAND & SILT
 SILT
  BEDROCK
  GRAVEL
  SAPROLITE
  WATER LEVEL

SPT = STANDARD PENETRATION TEST CAL = CALIBRATION BZ = BREATHER ZONE
 SS = SPLIT SPOON A = AUGER CUTTINGS C = CORED BH = BOREHOLE GS = GRAB SAMPLE

COMMENTS:

DRILLING CONTRACTOR: <u>CT & E</u>		ENGINEERING-SCIENCE DRILLING RECORD		BORING NO. <u>BG3WL</u>							
DRILLER: <u>DAVE DOLAN</u>		PROJECT NAME <u>RAAP</u> CLIENT <u>US AEC</u> PROJECT NO. <u>722843</u> WEATHER <u>80°F, Humid</u> DATE/TIME START <u>7-20-95 / 1005</u> DATE/TIME FINISH <u>7-20-95 / 1037</u>		SHEET <u>2</u> OF <u>2</u>							
GEOLOGIST: <u>S. GLENNIE</u>				LOCATION: <u>NE REGION</u> <u>of RAAP</u>							
RIG TYPE: <u>B80/92</u>				BORING SITE DESCRIPTION SOIL TYPE: <u>WHEELING SANDY LOAM</u>							
DRILLING METHOD: <u>HSA</u>											
WATER LEVEL MEASUREMENTS											
MP											
DTW FROM MP	<u>N/A</u>										
TIME											
DATE											
DEPTH (FEET)	SAMPLE NUMBER	RECOVERY %	BLOW COUNTS	PTD READING	READING AT	USCS	SAMPLE TYPE	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FEET)
21	3C	75	9, 8, 8, 17	0.0	SS	ML	SS	Light Brown Sand			21
22			9, 9, 16, 6	0.0	SS	SW	SS	Light Brown Sand			22
23	50										23
24								G.O.B @ 24 Ft			24
25											25
6											6
7											7
8											8
9											9
10											10
11											11
12											12
13											13
14											14
15											15
16											16
17											17
18											18
19											19
20											20

LEGEND:

SAND & GRAVEL	CLAY	SILT & CLAY	SAND	SAND & SILT
SILT	BEDROCK	GRAVEL	SAPROLITE	WATER LEVEL

SPT = STANDARD PENETRATION TEST CAL = CALIBRATION BZ = BREATHING ZONE
 SS = SPLIT SPOON A = AUGER CUTTINGS C = CORED BH = BOXHOLE GS = GRAB SAMPLE

COMMENTS:

DRILLING CONTRACTOR: <u>CT & E</u>		ENGINEERING-SCIENCE DRILLING RECORD		BORING NO. <u>BG4 WL</u>							
DRILLER: <u>DAVE DOLAN</u>				SHEET <u>1</u> OF <u>1</u>							
GEOLOGIST: <u>S. GLENNIE</u>		PROJECT NAME <u>RAAP</u>		LOCATION: <u>NW REGION OF</u>							
RIG TYPE: <u>B80/92</u>		CLIENT <u>US AEC</u>		<u>RAAP, NEAR SWMU31</u>							
DRILLING METHOD: <u>HSA</u>		PROJECT NO. <u>722843</u>		BORING SITE DESCRIPTION							
WATER LEVEL MEASUREMENTS		WEATHER <u>85°F - HUMID</u>		Soil Type:							
MP		DATE/TIME START <u>7-20-95 / 1317</u>		Wheeling sandy							
DTW FROM MP	<u>N/A</u>	DATE/TIME FINISH <u>7-20-95 / 1325</u>		Loam.							
TIME											
DATE											
DEPTH (FEET)	SAMPLE NUMBER	RECOVERY %	BLOW COUNTS	PTD READING	READING AT	USCS	SAMPLE TYPE	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FEET)
1											1
2											2
3	48	50	7,16, 14,20	0.0	SS	CH	SS	BROWN SILT WITH CLAY.			3
4											4
5											5
6											6
7											7
8											8
9											9
10											10
11											11
12											12
13											13
14											14
15											15
16											16
17											17
18	4C	25	17,19 21,14	0.0	SS	ML	SS	BROWN SAND WITH COBBLES.			18
19											19
20								E.O.B. @ 19 Ft.			20

LEGEND: SAND & GRAVEL CLAY SILT & CLAY SAND SAND & SILT
 SILT BEDROCK GRAVEL SAPROLITE WATER LEVEL

SPT = STANDARD PENETRATION TEST CAL = CALIBRATION BZ = BELLHUNG ZONE
SS = SPLIT SPOON A = AUGER CUTTINGS C = CORED BH = BOREHOLE GS = GRAB SAMPLE

COMMENTS:

DRILLING CONTRACTOR: CT & E DRILLER: DAVE DOLAN GEOLOGIST: S. GLENNIE RIG TYPE: BB0/92 DRILLING METHOD: HSA				ENGINEERING-SCIENCE DRILLING RECORD				BORING NO. BG5WL SHEET 1 OF 1 LOCATION: NW REGION OF RAAP - NEAR SWMU31 BORING SITE DESCRIPTION SOIL TYPE: WHEELING SANDY LOAM.			
WATER LEVEL MEASUREMENTS MP _____ DTW FROM MP N/A TIME _____ DATE _____				PROJECT NAME RAAP CLIENT US AEC PROJECT NO. 722843 WEATHER 85°F - HUMID DATE/TIME START 7-20-95 / 1301 DATE/TIME FINISH 7-20-95 / 1310							

DEPTH (FEET)	SAMPLE NUMBER	RECOVERY %	BLOW COUNTS	PID READING	READING AT	USCS	SAMPLE TYPE	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FEET)
1	N/A	100	5,5, 6,7	0.0	SS	ML	SS	Light Brown silt, minor clay - HIGH ORGANICS.			1
2	5B	50	8,11, 14,17	0.0	SS	SC	SS	Brown silt with clay, dry. Dark red mottling.			2
3											3
4											4
5	N/A	100	17,12 17,14	0.0	SS	SM	SS	Dark red-brown silty sand, minor clay.			5
6											6
7	5C	50	12,12 13,12	0.0	SS	CL	SS	SAME AS (4-6'); WITH MORE CLAY.			7
8								E.O.B. @ 8 ft.			8
9											9
10											10
11											11
12											12
13											13
14											14
15											15
16											16
17											17
18											18
19											19
20											20

LEGEND:
 SAND & GRAVEL
 CLAY
 SILT & CLAY
 SAND
 SAND & SILT
 SILT
 BEDROCK
 GRAVEL
 SAPROLITE
 WATER LEVEL

SPT = STANDARD PENETRATION TEST CAL = CALIBRATION BZ = BELLHUNG ZONE
 SS = SPLIT SPOON A = AUGER CUTTINGS C = CORED BS = BOREHOLE GS = GRAB SAMPLE

COMMENTS:

DRILLING CONTRACTOR: <u>CT & E</u> DRILLER: <u>DAVE DOLAN</u> GEOLOGIST: <u>S. GLENNIE</u> RIG TYPE: <u>BB0/92</u> DRILLING METHOD: <u>HSA</u>	ENGINEERING-SCIENCE DRILLING RECORD	BORING NO. <u>BGG WL</u> SHEET <u>1</u> OF <u>1</u> LOCATION: <u>NW REGION OF</u> <u>RAAP - NEAR SWMU31</u> BORING SITE DESCRIPTION SOIL TYPE: <u>WHEELING SANDY LOAM</u>
PROJECT NAME <u>RAAP</u> CLIENT <u>US AEC</u> PROJECT NO. <u>722843</u>		
WATER LEVEL MEASUREMENTS MP _____ DTM FROM MP <u>N/A</u> TIME _____ DATE _____		
WEATHER <u>85°F - HUMID</u>		
DATE/TIME START <u>7-20-95 / 1225</u> DATE/TIME FINISH <u>7-20-95 / 1255</u>		

DEPTH (FEET)	SAMPLE NUMBER	RECOVERY %	BLOW COUNTS	PTD READING	READING AT	USCS	SAMPLE TYPE	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FEET)
1	N/A	< 10%	4, 5, 5, 7	0.0	SS	OL	SS	DARK BROWN, ORGANIC RICH SOIL			1
2											2
3	GB	100	16, 12, 16, 24	0.0	SS	SC	SS	BROWN SILT, WITH CLAY BLACK OXIDE STAINING			3
4											4
5	N/A	100	16, 16, 13, 14	0.0	SS	ML	SS	BROWN SILT, WITH CLAY			5
6											6
7	N/A	50	8, 12, 16, 18	0.0	SS	ML	SS	BROWN SILT, BLACK OXIDE STAINING			7
8											8
9											9
10											10
11											11
12											12
13											13
14											14
15											15
16	GC	25	5, 10, 17, 31	0.0	SS	ML	SS	COARSE BROWN SAND WITH COBBLES.			16
17								Rock at 17 Ft.			17
18								E.O.B. @ 17 Ft.			18
19											19
20											20

LEGEND:	SAND & GRAVEL	CLAY	SILT & CLAY	SAND	SAND & SILT
	SILT	BEDROCK	GRAVEL	SAPROLITE	WATER LEVEL
SPT = STANDARD PENETRATION TEST CAL = CALIBRATION BZ = BREATHING ZONE SS = SPLIT SPOON A = AUGER CUTTINGS C = COLED BB = BOREHOLE GS = GRAB SAMPLE					
COMMENTS:					

DRILLING CONTRACTOR: <u>CT & E</u> DRILLER: <u>DAVE DOLAN</u> GEOLOGIST: <u>S. GLENNIE</u> RIG TYPE: <u>BBO/92</u> DRILLING METHOD: <u>HSA</u>		ENGINEERING-SCIENCE DRILLING RECORD		BORING NO. <u>BG1BL</u> SHEET <u>1</u> OF <u>1</u> LOCATION: <u>N.E. REGION</u> <u>OF RAAP</u> BORING SITE DESCRIPTION <u>BRADDOCK LOAM</u> <u>SOIL TYPE.</u>	
WATER LEVEL MEASUREMENTS MP _____ DTW FROM MP <u>N/A</u> TIME _____ DATE _____		PROJECT NAME <u>RAAP</u> CLIENT <u>US AEC</u> PROJECT NO. <u>722B43</u> WEATHER <u>80°F, HUMID</u> DATE/TIME START <u>7-20-95 / 1105</u> DATE/TIME FINISH <u>7-20-95 / 1117</u>			

DEPTH (FEET)	SAMPLE NUMBER	RECOVERY %	BLOW COUNTS	PTD READING	READING AT	USCS	SAMPLE TYPE	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FEET)
1	N/A	< 25	5.9, 9.11	0.0	SS	OL	SS	FILL MATERIAL; ORGANIC MATERIAL: GRAVEL + SOIL			1
2											2
3	18	75	9.7, 9.10	0.0	SS	SC	SS	RED-BROWN SILT WITH SAND, MINOR CLAY, MINOR OXIDE STAINING.			3
4											4
5	N/A	50	9.8, 6.6	0.0	SS	SM	SS	RED SILT AND SAND, SOME BLACK OXIDE STAINING.			5
6											6
7	N/A	30	7.7, 5.7	0.0	SS	SM	SS	SAME AS (4-6').			7
8											8
9	1C	50	4.4, 6.7	0.0	SS	SM	SS	SAME AS (4-6').			9
10											10
11								E.O.B @ 10 Ft			11
12											12
13											13
14											14
15											15
16											16
17											17
18											18
19											19
20											20

LEGEND: SAND & GRAVEL SILT CLAY BEDROCK SILT & CLAY GRAVEL SAND SAPROLITE SAND & SILT WATER LEVEL	
---	--

SPT = STANDARD PENETRATION TEST CAL = CALIBRATION BT = BREATHER ZONE SS = SPLIT SPOON A = AUGER CUTTINGS C = CORED BH = BOREHOLE GS = GRAB SAMPLE	COMMENTS:
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DRILLING CONTRACTOR: <u>CT & E</u> DRILLER: <u>DAVE DOLAN</u> GEOLOGIST: <u>S. GLENNIE</u> RIG TYPE: <u>BB0/92</u> DRILLING METHOD: <u>HSA</u>	ENGINEERING-SCIENCE DRILLING RECORD	BORING NO. <u>BG2 BL</u> SHEET <u>1</u> OF <u>1</u> LOCATION: <u>NE REGION OF</u> <u>RAAP.</u> BORING SITE DESCRIPTION <u>Soil TYPE:</u> <u>BRADDOCK LOAM</u>
PROJECT NAME <u>RAAP</u> CLIENT <u>US AEC</u> PROJECT NO. <u>722843</u>		
WATER LEVEL MEASUREMENTS MP _____ DTH FROM MP <u>N/A</u> TIME _____ DATE _____		
WEATHER <u>80°F, HUMID</u> DATE/TIME START <u>7-20-95 / 1130</u> DATE/TIME FINISH <u>7-20-95 / 1150</u>		

DEPTH (FEET)	SAMPLE NUMBER	RECOVERY %	BLOW COUNTS	PTD READING	READING AT	USCS	SAMPLE TYPE	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FEET)
1											1
2											2
3											3
4	2B	30	7.6, 4.2	0.0	SS	CL	SS	BROWN SILT, SOME SAND, MINOR CLAY. DAMP.			4
5											5
6											6
7											7
8											8
9											9
10											10
11											11
12											12
13											13
14											14
15								BROWN CLAY, WITH SILT-MICACEOUS, AND SAND VERY MOIST.			15
16	2C	50	3.2, 3.6	0.0	SS	SC	SS				16
17								E.O.B. @ 17 FT.			17
18											18
19											19
20											20

LEGEND:	SAND & GRAVEL SILT	CLAY BEDROCK	SILT & CLAY GRAVEL	SAND SAPROLITE	SAND & SILT WATER LEVEL
SPT = STANDARD PENETRATION TEST CAL = CALIBRATION BZ = BREATHING ZONE SS = SPLIT SPOON A = AUGER CUTTINGS C = CORED BH = BOREHOLE CS = GRAB SAMPLE					
COMMENTS:					

DRILLING CONTRACTOR: <u>CT & E</u>		ENGINEERING-SCIENCE DRILLING RECORD	BORING NO. <u>BG3 BL</u>	
DRILLER: <u>DAVE DOLAN</u>			SHEET <u>1</u> OF <u>1</u>	
GEOLOGIST: <u>S. GLENNIE</u>			LOCATION: <u>NW REGION of</u> <u>HORSESHOE AREA. NEAR</u>	
RIG TYPE: <u>B80/92</u>			BORING SITE DESCRIPTION <u>GATE 10.</u>	
DRILLING METHOD: <u>HSA</u>		PROJECT NAME <u>RAAP</u>	WEATHER <u>85°F - HUMID</u>	
PROJECT NO. <u>722B43</u>		DATE/TIME START <u>7-20-95 / 1450</u>		
DATE/TIME FINISH <u>7-20-95 / 1511</u>		Soil Type: <u>BRADDOCK LOAM.</u>		
WATER LEVEL MEASUREMENTS				
MP				
DTW FROM MP	<u>N/A</u>			
TIME				
DATE				

DEPTH (FEET)	SAMPLE NUMBER	RECOVERY %	BLOW COUNTS	PTD READING	READING AT	USCS	SAMPLE TYPE	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FEET)
1											1
2	3B	25	4,6, 6,6	0.0	SS	CH	SS	LIGHT BROWN MICACEOUS SILT. ORGANIC STAINING.			2
3											3
4											4
5											5
6											6
7											7
8											8
9											9
10											10
11											11
12											12
13											13
14											14
15											15
16											16
17											17
18											18
19											19
20											20
21	3C	100	5,6 6,10	0.0	SS	MH	SS	RED BROWN SILT.			21
								E.O.B. @ 22 Ft.			

LEGEND:		SAND & GRAVEL	CLAY	SILT & CLAY	SAND	SAND & SILT
SILT	BEDROCK	GRAVEL	SAPROLITE	WATER LEVEL		
SPT = STANDARD PENETRATION TEST CAL = CALIBRATION BZ = BOLLATHING ZONE						
SS = SPLIT SPOON A = AUGER CUTTINGS C = CORED SE = BOREHOLE GS = GRAB SAMPLE						
COMMENTS:						

DRILLING CONTRACTOR: <u>CT & E</u> DRILLER: <u>DAVE DOLAN</u> GEOLOGIST: <u>S. GLENNIE</u> RIC TYPE: <u>BBO/92</u> DRILLING METHOD: <u>HSA</u> WATER LEVEL MEASUREMENTS MP _____ DTW FROM MP <u>N/A</u> TIME _____ DATE _____	ENGINEERING-SCIENCE DRILLING RECORD PROJECT NAME <u>RAAP</u> CLIENT <u>US AEC</u> PROJECT NO. <u>722B43</u> WEATHER <u>85°F - HUMID</u> DATE/TIME START <u>7-20-95 / 1415</u> DATE/TIME FINISH <u>7-20-95 / 1444</u>	BORING NO. <u>BG48L</u> SHEET <u>1</u> OF <u>1</u> LOCATION: <u>NW REGION OF HORSESHOE AREA</u> BORING SITE DESCRIPTION <u>NEAR GATE 10.</u> SOIL TYPE: <u>BRADDOCK LOAM.</u>
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DEPTH (FEET)	SAMPLE NUMBER	RECOVERY %	BLOW COUNTS	PTD READING	READING AT	USCS	SAMPLE TYPE	LITHOLOGY/REMARKS	LITHOLOGIC COLUMN	WELL COMPLETION	DEPTH (FEET)
1											1
2											2
3	4830		5,8, 6,7	0.0	SS	ML	SS	BROWN SILT WITH CLAY			3
4											4
5	N/A 100		5,6, 6,2	0.0	SS	CL	SS	SAME AS (2-4') MORE CLAY			5
6											6
7	N/A 75		1,3 7,4	0.0	SS	CL	SS	RED-BROWN CLAY, MINOR SILT.			7
8											8
9	4C 75		2,5, 5,10	0.0	SS	CL	SS	RED-BROWN CLAY WITH SILT.			9
10								E.O.B. @ 10 FT.			10
11											11
12											12
13											13
14											14
15											15
16											16
17											17
18											18
19											19
20											20

LEGEND: SAND & GRAVEL SILT CLAY BEDROCK SILT & CLAY GRAVEL SAND SAPROLITE SAND & SILT WATER LEVEL	SPT = STANDARD PENETRATION TEST CAL = CALIBRATION BZ = BELLWINDING ZONE SS = SPLIT SPOON A = AUGER CUTTINGS C = COAL BH = BOREHOLE GS = GRAB SAMPLE COMMENTS:
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APPENDIX D
MONITORING WELL DEVELOPMENT -
FIELD DATA SHEETS

WELL DEVELOPMENT SUMMARY SHEET

Project Name: RADFORD
 Location: _____
 Weather: _____

Well Number: 31 MW1
12-18-94

PURGING CALCULATIONS

Well Depth: 52.40 feet
 Depth to Water: 34.79 feet
 Water Column Length: (L) 17.61 FT
 Inner Casing Diameter (d): 4 inches = _____ feet
 Volume of Standing Water (V): 11.5 gallons

$$V (\text{gallons}) = 0.41 \times d^2 \times L$$

Total Volume to Purge: 69 gallons ($V \times 6$)

PURGING EQUIPMENT

Purging Device: SUB. PUMP

OBSERVATIONS

Purge Water Appearance Initial: Clear / Turbid / Opaque
 Purge Water Appearance Initial: Clear / Turbid / Opaque

PURGE WATER TESTING

		After 3 vol	After 6 vol		
	Initial Test	2nd Test	3rd Test	4th Test*	5th Test*
Time	0945	0955	1005	1015	1025
Purged Volume (GAL)		35	70	95	115
Turbidity					
Odor	-	-	-	-	-
PID					
pH	7.03	7.43	7.42	7.35	7.30
Conductance	336	336	338	351	334
Temperature (°F)	60.4	62.4	61.0	65.1	63.1

ms/cm F

COMMENTS

* IF NOT CLEAR AFTER 6 VOLUMES, PUMP 5 MINUTES MORE AND TAKE MEASUREMENTS. IF CLEAR OR WITHIN 20% OF PREVIOUS READINGS, STOP. IF NOT, REPEAT UNTIL WITHIN 20%.

WELL DEVELOPMENT SUMMARY SHEET

Project Name: RADFORD Well Number: 31MW2
 Location: _____
 Weather: _____ 12-17-94

PURGING CALCULATIONS

Well Depth: 28.50 feet
 Depth to Water: 26.06 feet
 Water Column Length: (L) 2.44 FT
 Inner Casing Diameter (d): 4 inches = _____ feet
 Volume of Standing Water (V): 1.6 gallons

$$V (\text{gallons}) = 0.41 \times d^2 \times L$$

Total Volume to Purge: 9.6 gallons ($V \times 6$)

PURGING EQUIPMENT

Purging Device: SUB. pump

OBSERVATIONS

Purge Water Appearance Initial: Clear / Turbid / Opaque
 Purge Water Appearance Initial: Clear / Turbid / Opaque

PURGE WATER TESTING

	Initial Test	After 3 vol 2nd Test	After 6 vol 3rd Test	4th Test *	5th Test *
Time	<u>1055</u>	<u>1109</u>	<u>1129</u>		
Purged Volume (<u>GAL</u>)		<u>5</u>	<u>10</u>		
Turbidity					
Odor	<u>—</u>	<u>—</u>	<u>—</u>		
PID					
pH	<u>7.52</u>	<u>7.61</u>	<u>7.79</u>		
Conductance	<u>991</u>	<u>291</u>	<u>281</u>		
Temperature (<u>°F</u>)	<u>64.3</u>	<u>61.7</u>	<u>61.9</u>		

COMMENTS

* IF NOT CLEAR AFTER 6 VOLUMES, PUMP 5 MINUTES MORE AND TAKE MEASUREMENTS. IF CLEAR OR WITHIN 20% OF PREVIOUS READINGS, STOP. IF NOT, REPEAT UNTIL WITHIN 20%.

WELL DEVELOPMENT SUMMARY SHEET

Project Name: RADFORDWell Number: 31MW3

Location: _____

Weather: _____

12/17/94PURGING CALCULATIONSWell Depth: 32.43 feetDepth to Water: 24.16 feetWater Column Length: (L) 8.27 FTInner Casing Diameter (d): 4 inches = _____ feetVolume of Standing Water (V): 5.4 gallons

$$V \text{ (gallons)} = 0.41 \times d^2 \times L$$

Total Volume to Purge: 32.4 gallons ($V \times 6$)PURGING EQUIPMENTPurging Device: SUB. pumpOBSERVATIONSPurge Water Appearance Initial: Clear / Turbid / OpaquePurge Water Appearance Initial: Clear / Turbid / OpaquePURGE WATER TESTING

	Initial Test	After 3 vol	After 6 vol		
	Initial Test	2nd Test	3rd Test	4th Test *	5th Test *
Time	<u>0940</u>	<u>0950</u>	<u>1003</u>	<u>1010</u>	<u>1025</u>
Purged Volume (GAL)	<u>20</u>	<u>40</u>	<u>46</u>	<u>52</u>	
Turbidity					
Odor					
PID					
pH	<u>7.43</u>	<u>7.52</u>	<u>7.71</u>	<u>7.50</u>	<u>7.60</u>
Conductance	<u>180</u>	<u>332</u>	<u>340</u>	<u>341</u>	<u>293</u>
Temperature (°F)	<u>59.9</u>	<u>60.7</u>	<u>62.5</u>	<u>63.0</u>	<u>65.2</u>

us/cm FCOMMENTS

* IF NOT CLEAR AFTER 6 VOLUMES, PUMP 5 MINUTES MORE AND TAKE MEASUREMENTS. IF CLEAR OR WITHIN 20% OF PREVIOUS READINGS, STOP. IF NOT, REPEAT UNTIL WITHIN 20%.

WELL DEVELOPMENT SUMMARY SHEET

Project Name:

RADFORD

Well Number:

31 MW4

Location:

Weather:

12-17-94

PURGING CALCULATIONS

Well Depth:

30.45

feet

Depth to Water:

24.60

feet

Water Column Length: (L)

5.80 FT

Inner Casing Diameter (d):

4

inches =

feet

Volume of Standing Water (V):

3.8

gallons

$$V (\text{gallons}) = 0.41 \times d^2 \times L$$

Total Volume to Purge:

22.7

gallons ($V \times 6$)PURGING EQUIPMENT

Purging Device:

Sub. pump

OBSERVATIONS

Purge Water Appearance Initial:

Clear / Turbid / Opaque

Purge Water Appearance Initial:

Clear / Turbid / Opaque

PURGE WATER TESTING

	Initial Test	After 3 vol 2nd Test	After 6 vol 3rd Test	4th Test *	5th Test *
Time	1300				
Purged Volume (GAL)		12	24		
Turbidity					
Odor					
PID	NOTE: DRILLER LOST ORIGINAL SHEET WITH MEASUREMENTS. AMOUNT PURGED OBTAINED FROM DRILLER'S DAILY LOG. WELL HAD BEEN DEVELOPED COMPLETELY IN ACCORDANCE WITH PROCEDURES.				
pH					
Conductance					
Temperature (C)					

COMMENTS

* IF NOT CLEAR AFTER 6 VOLUMES, PUMP 5 MINUTES MORE AND TAKE MEASUREMENTS. IF CLEAR OR WITHIN 20% OF PREVIOUS READINGS, STOP. IF NOT, REPEAT UNTIL WITHIN 20%.

WELL DEVELOPMENT SUMMARY SHEET

Project Name: RADFORDWell Number: 48MW1

Location: _____

Weather: _____

12/21/94PURGING CALCULATIONSWell Depth: 142.00 feetDepth to Water: 106.90 feetWater Column Length: (L) 35.1 FTInner Casing Diameter (d): 4 inches = _____ feetVolume of Standing Water (V): 22.9 gallons

$$V (\text{gallons}) = 0.41 \times d^2 \times L$$

Total Volume to Purge: _____

22.9 gallons (V x 6)
137.5
PURGING EQUIPMENT

Purging Device: _____

Sub. pumpOBSERVATIONSPurge Water Appearance Initial: Clear / Turbid / OpaquePurge Water Appearance Initial: Clear / Turbid / OpaquePURGE WATER TESTING

	Initial Test	After 3 vol 2nd Test	After 6 vol 3rd Test	4th Test *	5th Test *
Time	<u>1515</u>	<u>1524</u>	<u>1535</u>	<u>1550</u>	
Purged Volume (GAL)		<u>69</u>	<u>138</u>	<u>175</u>	
Turbidity					
Odor	<u>—</u>	<u>—</u>	<u>—</u>	<u>—</u>	
PID					
pH	<u>7.03</u>	<u>7.22</u>	<u>7.19</u>	<u>7.24</u>	
Conductance	<u>369</u>	<u>352</u>	<u>342</u>	<u>343</u>	
Temperature (°F)	<u>55.2</u>	<u>50.7</u>	<u>54.3</u>	<u>52.7</u>	

45/cm FCOMMENTS

* IF NOT CLEAR AFTER 6 VOLUMES, PUMP 5 MINUTES MORE AND TAKE MEASUREMENTS. IF CLEAR OR WITHIN 20% OF PREVIOUS READINGS, STOP. IF NOT, REPEAT UNTIL WITHIN 20%.

WELL DEVELOPMENT SUMMARY SHEET

Project Name: RADFORD Well Number: 48MW2
 Location: _____
 Weather: _____ 1/9/95

PURGING CALCULATIONS

Well Depth: 135.7 feet
 Depth to Water: 117.5 feet
 Water Column Length: (L) 18.2 FT
 Inner Casing Diameter (d): 2 inches = _____ feet
 Volume of Standing Water (V): 3.0 gallons

$$V (\text{ga'lons}) = 0.41 \times d^2 \times L$$

Total Volume to Purge: 18 gallons ($V \times 6$)

PURGING EQUIPMENT

Purging Device: Sub. pump

OBSERVATIONS

Purge Water Appearance Initial: Clear / Turbid / Opaque
 Purge Water Appearance Initial: Clear / Turbid / Opaque

PURGE WATER TESTING

	Initial Test	After 3 vol	After 6 vol		
	Initial Test	2nd Test	3rd Test	4th Test *	5th Test *
Time	<u>1330</u>	<u>1345</u>	<u>1400</u>	<u>1410</u>	
Purged Volume (GAL)	<u>6</u>	<u>10</u>	<u>20</u>	<u>25</u>	
Turbidity					
Odor	<u>-</u>	<u>-</u>	<u>-</u>	<u>-</u>	
PID					
pH	<u>8.10</u>	<u>7.79</u>	<u>7.81</u>	<u>7.84</u>	
Conductance	<u>329</u>	<u>334</u>	<u>332</u>	<u>342</u>	
Temperature (°F)	<u>60.7</u>	<u>59.4</u>	<u>55.6</u>	<u>57.3</u>	

COMMENTS

* IF NOT CLEAR AFTER 6 VOLUMES, PUMP 5 MINUTES MORE AND TAKE MEASUREMENTS. IF CLEAR OR WITHIN 20% OF PREVIOUS READINGS, STOP. IF NOT, REPEAT UNTIL WITHIN 20%.

WELL DEVELOPMENT SUMMARY SHEET

Project Name: RADFORD Well Number: 48MW3
 Location: _____
 Weather: _____ 1/10/95

PURGING CALCULATIONS

Well Depth: 122.30 feet
 Depth to Water: 93.22 feet
 Water Column Length: (L) 29.08 FT
 Inner Casing Diameter (d): 4 inches = _____ feet
 Volume of Standing Water (V): 18.99 gallons

$$V (\text{gallons}) = 0.41 \times d^2 \times L$$

Total Volume to Purge: ~~18.99~~ gallons (V x 6)
114

PURGING EQUIPMENT

Purging Device: Sub. pump

OBSERVATIONS

Purge Water Appearance Initial: Clear / Turbid / Opaque
 Purge Water Appearance Initial: Clear / Turbid / Opaque

PURGE WATER TESTING

	Initial Test	After 3 vol	After 6 vol		
	Initial Test	2nd Test	3rd Test	4th Test*	5th Test*
Time	1230	1240	1250	1300	
Purged Volume (GAL)		60	120	150	
Turbidity					
Odor	-	-	-	-	
PID					
pH	7.20	7.26	7.31	7.27	
Conductance	346	354	352	357	
Temperature (°F)	54.2	55.7	57.8	58.0	

ms/cm

COMMENTS

* IF NOT CLEAR AFTER 6 VOLUMES, PUMP 5 MINUTES MORE AND TAKE MEASUREMENTS. IF CLEAR OR WITHIN 20% OF PREVIOUS READINGS, STOP. IF NOT, REPEAT UNTIL WITHIN 20%

WELL DEVELOPMENT SUMMARY SHEET

Project Name: RADFORD Well Number: 48 MW4
 Location: _____
 Weather: _____ 7/22/95

PURGING CALCULATIONS

Well Depth: 96.06 feet
 Depth to Water: 71.40 feet
 Water Column Length: (L) 24.66 Ft
 Inner Casing Diameter (d): 4 inches = _____ feet
 Volume of Standing Water (V): 16.10 gallons

$$V (\text{gallons}) = 0.41 \times d^2 \times L$$

Total Volume to Purge: 96.6 gallons ($V \times 6$)

PURGING EQUIPMENT

Purging Device: Sub. pump

OBSERVATIONS

Purge Water Appearance Initial: Clear / Turbid / Opaque
 Purge Water Appearance Initial: Clear / Turbid / Opaque

PURGE WATER TESTING

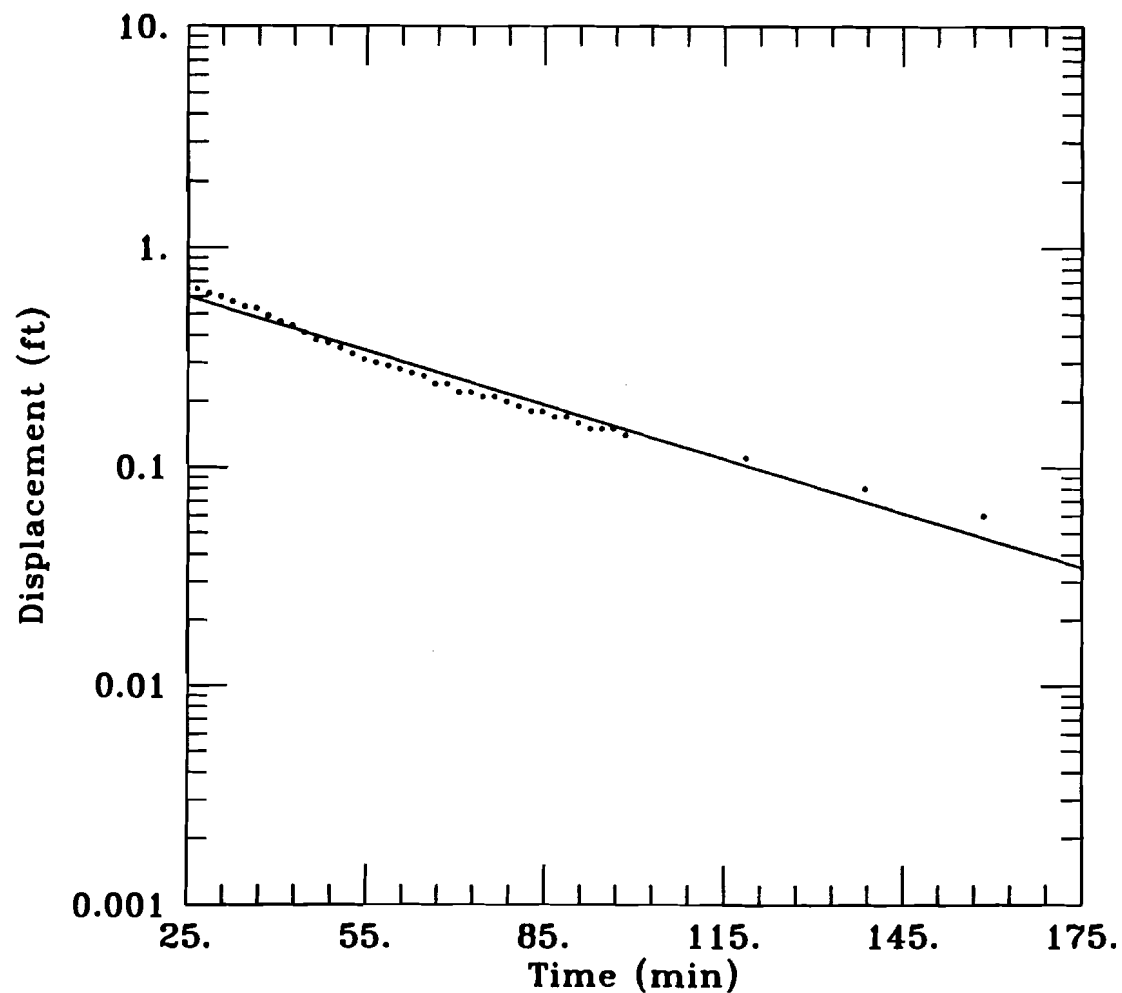
	Initial Test	After 3 vol 2nd Test	After 6 vol 3rd Test	4th Test *	5th Test *
Time	1000	1037	1130	1135	1145
Purged Volume (GAL)		50	100	115	130
Turbidity					
Odor					
PID					
pH	7.88	8.06	7.96	7.46	7.71
Conductance	154	280	431	313	361
Temperature (°F)	70.3	73.9	77.6	73.4	77.9

MS/cm (F)

COMMENTS

* IF NOT CLEAR AFTER 6 VOLUMES, PUMP 5 MINUTES MORE AND TAKE MEASUREMENTS. IF CLEAR OR WITHIN 20% OF PREVIOUS READINGS, STOP. IF NOT, REPEAT UNTIL WITHIN 20%.

APPENDIX E
AQUIFER SLUG TESTING DATA



DATA SET:
SMU31MW1.DAT
09/03/95

AQUIFER MODEL:
Unconfined
SOLUTION METHOD:
Bouwer-Rice

PROJECT DATA:
test date: January 12, 1995
obs. well: 31MW1

TEST DATA:
H0 = 3.25 ft
rc = 0.167 ft
rw = 0.413 ft
L = 10. ft
b = 20. ft
H = 17.24 ft

PARAMETER ESTIMATES:
K = 0.0001607 ft/min
y0 = 0.9645 ft

RAAP SWMU-31 31MW1 INJECTION

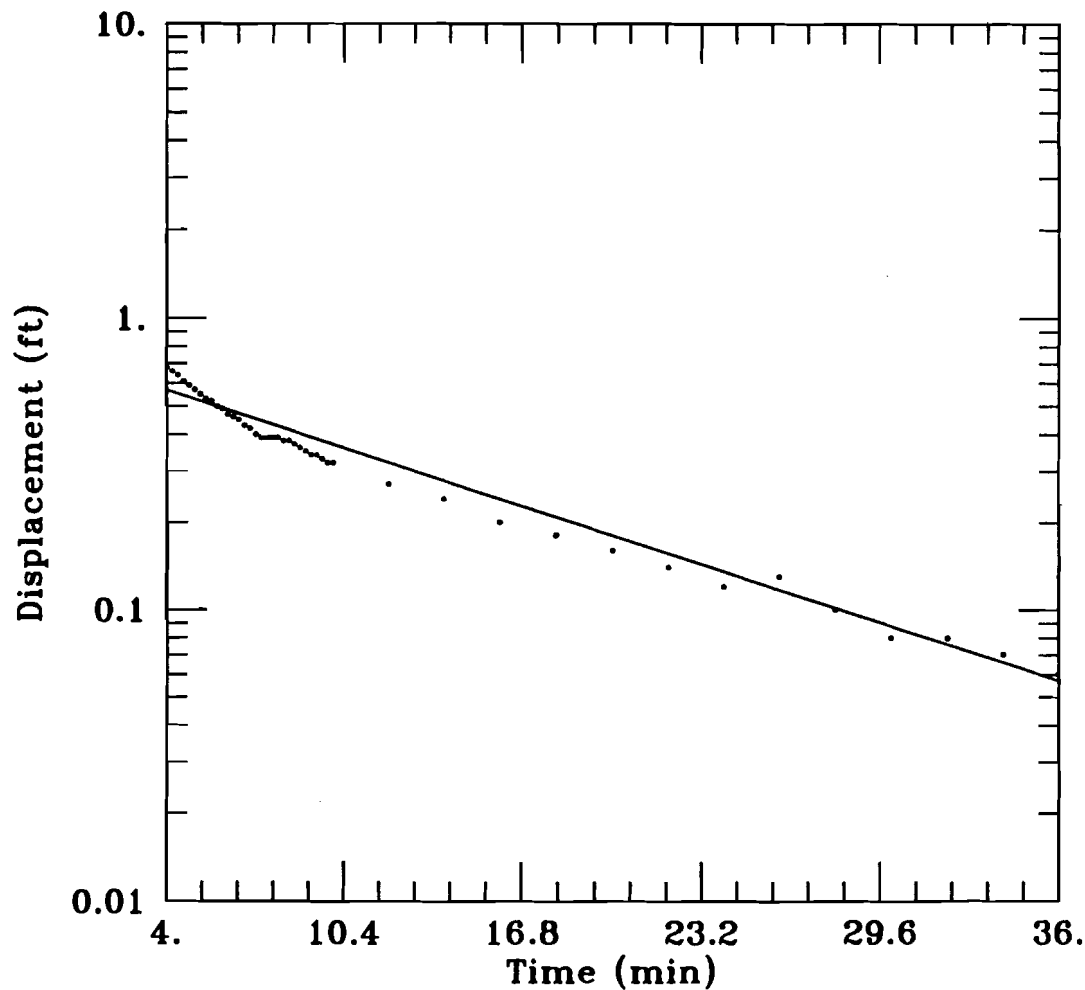
Client: USAEC

Company: Parsons Engineering Science

Location: Radford, Virginia

Project: 722843

AGTESOLV



DATA SET:
SMU31MW2.DAT
09/03/95

AQUIFER MODEL:
Unconfined
SOLUTION METHOD:
Bouwer-Rice

PROJECT DATA:
test date: JANUARY 12, 1995
obs. well: SWMU-31 31MW2

TEST DATA:
H0 = 2.18 ft
rc = 0.167 ft
rw = 0.413 ft
L = 10. ft
b = 20. ft
H = 4.46 ft

PARAMETER ESTIMATES:
K = 0.0004158 ft/min
y0 = 0.7575 ft

RAAP SWMU-31 31MW2 INJECTION

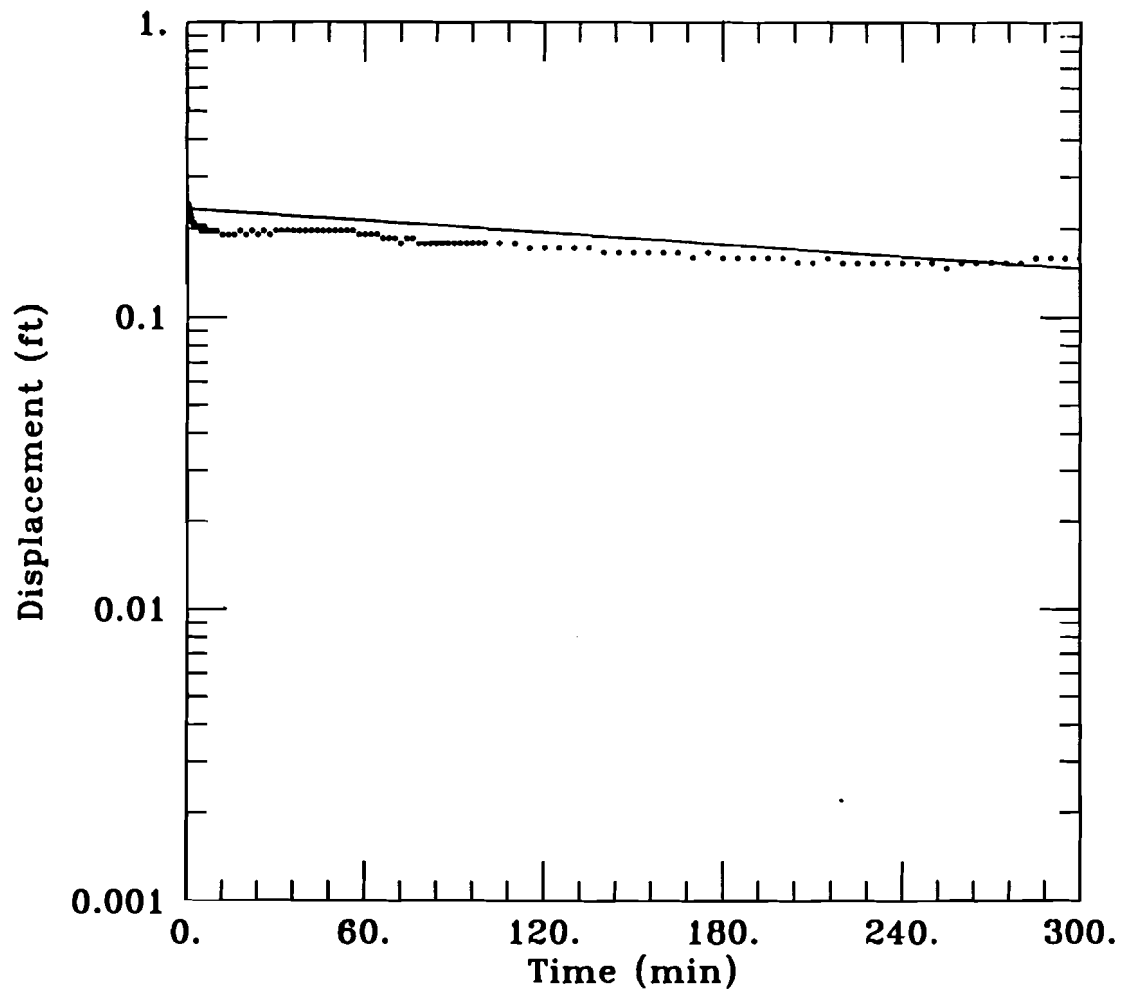
Client: USAEC

Company: PARSONS ENGINEERING SCIENCE

Location: RADFORD, VIRGINIA

Project: 722843

AQTESOLV



DATA SET:
S4U31MW3.DAT
07/03/95

AQUIFER MODEL:
Unconfined
SOLUTION METHOD:
Bouwer-Rice

PROJECT DATA:
test date: January 11, 1995
obs. well: 31MW3

TEST DATA:
H0 = 0.51 ft
rc = 0.167 ft
rw = 0.413 ft
L = 10. ft
b = 20. ft
H = 6.87 ft

PARAMETER ESTIMATES:
K = 1.024E-05 ft/min
y0 = 0.2338 ft

RAAP SWMU-31 31MW3 INJECTION

Client: USAEC

Company: Parsons Engineering Science

Location: Radford, Virginia

Project: 722843

AQTESOLV

Developed by Glenn M. Duffield
(c) 1988-1995 Geraqhty & Miller, Inc.

13:37:0

TEST DESCRIPTION

```

Units of Measurement
Length..... ft
Time..... min

```

Test Well Data

Initial displacement in well.....	0.51		
Radius of well casing.....	0.167		
Radius of wellbore.....	0.413		
Aquifer saturated thickness.....	20		
Well screen length.....	10		
Static height of water in well...	6.87		
Gravel pack porosity.....	0.3		
Effective well casing radius.....	0.2659		
Effective wellbore radius.....	0.413		
Log (Re/Rw)	1.862		
Constants A, B and C.....	2.269	0.364,	0.000
No. of observations.....	314		

ANALYTICAL METHOD

Bouwer-Rice (Unconfined Aquifer Slug Test)

RESULTS FROM VISUAL CURVE MATCHING

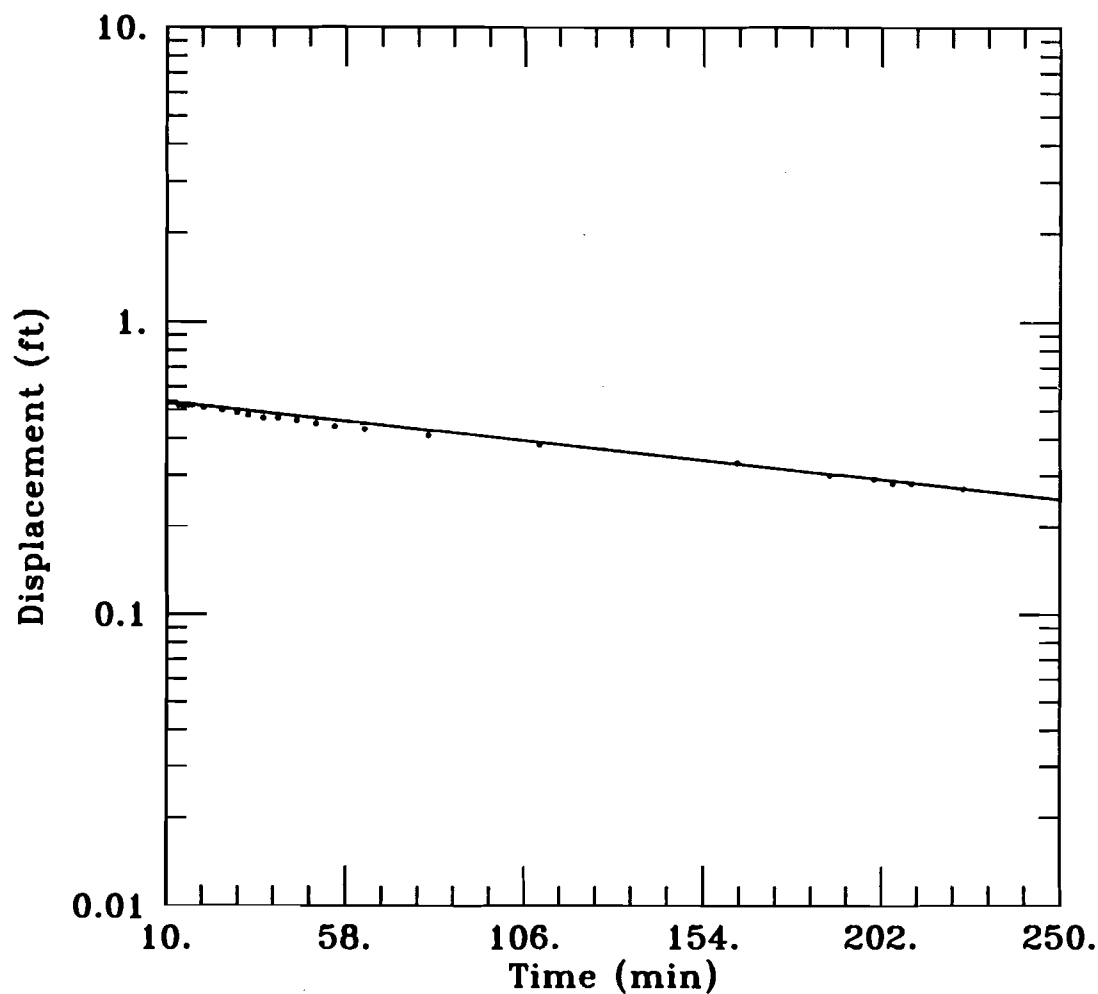
VISUAL MATCH PARAMETER ESTIMATES

```

      Estimate
K   =  1.0236E-005 ft/min
y0  =  2.3381E-001 ft

```

[illegible]



DATA SET:
SMU31M3W.DAT
09/03/95

AQUIFER MODEL:
Unconfined
SOLUTION METHOD:
Bouwer-Rice

PROJECT DATA:
test date: JANUARY 12, 1995
obs. well: 31MW3

TEST DATA:
H0 = 1.47 ft
rc = 0.167 ft
rw = 0.413 ft
L = 10. ft
b = 50. ft
H = 6.87 ft

PARAMETER ESTIMATES:
K = 2.034E-05 ft/min
y0 = 0.5517 ft

RAAP SWMU-31 31MW3 WITHDRAWAL

Client: USAEC

Company: PARSONS ENGINEERING SCIENCE

Location: RADFORD, VIRGINIA

Project: 722843

AQTESOLV

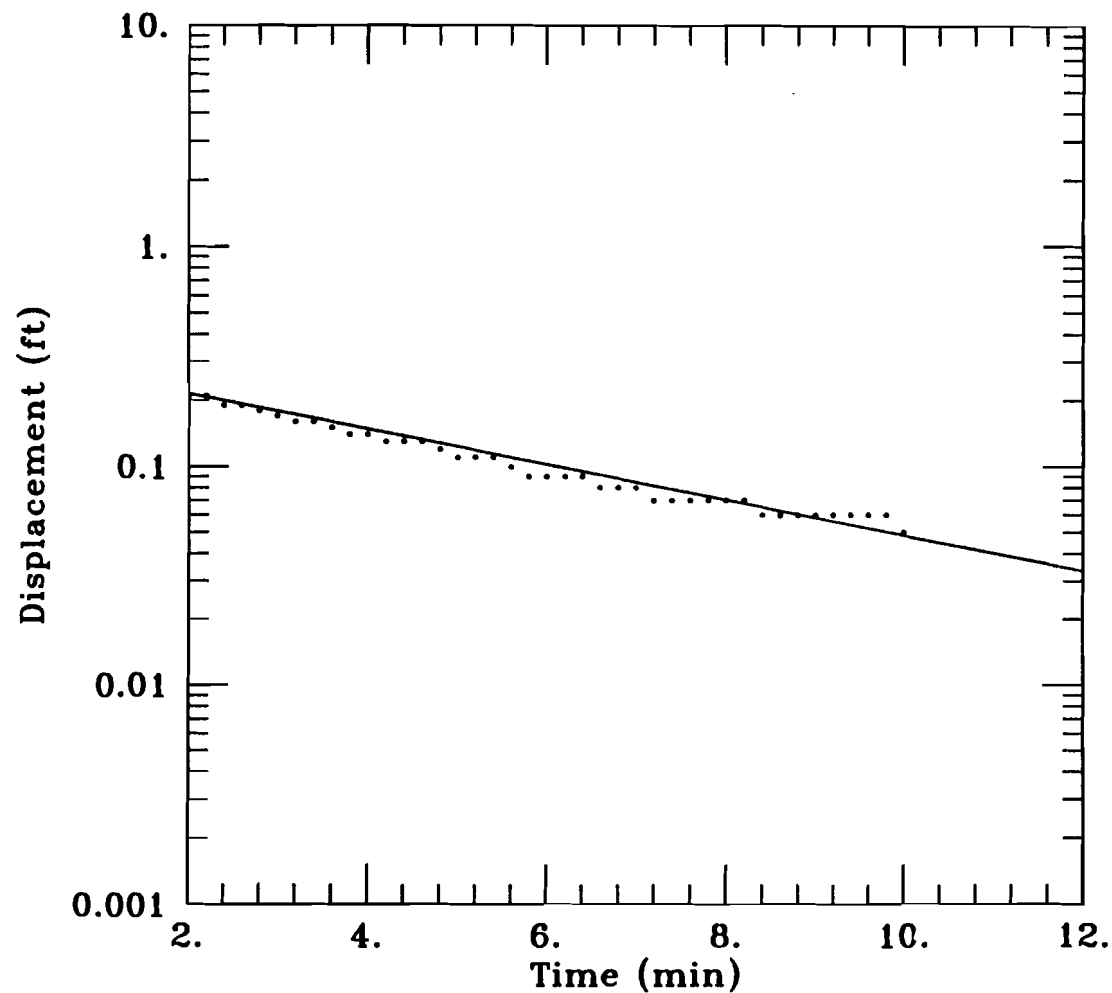
residual = observed - calculated
weighted residual = residual * weight

Weighted Residual Statistics:

Number of residuals..... 57
Number of estimated parameters.... 2
Degrees of freedom..... 55
Residual mean..... 0.001927
Residual standard deviation..... 0.1349
Residual variance..... 0.0182

Model Residuals:

Time	Observed	Calculated	Residual	Weight
1	1.35	0.66045	0.68955	1
1.17	1.05	0.6598	0.3902	1
1.25	0.94	0.65949	0.28051	1
1.5	0.84	0.65854	0.18146	1
1.58	0.78	0.65824	0.12176	1
1.67	0.74	0.65789	0.082106	1
1.75	0.73	0.65759	0.072409	1
1.91	0.71	0.65698	0.053017	1
2	0.69	0.65664	0.033358	1
2.25	0.68	0.65569	0.024306	1
2.41	0.67	0.65509	0.014911	1
2.5	0.656	0.65475	0.0012519	1
2.67	0.65	0.65411	-0.0041055	1
2.91	0.64	0.6532	-0.013199	1
3.17	0.63	0.65222	-0.022219	1
3.33	0.62	0.65162	-0.031617	1
3.67	0.61	0.65034	-0.040338	1
3.91	0.6	0.64944	-0.049437	1
4	0.59	0.6491	-0.0591	1
4.75	0.58	0.64629	-0.066294	1
5	0.57	0.64536	-0.075362	1
6	0.57	0.64164	-0.071645	1
6.25	0.55	0.64072	-0.090719	1
6.75	0.55	0.63887	-0.088871	1
7.25	0.55	0.63703	-0.087029	1
8.25	0.55	0.63336	-0.08336	1
9.25	0.54	0.62971	-0.089712	1
9.75	0.53	0.6279	-0.097896	1
10.25	0.53	0.62609	-0.096086	1
11.25	0.53	0.62248	-0.09248	1
12.25	0.53	0.61889	-0.088895	1
13.25	0.52	0.61533	-0.09533	1
14.25	0.52	0.61179	-0.091787	1
15.25	0.52	0.60826	-0.088263	1
16	0.52	0.60563	-0.085634	1
17	0.52	0.60215	-0.082146	1
20	0.51	0.5918	-0.081802	1
25	0.5	0.57496	-0.074955	1
29	0.49	0.56182	-0.071824	1
32	0.48	0.55217	-0.072173	1
36	0.47	0.53956	-0.069562	1
40	0.47	0.52724	-0.057239	1
45	0.46	0.51223	-0.05223	1
50	0.45	0.49765	-0.047649	1



DATA SET:
SMU31MW4.DAT
09/03/95

AQUIFER MODEL:
Unconfined
SOLUTION METHOD:
Bouwer-Rice

PROJECT DATA:
test date: January 11, 1995
obs. well: 31MW4

TEST DATA:
H0 = 0.33 ft
rc = 0.167 ft
rw = 0.413 ft
L = 10. ft
b = 20. ft
H = 5.61 ft

PARAMETER ESTIMATES:
K = 0.001161 ft/min
y0 = 0.3135 ft

RAAP SWMU-31 31MW4 INJECTION

Client: USAEC

Company: Parsons Engineering Science

Location: Radford, Virginia

Project: 722483

AQTESOLV

09:14:31

ANALYSIS OF MODEL RESIDUALS

residual = observed - calculated
 weighted residual = residual * weight

Weighted Residual Statistics:

Number of residuals..... 84
 Number of estimated parameters.... 2
 Degrees of freedom..... 82
 Residual mean..... 0.05972
 Residual standard deviation..... 0.1186
 Residual variance..... 0.01408

Model Residuals:

Time	Observed	Calculated	Residual	Weight
0.75	1.55	1.2931	0.25694	1
0.767	1.47	1.2102	0.25981	1
0.783	1.3	1.1371	0.16294	1
0.8	1.18	1.0642	0.11581	1
0.817	1.09	0.996	0.094004	1
0.833	1.01	0.93581	0.074193	1
0.85	0.61	0.87584	-0.26584	1
0.867	0.64	0.81971	-0.17971	1
0.883	0.59	0.77017	-0.18017	1
0.9	0.55	0.72082	-0.17082	1
0.917	0.52	0.67463	-0.15463	1
0.933	0.49	0.63386	-0.14386	1
0.95	0.47	0.59324	-0.12324	1
0.967	0.45	0.55522	-0.10522	1
0.983	0.43	0.52167	-0.091669	1
1	0.42	0.48824	-0.068238	1
1.2	0.4	0.224	0.176	1
1.4	0.3	0.10277	0.19723	1
1.6	0.26	0.047148	0.21285	1
1.8	0.23	0.021631	0.20837	1
2	0.21	0.009924	0.20008	1
2.2	0.21	0.004553	0.20545	1
2.4	0.19	0.0020889	0.18791	1
2.6	0.19	0.00095835	0.18904	1
2.8	0.18	0.00043968	0.17956	1
3	0.17	0.00020172	0.1698	1
3.2	0.16	9.2546E-005	0.15991	1
3.4	0.16	4.2459E-005	0.15996	1
3.6	0.15	1.948E-005	0.14998	1
3.8	0.14	8.937E-006	0.13999	1
4	0.14	4.1002E-006	0.14	1
4.2	0.13	1.8811E-006	0.13	1
4.4	0.13	8.6303E-007	0.13	1
4.6	0.13	3.9595E-007	0.13	1
4.8	0.12	1.8166E-007	0.12	1
5	0.11	8.3341E-008	0.11	1
5.2	0.11	3.8236E-008	0.11	1
5.4	0.11	1.7542E-008	0.11	1
5.6	0.1	8.0481E-009	0.1	1
5.8	0.09	3.6924E-009	0.09	1
6	0.09	1.694E-009	0.09	1
6.2	0.09	7.7719E-010	0.09	1
6.4	0.09	3.5657E-010	0.09	1
6.6	0.08	1.6359E-010	0.08	1

6.8	0.08	7.5052E-011	0.08	1
7	0.08	3.4433E-011	0.08	1
7.2	0.07	1.5797E-011	0.07	1
7.4	0.07	7.2476E-012	0.07	1
7.6	0.07	3.3251E-012	0.07	1
7.8	0.07	1.5255E-012	0.07	1
8	0.07	6.9989E-013	0.07	1
8.2	0.07	3.211E-013	0.07	1
8.4	0.06	1.4732E-013	0.06	1
8.6	0.06	6.7587E-014	0.06	1
8.8	0.06	3.1008E-014	0.06	1
9	0.06	1.4226E-014	0.06	1
9.2	0.06	6.5268E-015	0.06	1
9.4	0.06	2.9944E-015	0.06	1
9.6	0.06	1.3738E-015	0.06	1
9.8	0.06	6.3028E-016	0.06	1
10	0.05	2.8916E-016	0.05	1
12	0.05	1.1947E-019	0.05	1
14	0.04	4.936E-023	0.04	1
16	0.03	2.0393E-026	0.03	1
18	0.02	8.4255E-030	0.02	1
20	0.02	3.4811E-033	0.02	1
22	0.02	1.4382E-036	0.02	1
24	0.02	5.9421E-040	0.02	1
26	0.01	2.455E-043	0.01	1
28	0.02	1.0143E-046	0.02	1
30	0.01	4.1906E-050	0.01	1
32	0.01	1.7314E-053	0.01	1
34	0.01	7.1533E-057	0.01	1
36	0.01	2.9554E-060	0.01	1
38	0.01	1.2211E-063	0.01	1
40	0.01	5.0449E-067	0.01	1
42	0.01	2.0843E-070	0.01	1
44	0.01	8.6114E-074	0.01	1
46	0.01	3.5579E-077	0.01	1
48	0.01	1.47E-080	0.01	1
50	0.01	6.0732E-084	0.01	1
52	0.01	2.5092E-087	0.01	1
54	0.01	1.0367E-090	0.01	1
56	0.01	4.2831E-094	0.01	1

100

=====
RESULTS FROM VISUAL CURVE MATCHING

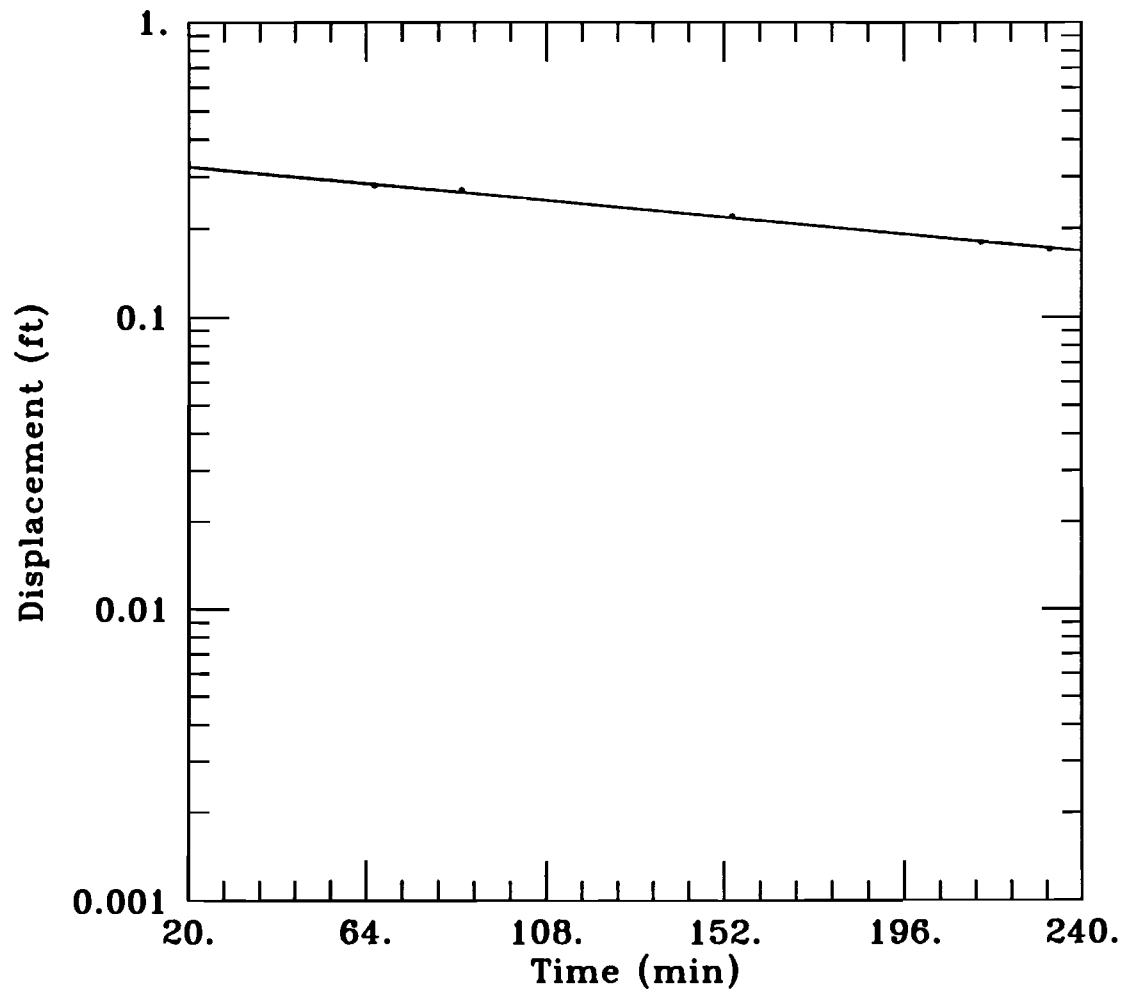
VISUAL MATCH PARAMETER ESTIMATES

```

      Estimate
K   =  8.3952E-003 ft/min
y0  =  9.5775E+000 ft

```

[illegible]



DATA SET:
SMU31M4W.DAT
09/03/95

AQUIFER MODEL:
Unconfined
SOLUTION METHOD:
Bouwer-Rice

PROJECT DATA:
test date: JANUARY 12, 1995
obs. well: 31MW4

TEST DATA:
H0 = 0.9 ft
rc = 0.167 ft
rw = 0.413 ft
L = 10. ft
b = 20. ft
H = 5.3 ft

PARAMETER ESTIMATES:
K = 1.821E-05 ft/min
y0 = 0.3432 ft

RAAP SWMU-31 31MW4 WITHDRAWAL

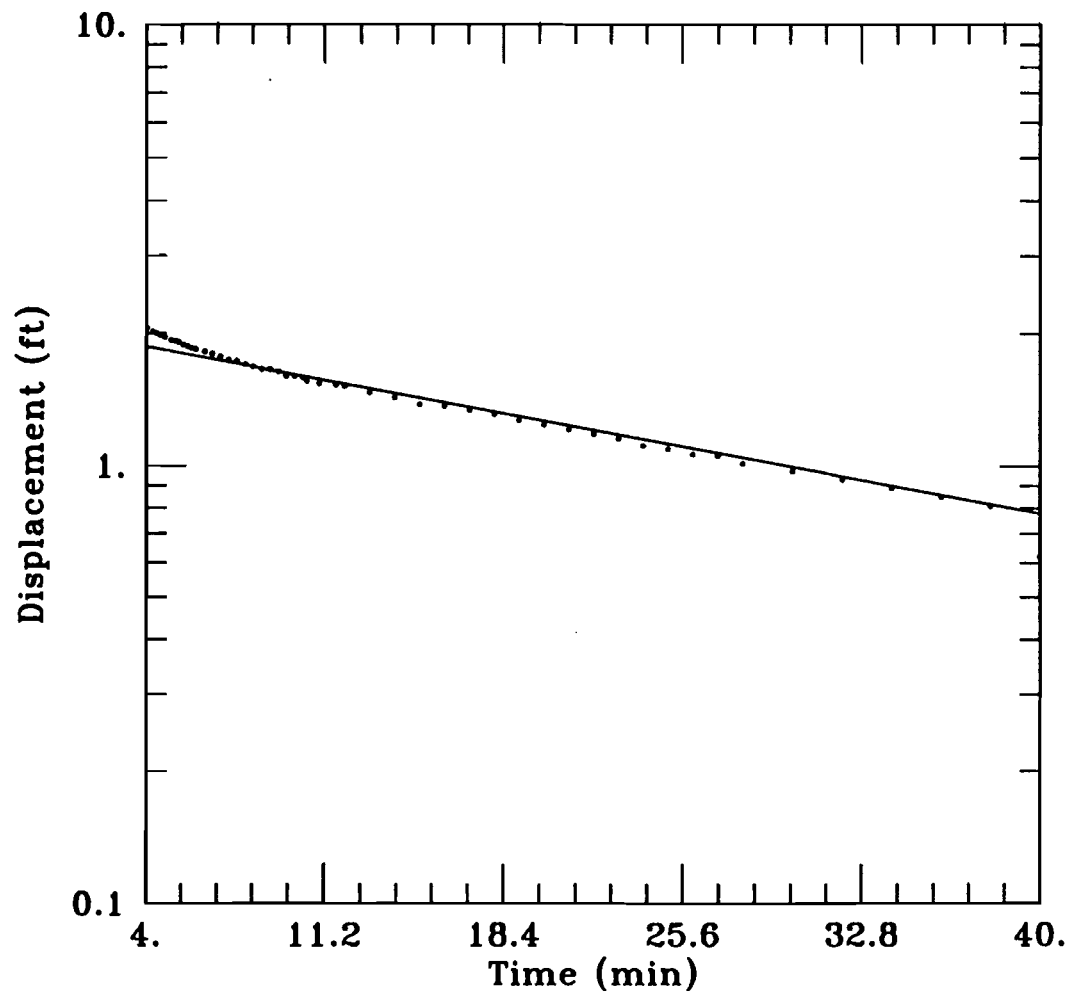
Client: USAEC

Company: PARSONS ENGINEERING SCIENCE

Location: RADFORD, VIRGINIA

Project: 722843

AGTESOLV



DATA SET:
SMU48MW1.DAT
09/03/95

AQUIFER MODEL:
Unconfined
SOLUTION METHOD:
Bouwer-Rice

PROJECT DATA:
test date: January 13, 1995
obs. well: 48MW1

TEST DATA:
H0 = 3.24 ft
rc = 0.167 ft
rw = 0.413 ft
L = 30. ft
b = 50. ft
H = 42.96 ft

PARAMETER ESTIMATES:
K = 9.178E-05 ft/min
y0 = 2.056 ft

RAAP SWMU-48 48MW1 INJECTION

Client: USAEC

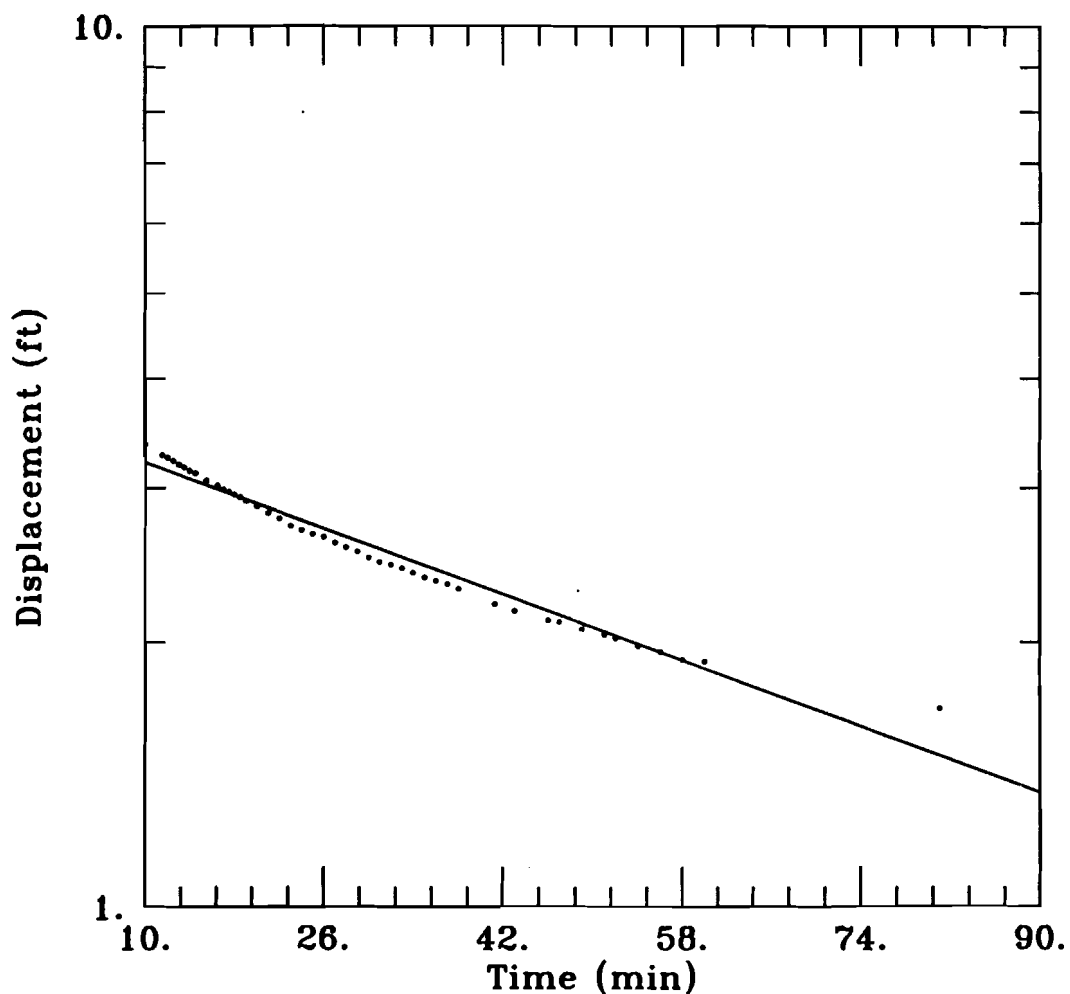
Company: Parsons Engineering Science

Location: Radford, Virginia

Project: 722843

AGTESOLV

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DATA SET:
SMU48M1W.DAT
09/03/95

AQUIFER MODEL:
Unconfined
SOLUTION METHOD:
Bouwer-Rice

PROJECT DATA:
test date: JANUARY 13, 1995
obs. well: 48MW1

TEST DATA:
H0 = 4.22 ft
rc = 0.167 ft
rw = 0.413 ft
L = 30. ft
b = 50. ft
H = 43. ft

PARAMETER ESTIMATES:
K = 4.107E-05 ft/min
y0 = 3.579 ft

RAAP SWMU-48 48MW1 WITHDRAWAL

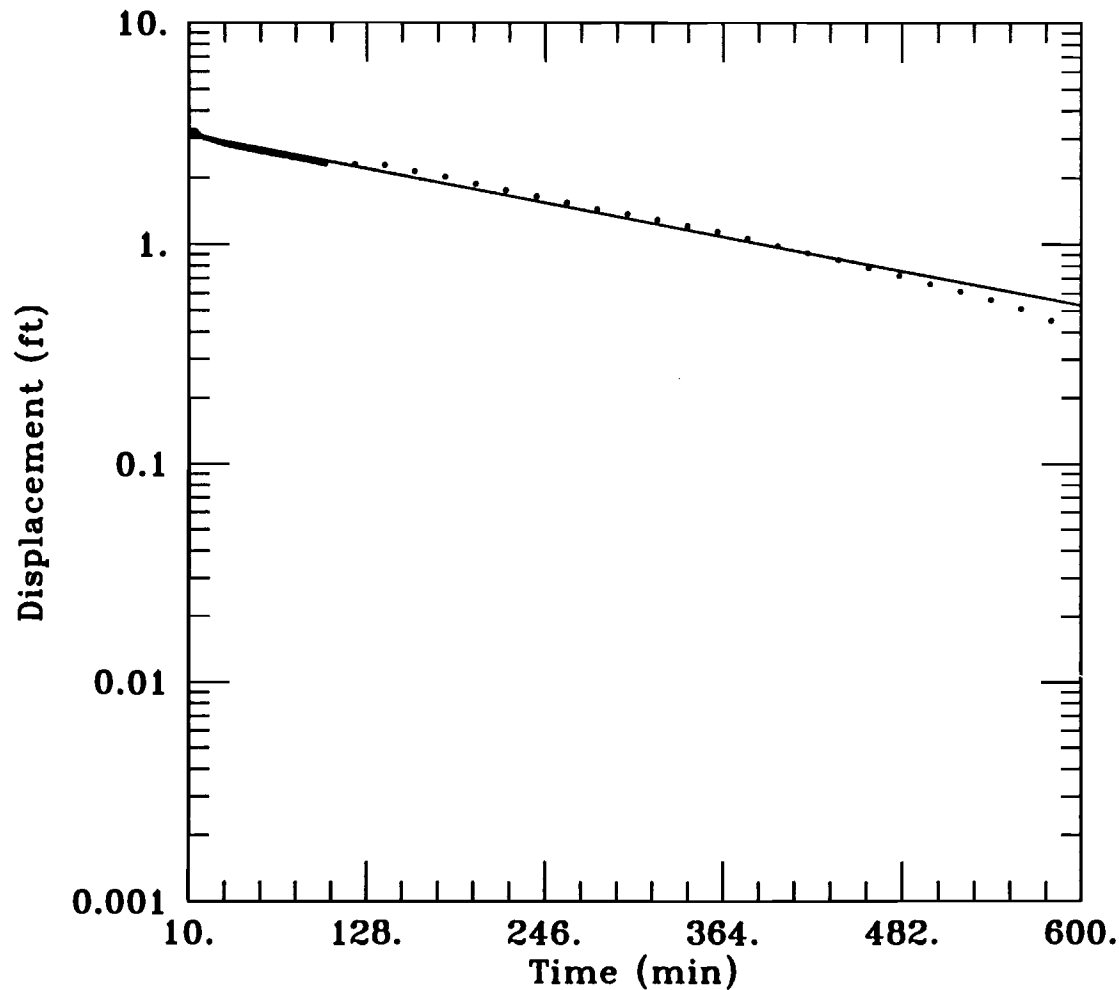
Client: USAEC

Company: PARSONS ENGINEERING SCIENCE

Location: RADFORD, VIRGINIA

Project: 722843

AGTESOLV



DATA SET:
SMU48MW2.DAT
09/03/95

AQUIFER MODEL:
Unconfined

SOLUTION METHOD:
Bouwer-Rice

PROJECT DATA:
test date: January 13, 1995
obs. well: 48MW2

TEST DATA:
H0 = 1.36 ft
rc = 0.086 ft
rw = 0.208 ft
L = 30. ft
b = 50. ft
H = 19.11 ft

PARAMETER ESTIMATES:
K = 2.923E-06 ft/min
y0 = 3.222 ft

RAAP SWMU-48 48MW2 INJECTION

Client: USAEC

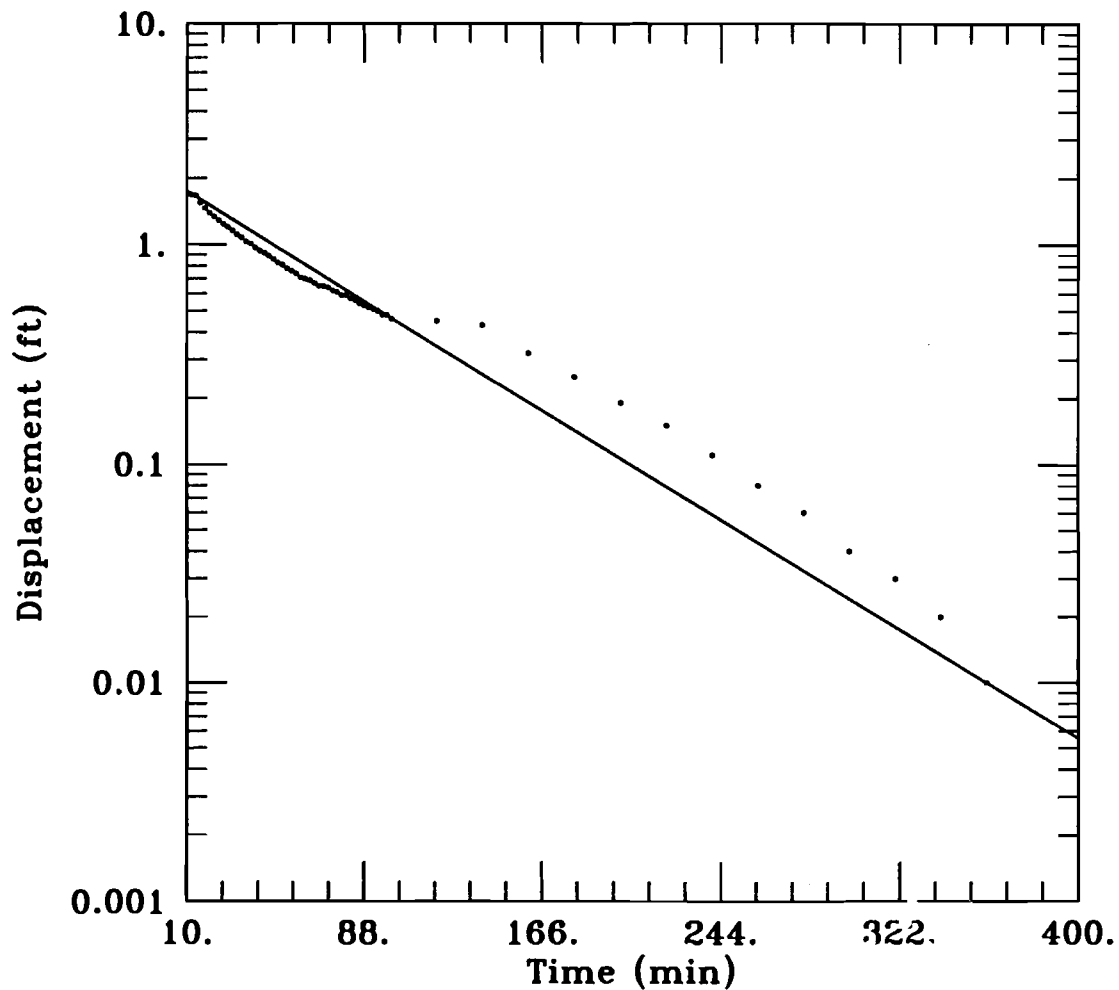
Company: **Parsons Engineering Science**

Location: **Radford, Virginia**

Project: **722483**

AQTESOLV

107



DATA SET:
SMU48MW3.DAT
09/03/95

AQUIFER MODEL:
Unconfined
SOLUTION METHOD:
Bouwer-Rice

PROJECT DATA:
test date: January 13, 1995
obs. well: 48MW3

TEST DATA:
H0 = 3.08 ft
rc = 0.167 ft
rw = 0.413 ft
L = 20. ft
b = 50. ft
H = 29.78 ft

PARAMETER ESTIMATES:
K = 7.268E-05 ft/min
y0 = 2.024 ft

RAAP SWMU-48 48MW3 INJECTION

Client: USAEC

Company: Parsons Engineering Science

Location: Radford, Virginia

Project: 722483

AQTESOLV

107

Client USAEC
 Subject Slug tests - R.A.A.P.
- FALLING HEAD/INJECTION -

Job No. 722843
 By Ben Walker
 Checked J.C. Kitchin

Sheet 1 of 1
 Date 1/12/95
 Rev. 11/7/95

Data analyzed using Bouwer - Rice (1979)
 Solution from Aqtesol v:

31MW1 INJECTION

k = hydraulic conductivity

$$K = 1.607 \times 10^{-4} \text{ ft./min.}$$

$$K = \frac{1.607 \times 10^{-4} \text{ ft.}}{\text{min.}} \times \frac{60 \text{ min.}}{1 \text{ hr.}} \times \frac{24 \text{ hr.}}{1 \text{ day}}$$

$$K = 0.231 \text{ ft./day}$$

$$= \times 3.53 \times 10^{-4} \text{ (cm/sec. conversion)}$$

$$K = 8.15 \times 10^{-5} \text{ cm/sec.}$$

T = transmissivity

$$T = kb$$

$$T = (0.231 \text{ ft./day}) \times 20 \text{ ft.}$$

$$T = 4.62 \text{ ft}^2/\text{day}$$

Client USAEC
 Subject Slug tests - R.A.A.P.
- FALLING HEAD/INJECTION -

Job No. 722843
 By Ben Wallen
 Checked J.C. [Signature]

Sheet 1 of 1
 Date 1/12/95
 Rev. 11/7/95

Data analyzed using Bouwer - Rice (1979)
 Solution from Aqtesolv :

31MW2 INJECTION

K = hydraulic conductivity

$$K = 4.158 \times 10^{-4} \text{ ft./min.}$$

$$K = \frac{4.158 \times 10^{-4} \text{ ft.}}{\text{min.}} \times \frac{60 \text{ min.}}{1 \text{ hr.}} \times \frac{24 \text{ hr.}}{1 \text{ day}}$$

$$K = 0.599 \text{ ft./day}$$

=

$\times 3.53 \times 10^{-4} \text{ (cm/sec. conversion)}$

$$K = 2.11 \times 10^{-4} \text{ cm/sec.}$$

T = transmissivity

$$T = Kb$$

$$T = (0.599 \text{ ft./day}) \times 20 \text{ ft.}$$

$$T = 11.98 \text{ ft}^2/\text{day}$$

ent USAEC
 bject Slug tests - R.A.A.P.
- FALLING HEAD/INJECTION -

Job No. 722843
 By Ben Walker
 Checked J.C. Richard

Sheet 1 of 1
 Date 1/11/95
 Rev. 11/7/95

Data analyzed using Bouwer - Rice (1979)
 Solution from Aqtesolv:

31MW3 INJECTION

k = hydraulic conductivity

$$K = 1.024 \times 10^{-5} \text{ ft./min.}$$

$$K = \frac{1.024 \times 10^{-5} \text{ ft.}}{\text{min.}} \times \frac{60 \text{ min.}}{1 \text{ hr.}} \times \frac{24 \text{ hr.}}{1 \text{ day}}$$

$$K = 0.015 \text{ ft./day}$$

=

$\times 3.53 \times 10^{-4}$ (cm/sec. conversion)

$$K = 5.30 \times 10^{-6} \text{ cm/sec.}$$

T = transmissivity

$$T = kb$$

$$T = (0.015 \text{ ft./day}) \times 20 \text{ ft.}$$

$$T = 0.30 \text{ ft}^2/\text{day}$$

Client USAEC

Job No. 722843

Sheet 1 of 1 ¹¹⁴

Subject Slug tests - R.A.A.P.

By Ben Wallen

Date 1/12/95

- FALLING HEAD/INJECTION -

Checked J.C. [Signature]

Rev. 11/7/95

Data analyzed using Bouwer - Rice (1979)
Solution from Aqtesol v:

31MW4 INJECTION

k = hydraulic conductivity

$$K = 1.161 \times 10^{-3} \text{ ft./min.}$$

$$K = \frac{1.161 \times 10^{-3} \text{ ft.}}{\text{min.}} \times \frac{60 \text{ min.}}{1 \text{ hr.}} \times \frac{24 \text{ hr.}}{1 \text{ day}}$$

$$K = 1.67 \text{ ft./day}$$

$$= \times 3.53 \times 10^{-4} \text{ (cm/sec. conversion)}$$

$$K = 5.30 \times 10^{-4} \text{ cm/sec.}$$

T = transmissivity

$$T = kb$$

$$T = (1.67 \text{ ft./day}) \times 20 \text{ ft.}$$

$$T = 33.4 \text{ ft}^2/\text{day}$$

Client USAEC
 Subject Slug tests - R.A.A.P.
- FALLINA HEAD/INJECTION -

Job No. 722843
 By Ben Walker
 Checked D.C. [Signature]

Sheet 1 of 1
 Date 1/13/95
 Rev. 11/7/95

Data analyzed using Bouwer - Rice (1979)
 Solution from Aqtesolv:

48MW1 INJECTION

K = hydraulic conductivity

$$K = 9.178 \times 10^{-5} \text{ ft./min.}$$

$$K = \frac{9.178 \times 10^{-5} \text{ ft.}}{\text{min.}} \times \frac{60 \text{ min.}}{1 \text{ hr.}} \times \frac{24 \text{ hr.}}{1 \text{ day}}$$

$$K = 0.132 \text{ ft./day}$$

=

$\times 3.53 \times 10^{-4} \text{ (cm/sec. conversion)}$

$$K = 4.66 \times 10^{-5} \text{ cm/sec.}$$

T = transmissivity

$$T = Kb$$

$$T = (0.132 \text{ ft./day}) \times 50 \text{ ft.}$$

$$T = 6.60 \text{ ft}^2/\text{day}$$

Client USAEC
 Subject Slug tests - R.A.A.P.
- FALLING HEAD/INJECTION -

Job No. 722843
 By Ben Walker
 Checked J.C. Melcher

Sheet 1 of 1
 Date 1/13/95
 Rev. 1/17/95

Data analyzed using Bouwer - Rice (1979)
 Solution from Aqtesol v:

48MW2 INJECTION

k = hydraulic conductivity

$$K = 2.923 \times 10^{-6} \text{ ft./min.}$$

$$K = \frac{2.923 \times 10^{-6} \text{ ft.}}{\text{min.}} \times \frac{60 \text{ min.}}{1 \text{ hr.}} \times \frac{24 \text{ hr.}}{1 \text{ day}}$$

$$K = 0.0042 \text{ ft./day}$$

=

$$\times 3.53 \times 10^{-4} \text{ (cm/sec. conversion)}$$

$$K = 1.48 \times 10^{-6} \text{ cm/sec.}$$

T = transmissivity

$$T = kb$$

$$T = (0.0042 \text{ ft./day}) \times 50 \text{ ft.}$$

$$T = 0.21 \text{ ft}^2/\text{day}$$

Client USAEC
 Subject Slug tests - R.A.A.P.
- FALLING HEAD/INJECTION -

Job No. 722843
 By Ben Walker
 Checked John Walker

Sheet 1 of 1
 Date 1/13/95
 Rev. 1/17/95

Data analyzed using Bouwer - Rice (1979)
 Solution from Aqtesol v:

48MW3

INJECTION

k = hydraulic conductivity

$$K = 7.268 \times 10^{-5} \text{ ft./min.}$$

$$K = \frac{7.268 \times 10^{-5} \text{ ft.}}{\text{min.}} \times \frac{60 \text{ min.}}{1 \text{ hr.}} \times \frac{24 \text{ hr.}}{1 \text{ day}}$$

$$K = 0.105 \text{ ft./day}$$

=

$\times 3.53 \times 10^{-4} \text{ (cm/sec. conversion)}$

$$k = 3.71 \times 10^{-5} \text{ cm/sec.}$$

T = transmissivity

$$T = kb$$

$$T = (0.105 \text{ ft./day}) \times 50 \text{ ft.}$$

$$T = 5.25 \text{ ft}^2/\text{day}$$

Client USAEC
 Subject Slug tests - R.A.A.P.
RISING HEAD / WITHDRAWAL

Job No. 722843
 By Ben Wallen
 Checked P.C. Kibuka

Sheet 1 of 1 ¹¹⁸
 Date 1/12/95
 Rev. 11/7/95

Data analyzed using Bouwer-Rice (1979)
 Solution from Aqtesol:

31MW3

WITHDRAWAL

$K = k_{\text{geom-12}}$
 Conductivity

$$K = 2.034 \times 10^{-5} \text{ ft./min.}$$

$$K = \frac{2.034 \times 10^{-5} \text{ ft.}}{\text{min.}} \times \frac{60 \text{ min.}}{1 \text{ hr.}} \times \frac{24 \text{ hr.}}{1 \text{ day}}$$

$$K = 0.0293 \text{ ft./day}$$

$$= \times 3.53 \times 10^{-4} (\text{cm/sec. conversion})$$

$$K = 1.03 \times 10^{-5} \text{ cm/sec}$$

$T = \text{transmissivity}$

$$T = Kb$$

$$T = (0.0293 \text{ ft./day}) \times 50 \text{ ft.}$$

$$T = 1.465 \text{ ft}^2/\text{day}$$

Client USAEC
 Subject Slug tests - R.A.A.P.
RISINK HEAD/WITHDRAWAL

Job No. 722843
 By Ben Wallen
 Checked 2. G. K. K.

Sheet 1 of 1
 Date 1/12/95
 Rev. 11/7/95

Data analyzed using Bouwer-Rice (1979)
 Solution from Aqtesol v:

3/mw4

WITHDRAWAL

$k = \text{hydraulic conductivity}$

$$k = 1.821 \times 10^{-5} \text{ ft./min.}$$

$$k = \frac{1.821 \times 10^{-5} \text{ ft.}}{\text{min.}} \times \frac{60 \text{ min.}}{1 \text{ hr.}} \times \frac{24 \text{ hr.}}{1 \text{ day}}$$

$$k = 0.026 \text{ ft./day}$$

$$= \times 3.53 \times 10^{-4} (\text{cm/sec. conversion})$$

$$k = 9.178 \times 10^{-6} \text{ cm/sec}$$

$T = \text{transmissivity}$

$$T = kb$$

$$T = (0.026 \text{ ft./day}) \times 20 \text{ ft.}$$

$$T = 0.52 \text{ ft}^2/\text{day}$$

Client USAEC
 Subject Slug tests - R.A.A.P.
RISING HEAD / WITHDRAWAL

 Job No. 722843
 By Ben Wallen
 Checked J.C. Michael

 Sheet 1 of 1²⁰
 Date 1/13/95
 Rev. 11/7/95

Data analyzed using Bouwer-Rice (1979)
 Solution from Aqtesol:

48 MWI WITHDRAWAL

K = hydraulic
 Conductivity

$$K = 4.107 \times 10^{-5} \text{ ft./min.}$$

$$K = \frac{4.107 \times 10^{-5} \text{ ft.}}{\text{min.}} \times \frac{60 \text{ min.}}{1 \text{ hr.}} \times \frac{24 \text{ hr.}}{1 \text{ day}}$$

$$K = 0.059 \text{ ft./day}$$

$$= \times 3.53 \times 10^{-4} \text{ (cm/sec. conversion)}$$

$$K = 2.08 \times 10^{-5} \text{ cm/sec}$$

T = transmissivity

$$T = Kb$$

$$T = (0.059 \text{ ft./day}) \times 50 \text{ ft.}$$

$$T = 2.95 \text{ ft}^2/\text{day}$$

PARSONS ENGINEERING SCIENCE, INC.

Client USAEC Job No. 722843 Sheet 1 of 1
 Subject R.A.A.P. - SLWA TESTS By Ben Wallen Date 11/1/95
G.W. VELOCITY Checked Ben Wallen / RZ T.C. Rev. 11/7/95
 ALK/0101

CALCULATION OF GROUNDWATER VELOCITY
FOR SWMU 31 USING
DARCY'S EQUATION

DARCY'S EQUATION: $V = Ki/n$ where:

V = G.W. Velocity

K = Hydraulic Conductivity

i = Hydraulic Gradient

n = Effective Porosity

$$V = \frac{(7.80 \times 10^{-5} \text{ cm/sec})(.01)}{(.35)}$$

$$V = 2.23 \times 10^{-6} \text{ cm/sec}$$

Conversion to ft/yr:

$$\frac{2.23 \times 10^{-6} \text{ cm}}{\text{sec}} \times \frac{60 \text{ sec}}{1 \text{ min}} \times \frac{60 \text{ min}}{1 \text{ hr}} \times \frac{24 \text{ hr}}{1 \text{ day}} \times \frac{365 \text{ days}}{1 \text{ yr}} \times \frac{1 \text{ in}}{2.54 \text{ cm}} \times \frac{1 \text{ ft}}{12 \text{ in}} =$$

$$2.31 \text{ ft/yr}$$

PARSONS ENGINEERING SCIENCE, INC.

Client USAEC Job No. 722843 Sheet 1 of 1
 Subject R.A.A.P. - SLua TESTS By Ben Wallen Date 11/1/95
G.W. VELOCITY Checked Ben Wallen / R.C. Rev. 11/7/95
 RICHARDSON

CALCULATION OF GROUNDWATER VELOCITY
FOR SWMU 48 USING
DARCY'S EQUATION

DARCY'S EQUATION: $V = Ki/n$ where:

V = G.W. Velocity

K = Hydraulic Conductivity

i = Hydraulic Gradient

n = Effective Porosity

$$V = \frac{(2.65 \times 10^{-5} \text{ cm/sec})(.125)}{(.10)}$$

$$V = 3.31 \times 10^{-5} \text{ cm/sec}$$

Conversion to ft/yr:

$$\frac{3.31 \times 10^{-5} \text{ cm}}{\text{sec}} \times \frac{60 \text{ sec}}{1 \text{ min}} \times \frac{60 \text{ min}}{1 \text{ hr}} \times \frac{24 \text{ hr}}{1 \text{ day}} \times \frac{365 \text{ days}}{1 \text{ yr}} \times \frac{1 \text{ m}}{2.54 \text{ cm}} \times \frac{1 \text{ ft}}{12 \text{ in}} =$$

$$\underline{34.25 \text{ ft/yr}}$$

APPENDIX F
GEOTECHNICAL DATA

**APPENDIX F
GEOTECHNICAL DATA
RADFORD ARMY AMMUNITION PLANT**

Sample	Depth	Description	USCS (1)	Grain Size Distribution (2)			Atterberg Limits (3)			Comments
				Percent Gravel	Percent Sand	Percent Fines	LL	PL	PI	
31MW1	10-12'	Light grey sandy silty clay	CL	0	38	62	28	18.5	9.5	
48MW3	10-12'	Brown clayey sand	SC-SM	2	60	38	27.8	22	5.8	1 of 2 samples
48MW3	10-12'	Brown clayey sand	SC-SM	2	65	33	28.8	22.5	6.3	2 of 2 samples
48SB5	10-11'	Brown silty sand with gravel	SM	15	57	28	NP	NP	NP	
48MW2	40-42'	Light grey sandy silt	ML	0	30	70	NP	NP	NP	
54SB1	15-17'	Brown silty sand	SM	0	68	32	NP	NP	NP	
54SB2	10-12'	Brown sandy silt	ML	0	47	53	NP	NP	NP	
54SB3	10-12'	Brown silty sand	SM	0	68	32	NP	NP	NP	
54SB4	5-7'	Brown sandy silt	CL-ML	0	40	60	26	21	5	
54SB5	15-17'	Brown silty sand	SM	0	52	48	NP	NP	NP	
54SB6	15-20'	Brown silty sand	SM	0	52	48	NP	NP	NP	
54SB7	10-12'	Brown silty sand	SM	0	82	18	NP	NP	NP	
54SB8	15-17'	Brown silty sand	SM	0	59	41	NP	NP	NP	
54SB9	10-12'	Brown sandy silt	ML	0	46	54	24.1	21.2	2.9	

**APPENDIX F
GEOTECHNICAL DATA
RADFORD ARMY AMMUNITION PLANT**

Sample	Depth	Description	USCS (1)	Grain Size Distribution (2)			Atterberg Limits (3)			Comments
				Percent Gravel	Percent Sand	Percent Fines	LL	PL	PI	
54SB10	10-12'	Brown silty sand	SM	0	63	37	NP	NP	NP	
54SB11	15-17'	Brown silty sand	SM	0	63	37	NP	NP	NP	
54SB12	5-7'	Brown sandy lean clay	CL-ML	0	42	58	23.2	18	5.2	
54SB13	5-7'	Brown silty sand	SM	0	48	52	NP	NP	NP	
54SB14	7-9'	Brown silty sand	SM	0	75	25	NP	NP	NP	
54SB16	10-12'	Brown silty sand	SM	0	71	29	NP	NP	NP	
BG1BUC3	3-5'	Brown silty sand some clay	SM	0	81	19	33	19	4	
BG4CUC17	15-17'	Brown sandy silt	ML	3	41	56	29	24	5	
BG8BUC5	3-5'	Brown silty sand some clay	SM	0	61	39	41	28	13	
BG8CUC10	8-10'	Brown silty gravel with sand	GM	35	33	32	36	26	10	
BG3CWL22	20-22'	Brown sandy silt	ML	0	17	83	NP	NP	NP	
BG5BWL3	1-3'	Brown clayey silt	SC	0	71	29	32	19	13	
BG5CWL8	6-8'	Dark brown silty sand	CL	0	41	59	30	20	10	
BG6BWL4	2-4'	Brown clayey silt	SC	0	64	36	31	20	11	

**APPENDIX F
GEOTECHNICAL DATA
RADFORD ARMY AMMUNITION PLANT**

Sample	Depth	Description	USCS (1)	Grain Size Distribution (2)			Atterberg Limits (3)			Comments
				Percent Gravel	Percent Sand	Percent Fines	LL	PL	PI	
BG1BBL4	2-4'	Brown clayey sandy silt	SC	0	57	43	28	16	12	
BG1CBL10	8-10'	Brown silty sand	SM	0	52	48	30	25	5	
BG2CBL17	15-17'	Brown clayey silt	SC	0	61	39	32	22	10	
BG4BBL5	3-5'	Brown lean clay with sand	CL	2	27	71	26	18	8	

(1) USCS: Unified Soil Classification System

(2) Grain Size Distribution:

Gravel: Particles of rock that are retained on a 4.75 mm (No. 4) sieve.

Sand: Particles that will pass a 4.75 mm sieve, but are retained on a 0.075 mm (No. 200) sieve.

Fines: Include silt and sand. Particles that will pass a 0.075 mm (No. 200) sieve.

(3) Atterberg Limits:

LL: Liquid Limit

PL: Plasticity Limit

PI: Plasticity Index (PI = LL - PL)

NP: Nonplastic

VISUAL MANUAL SOIL CLASSIFICATION DATA SUMMARY

Sample ID	BG1CWL8	BG2CWL12	BG4BWL4	BG5CWL8	BG5BWL3	BG6CWL17	BG4CWL17	BG1BBL4
Group Symbol	CL	CL	CH	CL	CL	ML	ML	
Color	Light Brown	Light Brown\ Gray-Brown	Brown	Dark Red-Brown	Light Brown	Brown	Brown	Red-Brown
Odor	None	None	None	None	None	None	None	None
Moisture Content	Moist	Moist	Moist	Moist	Moist	Moist to Wet	Moist	Moist
HCI Reaction	None	None	None	None	None	None	None	None
Consistency	Soft	Firm	Hard	Firm	Firm	Soft	Soft	Firm
Cementation	Moderate	Moderate	Moderate	Moderate	Moderate	Weak	Weak	Moderate
Structure	Stratified	Stratified	Homogeneous	Homogeneous	Stratified	Stratified	Homogeneous	Stratified
Maximum Particle size	Fine Sand	Fine Sand	Fine Sand	Fine Sand	Fine Sand	Medium Sand	Coarse gravel	Fine Sand
Dry Strength	Very High	Very High	Very High	Very High	Very High	N/A	N/A	Very High
Dilatancy	None	None	None	None	None	N/A	N/A	None
Toughness	Medium	Medium	High	Medium	Medium	N/A	N/A	Low
Plasticity	Low	Low	High	Low	Low	N/A	N/A	Non-Plastic
Angularity	N/A	N/A	N/A	N/A	N/A	Subangular	Subrounded	N/A
Size Range	N/A	N/A	N/A	N/A	N/A	fine-med. sand	sand-gravel	N/A
Hardness	N/A	N/A	N/A	N/A	N/A	Hard	Hard	N/A
Other	Minor oxide staining				Dark red Mottling	Soil at bedrock interface		Black oxide staining

VISUAL MANUAL SOIL CLASSIFICATION DATA SUMMARY

Sample ID	Group	Symbol	Color	Odor	Moisture Content	HCl Reaction	Consistency	Cementation	Structure	Maximum Particle size	Dry Strength	Dilatancy	Toughness	Plasticity	Angularity	Size Range	Hardness	Other
BG1CBL10		CL	Red-Brown	None	Moist	None	Soft	Moderate	Homogeneous	Fine Sand	High	None	Medium	Medium	N/A	N/A	N/A	Some black oxide staining
BG2BBL5		CL	Brown to Red-Brown	None	Moist	None	Soft	Weak	Homogeneous	Fine Sand	Very High	Slow	Medium	Low	N/A	N/A	N/A	
BG3BBL3		CH	Dark Brown to Black	Organic Decay	Moist	None	Soft	Weak	Stratified	Silt	Very High	None	High	Low	N/A	N/A	N/A	Small sized roots in soil
BG3CBL22		MH	Light brown to Red-Brown	None	Moist	None	Firm	Moderate	Homogeneous	Fine Sand	Medium	Slow	Low	Low	N/A	N/A	N/A	Black oxide staining
BG4BBL5		CH	Light brown	None	Moist	None	Soft	Weak	Homogeneous	Fine Sand	Medium	Slow	Low	Low	N/A	N/A	N/A	Black oxide staining
BG3CUC22		MH	Brown	None	Moist	None	Hard	Moderate	Homogeneous	Medium Sand	Medium	Slow	Low	Non-plastic	N/A	N/A	N/A	Very Micaceous
BG3CUC3		CL	Red-Brown	Organic Decay	Moist	None	Soft	Weak	Homogeneous	Fine Sand	Very High	None	Medium	Medium	N/A	N/A	N/A	Small sized roots in soil
BG4BUC5		CL	Dark brown to Light brown	None	Moist	None	Firm	Moderate	Stratified	Medium Sand	Very High	None	Medium	Low	N/A	N/A	N/A	Heavy mottling fill material?

APPENDIX G
DATA SUMMARY TABLES

DATA SUMMARY TABLES FOR JANUARY 1995 SAMPLING EVENT

Field Sample Number ->	SCSW1	SCSW2	SCSW3	17AFBSO	48EQSO	48TBSO		54TBSO		SCEQSE		SCTBAQ	
Lab Analysis Number ->	UC00196	UC00197	UC00198	UB06523	UB06570	UB06571		UB06630		UC00201		UC00202	
Volatile Organics (ug/L)													
1,1,1-Trichloroethane	1 U	1 U	1 U	1 U	1.1	1.2		1.4		1 U		1 U	
1,1,2-Trichloroethane	1 U	1 U	1 U	1 U	1 U	1 U		1 U		1 U		1 U	
1,1-Dichloroethene	1 U	1 U	1 U	1 U	1 U	1 U		1 U		1 U		1 U	
1,1-Dichloroethane	1 U	1 U	1 U	1 U	1 U	1 U		1 U		1 U		1 U	
*1,2-DICHLOROETHYLENES (Total)	5 U	5 U	5 U	5 U	5 U	5 U		5 U		5 U		5 U	
1,2-Dichloroethane	1 U	1 U	1 U	1 U	1 U	3.5		6.1		1 U		1 U	
1,2-Dichloropropane	1 U	1 U	1 U	1 U	1 U	1 U		1 U		1 U		1 U	
Acetone	8 U	8 U	8 U	8 U	8 U	32		27		8 U		8 U	
Acrylonitrile	8.4 U	8.4 U	8.4 U	8.4 U	8.4 U	8.4 U		8.4 U		8.4 U		8.4 U	
Bromodichloromethane	1 U	1 U	1 U	1 U	1 U	1 U		1 U		1 U		1 U	
Vinyl chloride	12 U	12 U	12 U	12 U	12 U	12 U		12 U		12 U		12 U	
Chloroethane	8 U	8 U	8 U	8 U	8 U	8 U		8 U		8 U		8 U	
Benzene	1 U	1 U	1 U	1 U	1 U	1 U		1 U		1 U		1 U	
Trichlorofluoromethane	1 U	1 U	1 U	1 U	1 U	1 U		1 U		1 U		1 U	
Carbon tetrachloride	1 U	1 U	1 U	1 U	1 U	1 U		1 U		1 U		1 U	
Methylene chloride	1 U	1 U	1 U	3.3	1 U	4.5		3.4		1 U		3.3	
Bromomethane	14 U	14 U	14 U	14 U	14 U	14 U		14 U		14 U		14 U	
Chloromethane	1.2 U	1.2 U	1.2 U	1.2 U	1.2 U	1.2 U		1.2 U		1.2 U		1.2 U	
Bromoform	11 U	11 U	11 U	11 U	11 U	11 U		11 U		11 U		11 U	
Chloroform	1 U	1 U	1 U	1 U	1 U	1 U		1 U		1 U		1 U	
Chlorobenzene	1 U	1 U	1 U	1 U	1 U	1 U		1 U		1 U		1 U	
Ethylbenzene	1 U	1 U	1 U	1 U	1 U	1 U		1 U		1 U		1 U	
Toluene	1 U	1 U	1 U	1 U	1 U	1 U		1 U		1 U		1 U	
2-BUTANONE	10 U	10 U	10 U	10 U	10 U	10 U		10 U		10 U		10 U	
4-METHYL-2-PENTANONE	1.4 U	1.4 U	1.4 U	1.4 U	1.4 U	1.4 U		1.4 U		1.4 U		1.4 U	
1,1,2,2-Tetrachloroethane	1.5 U	1.5 U	1.5 U	1.5 U	1.5 U	1.5 U		1.5 U		1.5 U		1.5 U	
Tetrachloroethylene	1 U	1 U	1 U	1 U	1 U	1 U		1 U		1 U		1 U	
Trichloroethylene	1 U	1 U	1 U	1 U	1 U	1 U		1 U		1 U		1 U	
*XYLENES	2 U	2 U	2 U	2 U	2 U	2 U		2 U		2 U		2 U	

Field Sample Number ->	48MW1	48MW2	48MW3	SCSW1	SCSW2	SCSW3	17AFBSO	48EQGW	48EQSO	SCEQSE
Lab Analysis Number ->	UC00247	UC00245	UC00248	UC00196	UC00197	UC00198	UB06523	UC00246	UB06570	UC00201
Semivolatile Organics (ug/L)										
1,2,4-Trichlorobenzene	2.4 U	2.4 U	2.4 U	2.4 U	2.4 U	2.4 U	2.4 U	2.4 U	2.4 U	2.4 U
1,2-Dichlorobenzene	1.2 U	1.2 U	1.2 U	1.2 U	1.2 U	1.2 U	1.2 U	1.2 U	1.2 U	1.2 U
1,3-Dichlorobenzene	3.4 U	3.4 U	3.4 U	3.4 U	3.4 U	3.4 U	3.4 U	3.4 U	3.4 U	3.4 U
1,4-Dichlorobenzene	1.5 U	1.5 U	1.5 U	1.5 U	1.5 U	1.5 U	1.5 U	1.5 U	1.5 U	1.5 U
2,4,5-Trichlorophenol	2.8 U	2.8 U	2.8 U	2.8 U	2.8 U	2.8 U	2.8 U	2.8 U	2.8 U	2.8 U
2,4,6-Trichlorophenol	3.6 U	3.6 U	3.6 U	3.6 U	3.6 U	3.6 U	3.6 U	3.6 U	3.6 U	3.6 U
2,4-Dichlorophenol	8.4 U	8.4 U	8.4 U	8.4 U	8.4 U	8.4 U	8.4 U	8.4 U	8.4 U	8.4 U
2,4-Dimethylphenol	4.4 U	4.4 U	4.4 U	4.4 U	4.4 U	4.4 U	4.4 U	4.4 U	4.4 U	4.4 U
2,4-Dinitrophenol	180 U	180 U	180 U	180 U	180 U	180 U	180 U	180 U	180 U	180 U
2,4-Dinitrotoluene	5.8 U	5.8 U	5.8 U	5.8 U	5.8 U	5.8 U	5.8 U	5.8 U	5.8 U	5.8 U
2,6-Dinitrotoluene	6.7 U	6.7 U	6.7 U	6.7 U	6.7 U	6.7 U	6.7 U	6.7 U	6.7 U	6.7 U
2-Chlorophenol	2.8 U	2.8 U	2.8 U	2.8 U	2.8 U	2.8 U	2.8 U	2.8 U	2.8 U	2.8 U
2-Chloronaphthalene	2.6 U	2.6 U	2.6 U	2.6 U	2.6 U	2.6 U	2.6 U	2.6 U	2.6 U	2.6 U
2-Methylphenol	3.6 U	3.6 U	3.6 U	3.6 U	3.6 U	3.6 U	3.6 U	3.6 U	3.6 U	3.6 U
3,3'-Dichlorobenzidine	5 U	5 U	5 U	5 U	5 U	5 U	5 U	5 U	5 U	5 U
4,6-Dinitro-2-cresol	50 U	50 U	50 U	50 U	50 U	50 U	50 U	50 U	50 U	50 U
4-BROMOPHENYLPHENYL ETHER	22 U	22 U	22 U	22 U	22 U	22 U	22 U	22 U	22 U	22 U
3-METHYL-4-CHLOROPHENOL	8.5 U	8.5 U	8.5 U	8.5 U	8.5 U	8.5 U	8.5 U	8.5 U	8.5 U	8.5 U
4-Methylphenol	2.8 U	2.8 U	2.8 U	2.8 U	2.8 U	2.8 U	2.8 U	2.8 U	2.8 U	2.8 U
4-Nitrophenol	96 U	96 U	96 U	96 U	96 U	96 U	96 U	96 U	96 U	96 U
Anthracene	5.2 U	5.2 U	5.2 U	5.2 U	5.2 U	5.2 U	5.2 U	5.2 U	5.2 U	5.2 U
Bis (2-chloroethoxy) methane	6.8 U	6.8 U	6.8 U	6.8 U	6.8 U	6.8 U	6.8 U	6.8 U	6.8 U	6.8 U
Bis (2-chloroisopropyl) ether	5 U	5 U	5 U	5 U	5 U	5 U	5 U	5 U	5 U	5 U
Bis (2-chloroethyl) ether	0.68 U	0.68 U	0.68 U	0.68 U	0.68 U	0.68 U	0.68 U	0.68 U	0.68 U	0.68 U
Bis (2-ethylhexyl) phthalate	7.7 U	12	23	7.7 U	7.7 U	7.7 U	7.7 U	7.7 U	7.7 U	7.7 U
Benzo[a]anthracene	9.8 U	9.8 U	9.8 U	9.8 U	9.8 U	9.8 U	9.8 U	9.8 U	9.8 U	9.8 U
Benzo[a]pyrene	14 U	14 U	14 U	14 U	14 U	14 U	14 U	14 U	14 U	14 U
Benzo[b]fluoranthene	10 U	10 U	10 U	10 U	10 U	10 U	10 U	10 U	10 U	10 U
Butylbenzyl phthalate	28 U	28 U	28 U	28 U	28 U	28 U	28 U	28 U	28 U	28 U
Benzo[k]fluoranthene	10 U	10 U	10 U	10 U	10 U	10 U	10 U	10 U	10 U	10 U
Chrysene	7.4 U	7.4 U	7.4 U	7.4 U	7.4 U	7.4 U	7.4 U	7.4 U	7.4 U	7.4 U
Hexachlorobenzene	12 U	12 U	12 U	12 U	12 U	12 U	12 U	12 U	12 U	12 U
Hexachlorocyclopentadiene	54 U	54 U	54 U	54 U	54 U	54 U	54 U	54 U	54 U	54 U
Hexachloroethane	8.3 U	8.3 U	8.3 U	8.3 U	8.3 U	8.3 U	8.3 U	8.3 U	8.3 U	8.3 U
Dibenz[ah]anthracene	12 U	12 U	12 U	12 U	12 U	12 U	12 U	12 U	12 U	12 U
Diethyl phthalate	5.9 U	5.9 U	5.9 U	5.9 U	5.9 U	5.9 U	5.9 U	5.9 U	5.9 U	5.9 U
Dimethyl phthalate	2.2 U	2.2 U	2.2 U	2.2 U	2.2 U	2.2 U	2.2 U	2.2 U	2.2 U	2.2 U
Di-n-butyl phthalate	33 U	33 U	33 U	33 U	33 U	33 U	33 U	33 U	33 U	33 U
Di-n-octyl phthalate	1.5 U	1.5 U	1.5 U	1.5 U	1.5 U	1.5 U	1.5 U	1.5 U	1.5 U	1.5 U

Field Sample Number ->	48MW1		48MW2		48MW3		SCSW1		SCSW2		SCSW3		17AFB50		48EQGW		48EQSO		SCEQSE	
Lab Analysis Number ->	UC00247		UC00245		UC00248		UC00196		UC00197		UC00198		UB06523		UC00246		UB06570		UC00201	
Semivolatile Organics (ug/L)																				
Fluoranthene	24 U		24 U		24 U		24 U		24 U		24 U		24 U		24 U		24 U		24 U	
Hexachlorobutadiene	8.7 U		8.7 U		8.7 U		8.7 U		8.7 U		8.7 U		8.7 U		8.7 U		8.7 U		8.7 U	
Indeno[1,2,3-C,D]pyrene	21 U		21 U		21 U		21 U		21 U		21 U		21 U		21 U		21 U		21 U	
Naphthalene	0.5 U		0.5 U		0.5 U		0.5 U		0.5 U		0.5 U		0.5 U		0.5 U		0.5 U		0.5 U	
Nitrobenzene	3.7 U		3.7 U		3.7 U		3.7 U		3.7 U		3.7 U		3.7 U		3.7 U		3.7 U		3.7 U	
N-Nitrosodi-n-propylamine	6.8 U		6.8 U		6.8 U		6.8 U		6.8 U		6.8 U		6.8 U		6.8 U		6.8 U		6.8 U	
N-Nitrosodiphenylamine	3.7 U		3.7 U		3.7 U		3.7 U		3.7 U		3.7 U		3.7 U		3.7 U		3.7 U		3.7 U	
Pentachlorophenol	9.1 U		9.1 U		9.1 U		9.1 U		9.1 U		9.1 U		9.1 U		9.1 U		9.1 U		9.1 U	
Phenanthrene	9.9 U		9.9 U		9.9 U		9.9 U		9.9 U		9.9 U		9.9 U		9.9 U		9.9 U		9.9 U	
Phenol	2.2 U		2.2 U		2.2 U		2.2 U		2.2 U		2.2 U		2.2 U		2.2 U		2.2 U		2.2 U	
Pyrene	17 U		17 U		17 U		17 U		17 U		17 U		17 U		17 U		17 U		17 U	

Field Sample Number ->	17PZ1		17MW2		17MW3		40MW3		SPG3SW1		SCSW1		SCSW2		SCSW3		17AFB80	
Lab Analysis Number ->	UC00208		UC00209		UC00244		UC00243		UC00131		UC00196		UC00197		UC00198		UB06523	
Explosives (ug/L)																		
2,4,6-Trinitrotoluene	0.426 UJ4		0.426 UJ4		0.426 UJ4		0.426 UJ4		0.426 UJ4		0.426 UJ4		0.426 UJ4		0.426 UJ4		0.426 UJ4	
2,4-Dinitrotoluene	0.397 UJ4		0.397 UJ4		0.397 UJ4		0.397 UJ4		0.397 UJ4		0.397 UJ4		0.397 UJ4		0.397 UJ4		0.397 UJ4	
2,6-Dinitrotoluene	0.6 U		0.6 U		0.6 U		0.6 U		0.6 U		0.6 U		0.6 U		0.6 U		0.6 U	
Cyclotetramethylenetetranitramine	0.533 U		0.533 U		0.533 U		0.533 U		0.533 U		5.3 J9		5.3 J9		5.3 J9		0.533 U	
Cyclonite (RDX)	0.416 UJ4		0.416 UJ4		0.416 UJ4		0.416 UJ4		0.416 UJ4		0.416 UJ4		0.416 UJ4		0.416 UJ4		0.416 UJ4	
TETRYL	0.631 U		0.631 U		0.631 U		0.631 U		0.631 U		0.631 U		0.631 U		0.631 U		0.631 U	

Field Sample Number ->	17FBAQGW		48EQSO		54EQS02		54EQSO		54FBSO		SCEQSE		SPG3FBAQ		SPG3FBSE	
Lab Analysis Number ->	UC00210		UB06570		UB06649		UB06628		UB06629		UC00201		UC00199		UC00200	
Explosives (ug/L)																
2,4,6-Trinitrotoluene	0.426 UJ4		0.426 UJ4		0.426 UJ4		0.727 J4		0.426 UJ4		0.426 UJ4		0.426 UJ4		0.426 UJ4	
2,4-Dinitrotoluene	0.397 UJ4		0.397 UJ4		0.397 UJ4		0.397 UJ4		0.397 UJ4		0.397 UJ4		0.397 UJ4		0.397 UJ4	
2,6-Dinitrotoluene	0.6 U		0.6 U		0.6 U		0.6 U		0.6 U		0.6 U		0.6 U		0.6 U	
Cyclotetramethylenetetranitramine	0.533 U		0.533 U		0.533 U		0.533 U		0.533 U		0.533 U		0.533 U		0.533 U	
Cyclonite (RDX)	0.416 UJ4		0.416 UJ4		0.416 UJ4		0.416 UJ4		0.416 UJ4		0.416 UJ4		0.416 UJ4		0.416 UJ4	
TETRYL	0.631 U		0.631 U		0.631 U		0.631 U		0.631 U		0.631 U		0.631 U		0.631 U	

Field Sample Number ->	17PE1		17MW2		17MW3*		40MW3*		SPG3SW1		31MW1		31MW2		31MW3
Lab Analysis Number ->	UC00208		UC00209		UC00244		UC00243		UC00131		UC00207		UC00203		UC00204
Metals (ug/L)															
Arsenic	2.35 UJ4		2.35 UJ4		2.35 UJ4		2.35 UJ4		2.35 UJ4		2.35 UJ4		2.35 UJ4		2.35 UJ4
Mercury	0.1 UJ4		0.1 UJ4		0.1 U		0.1 U		0.1 UJ4		0.1 UJ4		0.1 UJ4		0.1 UJ4
Lead	4.47 UJ4		4.47 UJ4		4.47 UJ4		4.47 UJ4		25.2 J4		4.47 UJ4		4.47 UJ4		4.47 UJ4
Selenium	2.53 U		2.53 U		2.53 UJ4		2.53 UJ4		2.53 U		2.53 U		2.53 U		2.53 U
Silver	0.333 UJ4		0.333 UJ4		0.333 UJ4		0.333 UJ4		0.333 UJ4		0.333 UJ4		0.333 UJ4		0.333 UJ4
Barium	117 J4		63.2 J4		167 UJ4		32.5 UJ4		26.6 J4		222 J4		23.7 J4		38.1 J4
Beryllium	4.66		4.1		4.72 U		2.47 U		1.64		3.84		1.56		1.86
Cadmium	6.78 UJ4		6.78 UJ4		6.78 UJ4		6.78 UJ4		6.78 UJ4		6.78 UJ4		6.78 UJ4		6.78 UJ4
Chromium	16.8 UJ4		16.8 UJ4		16.8 UJ4		16.8 UJ4		16.8 UJ4		16.8 UJ4		16.8 UJ4		16.8 UJ4
Nickel	32.1 UJ4U		32.1 UJ4		32.1 UJ4		32.1 UJ4		32.1 UJ4		32.1 UJ4		32.1 UJ4		32.1 UJ4
Antimony	60 U		60.2		60 U		60 U		60 U		65.2		60 U		60 U
Thallium	125 U		125 U		125 UJ4		125 UJ4		125 U		125 U		125 U		125 U
Field Sample Number ->	17PE1		17MW2		17MW3		40MW3		SPG3SW1		31MW1		31MW2		31MW3
Lab Analysis Number ->	UC00208		UC00209		UC00244		UC00243		UC00131		UC00207		UC00203		UC00204
*TOTAL ORGANIC CARBON (ug/L)	1000 U		1000 U		1240		1000 U		1200		2040		1320		1160
*TOTAL ORGANIC HALOGENS (ug/L)	15.7		27.5		107		63.9		10 U		15.4		15		25.3
*TOTAL HARDNESS (ug/L)	445000 *		268000 *		368000 *		148000		152000		153000		818 *		
TOTAL PETROLEUM HYDROCARBONS (ug/L)	143		480		247		100 U		100 U						

Sheet1

Field Sample Number ->	31MW4	31MW5	48MW1*	48MW2*	48MW3*	SCSW1	SCSW2	SCSW3						
Lab Analysis Number ->	UC00205	UC00206	UC00247	UC00245	UC00248	UC00196	UC00197	UC00198						
Metals (ug/L)														
Arsenic	2.35 UJ4	2.35 UJ4	2.35 UJ4	2.35 UJ4	2.35 UJ4	2.35 UJ4	2.35 UJ4	2.35 UJ4	2.35 UJ4	2.35 UJ4	2.35 UJ4	2.35 UJ4	2.35 UJ4	2.35 UJ4
Mercury	0.1 UJ4	0.1 UJ4	0.1 U	0.1 U	0.1 U	0.1 U	0.1 UJ4	0.1 UJ4	0.1 UJ4	0.1 UJ4	0.1 UJ4	0.1 UJ4	0.1 UJ4	0.1 UJ4
Lead	4.47 UJ4	4.47 UJ4	4.47 UJ4	4.47 UJ4	4.47 UJ4	4.47 UJ4	4.47 UJ4	4.47 UJ4	4.47 UJ4	4.47 UJ4	4.47 UJ4	4.47 UJ4	4.47 UJ4	4.47 UJ4
Selenium	2.53 U	2.53 U	2.53 UJ4	2.53 UJ4	2.53 UJ4	2.53 UJ4	2.53 U	2.53 U	2.53 U	2.53 U	2.53 U	2.53 U	2.53 U	2.53 U
Silver	0.333 UJ4	0.333 UJ4	0.333 UJ4	0.333 UJ4	0.333 UJ4	0.333 UJ4	0.333 UJ4	0.333 UJ4	0.333 UJ4	0.333 UJ4	0.333 UJ4	0.333 UJ4	0.333 UJ4	0.333 UJ4
Barium	29.2 J4	42.8 J4	67 UJ4	215 UJ4	91.9 UJ4	44.7 J4	47.3 J4	48 J4	48 J4	48 J4	48 J4	48 J4	48 J4	48 J4
Beryllium	1.1 J5	2.43	4.18 U	2.22 U	3.17 U	1.95	2.22	2.23	2.23	2.23	2.23	2.23	2.23	2.23
Cadmium	6.78 UJ4	6.78 UJ4	6.78 UJ4	6.78 UJ4	6.78 UJ4	6.78 UJ4	6.78 UJ4	6.78 UJ4	6.78 UJ4	6.78 UJ4	6.78 UJ4	6.78 UJ4	6.78 UJ4	6.78 UJ4
Chromium	16.8 UJ4	16.8 UJ4	16.8 UJ4	16.8 UJ4	16.8 UJ4	16.8 UJ4	16.8 UJ4	30.9 J4	16.8 UJ4	16.8 UJ4	16.8 UJ4	16.8 UJ4	16.8 UJ4	16.8 UJ4
Nickel	32.1 UJ4	32.1 UJ4	32.1 UJ4	32.1 UJ4	32.1 UJ4	32.1 UJ4	32.1 UJ4	32.1 UJ4	32.1 UJ4	32.1 UJ4	32.1 UJ4	32.1 UJ4	32.1 UJ4	32.1 UJ4
Antimony	60 U	60 U	60 U	60 U	60 U	60 U	60 U	60 U	60 U	60 U	60 U	60 U	60 U	60 U
Thallium	125 U	125 U	125 UJ4	125 UJ4	125 UJ4	125 UJ4	125 U	125 U	125 U	125 U	125 U	125 U	125 U	125 U
Field Sample Number ->	31MW4	31MW5	48MW1	48MW2	48MW3	SCSW1	SCSW2	SCSW3						
Lab Analysis Number ->	UC00205	UC00206	UC00247	UC00245	UC00248	UC00196	UC00197	UC00198						
*TOTAL ORGANIC CARBON (ug/L)	1000 U	1350	1000 U	2620	1610	2690	2490 J7	2370						
*TOTAL ORGANIC HALOGENS (ug/L)	15.6	33.4	13.7	33.6	178	16.9	18 J7	16						
*TOTAL HARDNESS (ug/L)														
TOTAL PETROLEUM HYDROCARBONS (ug/L)														

Field Sample Number ->	17AFBSO	17FBAQGW	31MWEQSO	31MWFBSO	48EQGW*	48EQSO	54EQSO1	54EQSO2	
Lab Analysis Number ->	UB06523	UC00210	UB06522	UB06521	UC00246	UB06570	UB06628	UB06649	
Metals (ug/L)									
Arsenic	2.35 UJ4	2.35 UJ4	2.35 UJ4	2.35 UJ4	2.35 UJ4	2.35 UJ4	2.35 UJ4	2.35 UJ4	
Mercury	0.1 UJ4	0.1 UJ4	0.1 UJ4	0.1 UJ4	0.1 U	0.1 UJ4	0.1 UJ4	0.1 UJ4	
Lead	4.47 UJ4	4.47 UJ4	4.47 UJ4	4.47 UJ4	4.47 UJ4	4.47 UJ4	10.3 UJ4	4.47 UJ4	
Selenium	2.53 UJ4	2.53 U	2.53 UJ4	2.53 UJ4	2.53 UJ4	2.53 UJ4	2.53 U	2.53 U	
Silver	0.333 UJ4	0.333 UJ4	0.333 UJ4	0.333 UJ4	0.333 UJ4	0.333 UJ4	0.333 UJ4	0.333 UJ4	
Barium	2.82 UJ4	2.82 UJ4	2.82 UJ4	2.82 UJ4	2.82 UJ4	2.82 UJ4	43.7 UJ4	2.82 UJ4	
Beryllium	1.12 U	1.12 U	1.12 U	1.12 U	1.12 U	1.12 U	1.12 U	1.12 U	
Cadmium	6.78 UJ4	6.78 UJ4	6.78 UJ4	6.78 UJ4	6.78 UJ4	6.78 UJ4	6.78 UJ4	6.78 UJ4	
Chromium	16.8 UJ4	16.8 UJ4	16.8 UJ4	16.8 UJ4	16.8 UJ4	16.8 U.4	47.6 J4	16.8 UJ4	
Nickel	32.1 UJ4	32.1 UJ4	32.1 UJ4	32.1 UJ4	32.1 UJ4	32.1 UJ4	32.1 UJ4	32.1 UJ4	
Antimony	60 U	60 U	60 U	60 U	60 U	60 U	60 U	60 U	
Thallium	125 U	125 U	125 U	125 U	125 UJ4	125 U	125 U	125 U	
Field Sample Number ->	17FBAQGW	48EQGW	48EQSO	54EQSO	54EQSO2	54FBSO	SCEQSE	SPG3FBAQ	
Lab Analysis Number ->	UC00210	UC00246	UB06570	UB06628	UB06649	UB06629	UC00201	UC00199	
*TOTAL ORGANIC CARBON (ug/L)	1000 U	1000 U	110 U	646	110 U	200	1000 U	1000 U	
*TOTAL ORGANIC HALOGENS (ug/L)	10 U	10 U	10 U	10 U	10 U				
*TOTAL HARDNESS (ug/L)									
TOTAL PETROLEUM HYDROCARBONS (ug/L)									

Field Sample Number ->	54EQSOWA		54FBSO		SCEQSE		SPG3FBAQ		SPG3FBSE
Lab Analysis Number ->	UB06627		UB06629		UC00201		UC00199		UC00200
Metals (ug/L)									
Arsenic	2.35 UJ4		2.35 UJ4		2.35 UJ4		2.35 UJ4		2.35 UJ4
Mercury	0.1 UJ4		0.1 UJ4		0.1 UJ4		0.1 UJ4		0.1 UJ4
Lead	4.47 UJ4		4.47 UJ4		4.47 UJ4		4.47 UJ4		4.47 UJ4
Selenium	2.53 U		2.53 U		2.53 U		2.53 U		2.53 U
Silver	0.333 UJ4		0.333 UJ4		0.333 UJ4		0.333 UJ4		0.333 UJ4
Barium	2.82 UJ4		2.82 UJ4		2.82 UJ4		2.82 UJ4		2.82 UJ4
Beryllium	1.12 U		1.12 U		1.12 U		1.12 U		1.12 U
Cadmium	6.78 UJ4		6.78 UJ4		6.78 UJ4		6.78 UJ4		6.78 UJ4
Chromium	16.8 UJ4		16.8 UJ4		16.8 UJ4		16.8 UJ4		16.8 UJ4
Nickel	32.1 UJ4		32.1 UJ4		32.1 UJ4		32.1 UJ4		32.1 UJ4
Antimony	60 U		60 U		60 U		60 U		60 U
Thallium	125 U		125 U		125 U		125 U		125 U
Field Sample Number ->	SPG3FBSE								
Lab Analysis Number ->	UC00200								
*TOTAL ORGANIC CARBON (ug/L)	1000 U								
*TOTAL ORGANIC HALOGENS (ug/L)									
*TOTAL HARDNESS (ug/L)									
TOTAL PETROLEUM HYDROCARBONS (ug/L)									

Field Sample Number ->	17ASB105	17ASB122	17ASB205	17ASB225	17ASB305	17ASB325	17ASB340
Lab Analysis Number ->	UB06429	UB06433	UB06435	UB06439	UB06442	UB06446	UB06447
Volatile Organics (ug/g)							
1,1,1-Trichloroethane	0.26 U	0.26 U	0.25 U	0.29 U	0.30 U	0.22 U	0.22 U
1,1,2-Trichloroethane	0.42 U	0.43 U	0.41 U	0.47 U	0.50 U	0.36 U	0.36 U
1,1-Dichloroethene	0.35 U	0.35 U	0.34 U	0.39 U	0.41 U	0.30 U	0.30 U
1,1-Dichloroethane	0.63 U	0.64 U	0.61 U	0.70 U	0.74 U	0.54 U	0.54 U
*1,2-DICHLOROETHYLENES (Total)	0.41 U	0.42 U	0.40 U	0.46 U	0.48 U	0.35 U	0.35 U
1,2-Dichloroethane	0.41 U	0.42 U	0.40 U	0.46 U	0.48 U	0.35 U	0.35 U
1,2-Dichloropropane	0.68 U	0.69 U	0.66 U	0.76 U	0.80 U	0.58 U	0.58 U
Acetone	4.23 U	4.31 U	4.11 U	4.73 U	4.99 U	3.62 U	3.62 U
Acrylonitrile	2.56 U	2.61 U	2.49 U	2.87 U	3.03 U	2.19 U	2.20 U
Bromodichloromethane	0.26 U	0.26 U	0.25 U	0.29 U	0.30 U	0.22 U	0.22 U
Vinyl chloride	2.31 U	2.35 U	2.24 U	2.58 U	2.72 U	1.97 U	1.98 U
Chloroethane	0.82 U	0.84 U	0.80 U	0.92 U	0.97 U	0.70 U	0.70 U
Benzene	0.13 U	0.13 U	0.12 U	0.14 U	0.15 U	0.11 U	0.11 U
Trichlorofluoromethane	0.29 U	0.30 U	0.29 U	0.33 U	0.35 U	0.25 U	0.25 U
Carbon tetrachloride	0.40 U	0.41 U	0.39 U	0.44 U	0.47 U	0.34 U	0.34 U
Methylene chloride	5.64 U	5.75 U	5.48 U	6.30 U	6.66 U	4.82 U	4.83 U
Bromomethane	0.33 U	0.34 U	0.32 U	0.37 U	0.39 U	0.29 U	0.29 U
Chloromethane	1.23 U	1.25 U	1.20 U	1.38 U	1.45 U	1.05 U	1.05 U
Bromoform	0.26 U	0.26 U	0.25 U	0.29 U	0.30 U	0.22 U	0.22 U
Chloroform	0.31 U	0.31 U	0.30 U	0.34 U	0.36 U	0.26 U	0.26 U
Chlorobenzene	0.13 U	0.13 U	0.12 U	0.14 U	0.15 U	0.11 U	0.11 U
Ethylbenzene	0.24 U	0.25 U	0.24 U	0.27 U	0.29 U	0.21 U	0.21 U
Toluene	0.13 U	0.13 U	0.12 U	0.14 U	0.15 U	0.11 U	0.11 U
2-BUTANONE	5.51 U	5.62 U	5.35 U	6.16 U	6.51 U	4.71 U	4.72 U
4-METHYL-2-PENTANONE	0.81 U	0.82 U	0.78 U	0.90 U	0.95 U	0.69 U	0.69 U
1,1,2,2-Tetrachloroethane	0.26 U	0.26 U	0.25 U	0.29 U	0.30 U	0.22 U	0.22 U
Tetrachloroethylene	0.21 U	0.21 U	0.20 U	0.23 U	0.24 U	0.18 U	0.18 U
Trichloroethylene	0.29 U	0.30 U	0.29 U	0.33 U	0.35 U	0.25 U	0.25 U
*XYLENES Total	1.00 U	1.02 U	0.97 U	1.12 U	1.18 U	0.86 U	0.86 U

Field Sample Number ->	48SB4A11		48SB4B21		48SS1		48SS2		48SS3		48SS8		SCSE1	
Lab Analysis Number ->	UB06567		UB06568		UB06558		UB06559		UB06560		UB06564		UC00193	
Volatile Organics (ug/g)														
1,1,1-Trichloroethane	0.26 U		0.24 U		0.26 U		0.25 U		0.23 U		0.24 U		0.25 U	
1,1,2-Trichloroethane	0.42 U		0.40 U		0.44 U		0.40 U		0.38 U		0.40 U		0.41 U	
1,1-Dichloroethene	0.34 U		0.33 U		0.36 U		0.33 U		0.31 U		0.33 U		0.33 U	
1,1-Dichloroethane	0.63 U		0.59 U		0.65 U		0.60 U		0.57 U		0.59 U		0.60 U	
*1,2-DICHLOROETHYLENES (Total)	0.41 U		0.39 U		0.42 U		0.39 U		0.37 U		0.39 U		0.39 U	
1,2-Dichloroethane	0.41 U		0.39 U		0.42 U		0.39 U		0.37 U		0.39 U		0.39 U	
1,2-Dichloropropane	0.68 U		0.64 U		0.70 U		0.65 U		0.61 U		0.64 U		0.65 U	
Acetone	4.21 U		3.99 U		4.37 U		4.05 U		3.83 U		3.98 U		4.06 U	
Acrylonitrile	2.55 U		2.42 U		2.65 U		2.45 U		2.32 U		2.41 U		2.46 U	
Bromodichloromethane	0.26 U		0.24 U		0.26 U		0.25 U		0.23 U		0.24 U		0.25 U	
Vinyl chloride	2.30 U		2.18 U		2.38 U		2.21 U		2.09 U		2.17 U		2.21 U	
Chloroethane	0.82 U		0.77 U		0.85 U		0.79 U		0.74 U		0.77 U		0.79 U	
Benzene	0.13 U		0.12 U		0.13 U		0.12 U		0.12 U		0.12 U		0.12 U	
Trichlorofluoromethane	0.29 U		0.28 U		0.30 U		0.28 U		0.27 U		0.28 U		0.28 U	
Carbon tetrachloride	0.40 U		0.37 U		0.41 U		0.38 U		0.36 U		0.37 U		0.38 U	
Methylene chloride	5.61 U		5.32 U		5.83 U		5.40 U		5.10 U		5.30 U		5.41 U	
Bromomethane	0.33 U		0.31 U		0.34 U		0.32 U		0.30 U		0.31 U		0.32 U	
Chloromethane	1.22 U		1.16 U		1.27 U		1.18 U		1.11 U		1.16 U		1.18 U	
Bromoform	0.26 U		0.24 U		0.26 U		0.25 U		0.23 U		0.24 U		0.25 U	
Chloroform	0.31 U		0.29 U		0.32 U		0.29 U		0.28 U		0.29 U		0.30 U	
Chlorobenzene	0.13 U		0.12 U		0.13 U		0.12 U		0.12 U		0.12 U		0.12 U	
Ethylbenzene	0.24 U		0.23 U		0.25 U		0.23 U		0.22 U		0.23 U		0.23 U	
Toluene	0.13 U		0.12 U		0.13 U		0.12 U		0.12 U		0.12 U		0.12 U	
2-BUTANONE	5.48 U		5.20 U		5.70 U		5.28 U		4.99 U		5.18 U		5.29 U	
4-METHYL-2-PENTANONE	0.80 U		0.76 U		0.83 U		0.77 U		0.73 U		0.76 U		0.77 U	
1,1,2,2-Tetrachloroethane	0.26 U		0.24 U		0.26 U		0.25 U		0.23 U		0.24 U		0.25 U	
Tetrachloroethylene	0.20 U		0.19 U		0.21 U		0.20 U		0.19 U		0.19 U		0.20 U	
Trichloroethylene	0.29 U		0.28 U		0.30 U		0.28 U		0.27 U		0.28 U		0.28 U	
*XYLENES Total	0.99 U		0.94 U		1.03 U		0.96 U		0.90 U		0.94 U		0.96 U	

Field Sample Number ->	SCSE2		SCSE3	
Lab Analysis Number ->	UC00194		UC00195	
Volatile Organics (ug/g)				
1,1,1-Trichloroethane	0.29 U		0.28 U	
1,1,2-Trichloroethane	0.49 U		0.47 U	
1,1-Dichloroethene	0.40 U		0.38 U	
1,1-Dichloroethane	0.72 U		0.70 U	
*1,2-DICHLOROETHYLENES (Total)	0.47 U		0.45 U	
1,2-Dichloroethane	0.47 U		0.45 U	
1,2-Dichloropropane	0.78 U		0.75 U	
Acetone	4.87 U		4.68 U	
Acrylonitrile	2.95 U		2.84 U	
Bromodichloromethane	0.29 U		0.28 U	
Vinyl chloride	2.65 U		2.55 U	
Chloroethane	0.94 U		0.91 U	
Benzene	0.15 U		0.14 U	
Trichlorofluoromethane	0.34 U		0.33 U	
Carbon tetrachloride	0.46 U		0.44 U	
Methylene chloride	6.49 U		6.24 U	
Bromomethane	0.38 U		0.37 U	
Chloromethane	1.42 U		1.36 U	
Bromoform	0.29 U		0.28 U	
Chloroform	0.35 U		0.34 U	
Chlorobenzene	0.15 U		0.14 U	
Ethylbenzene	0.28 U		0.27 U	
Toluene	0.15 U		0.14 U	
2-BUTANONE	6.34 U		6.10 U	
4-METHYL-2-PENTANONE	0.93 U		0.89 U	
1,1,2,2-Tetrachloroethane	0.29 U		0.28 U	
Tetrachloroethylene	0.24 U		0.23 U	
Trichloroethylene	0.34 U		0.33 U	
*XYLENES Total	1.15 U		1.11 U	

Field Sample Number ->	17ASB105	17ASB122	17ASB205	17ASB225	17ASB305	17ASB325	17ASB340	48SB4A11
Lab Analysis Number ->	UB06429	UB06433	UB06435	UB06439	UB06442	UB06446	UB06447	UB06567
Semivolatile Organics (ug/g)								
1,2,4-Trichlorobenzene	0.28 U	0.29 U	0.27 U	0.32 U	0.33 U	0.24 U	0.24 U	0.28 U
1,2-Dichlorobenzene	0.05 U	0.05 U	0.05 U	0.06 U	0.06 U	0.05 U	0.05 U	0.05 U
1,3-Dichlorobenzene	0.05 U	0.05 U	0.05 U	0.06 U	0.06 U	0.05 U	0.05 U	0.05 U
1,4-Dichlorobenzene	0.04 U	0.04 U	0.04 U	0.05 U	0.05 U	0.04 U	0.04 U	0.04 U
2,4,5-Trichlorophenol	0.63 U	0.64 U	0.61 U	0.70 U	0.74 U	0.54 U	0.54 U	0.63 U
2,4,6-Trichlorophenol	0.08 U	0.08 U	0.08 U	0.09 U	0.09 U	0.07 U	0.07 U	0.08 U
2,4-Dichlorophenol	0.08 U	0.08 U	0.08 U	0.09 U	0.10 U	0.07 U	0.07 U	0.08 U
2,4-Dimethylphenol	3.85 U	3.92 U	3.74 U	4.30 U	4.54 U	3.29 U	3.29 U	3.83 U
2,4-Dinitrophenol	6.03 U	6.14 U	5.85 U	6.73 U	7.11 U	5.15 U	5.16 U	5.99 U
2,4-Dinitrotoluene	1.79 U	1.83 U	1.74 U	2.01 U	2.12 U	1.54 U	1.54 U	1.79 U
2,6-Dinitrotoluene	0.41 U	0.42 U	0.40 U	0.46 U	0.48 U	0.35 U	0.35 U	0.41 U
2-Chlorophenol	0.07 U	0.07 U	0.07 U	0.08 U	0.08 U	0.06 U	0.06 U	0.07 U
2-Chloronaphthalene	0.31 U	0.31 U	0.30 U	0.34 U	0.36 U	0.26 U	0.26 U	0.31 U
2-Methylphenol	0.13 U	0.13 U	0.12 U	0.14 U	0.15 U	0.11 U	0.11 U	0.13 U
3,3'-Dichlorobenzidine	2.05 U	2.09 U	1.99 U	2.29 U	2.42 U	1.75 U	1.76 U	2.04 U
4,6-Dinitro-2-cresol	1.03 U	1.05 U	1.00 U	1.15 U	1.21 U	0.88 U	0.88 U	1.02 U
4-BROMOPHENYLPHENYL ETHER	0.05 U	0.05 U	0.05 U	0.06 U	0.06 U	0.04 U	0.05 U	0.05 U
3-METHYL-4-CHLOROPHENOL	1.19 U	1.22 U	1.16 U	1.33 U	1.41 U	1.02 U	1.02 U	1.19 U
4-Methylphenol	0.31 U	0.31 U	0.30 U	0.34 U	0.36 U	0.26 U	0.26 U	0.31 U
4-Nitrophenol	4.23 U	4.31 U	4.11 U	4.73 U	4.99 U	3.62 U	3.62 U	4.21 U
Anthracene	0.91 U	0.93 U	0.88 U	1.02 U	1.07 U	0.78 U	0.78 U	0.91 U
Bis(2-chloroethoxy) methane	0.24 U	0.25 U	0.24 U	0.27 U	0.29 U	0.21 U	0.21 U	0.24 U
Bis(2-chloroisopropyl) ether	0.56 U	0.58 U	0.55 U	0.63 U	0.67 U	0.48 U	0.48 U	0.56 U
Bis(2-chloroethyl) ether	0.46 U	0.47 U	0.45 U	0.52 U	0.54 U	0.39 U	0.40 U	0.46 U
Bis(2-ethylhexyl) phthalate	10.13	2.48	5.85	0.69 U	3.48	2.30	0.53 U	3.57
Benzo[a]anthracene	0.99	0.05 U	0.05 U	0.06 U	0.06 U	0.29	0.05 U	0.05 U
Benzo[a]pyrene	1.54 U	1.57 U	1.49 U	1.72 U	1.82 U	1.32 U	1.32 U	1.53 U
Benzo[b]fluoranthene	1.92	0.41 U	0.39 U	0.44 U	0.47 U	0.34 U	0.34 U	0.40 U
Butylbenzyl phthalate	2.31 U	2.35 U	2.24 U	2.58 U	2.72 U	1.97 U	1.98 U	2.30 U
Benzo[k]fluoranthene	0.56	0.17 U	0.16 U	0.19 U	0.20 U	0.14 U	0.14 U	0.17 U
Chrysene	1.04	0.04 U	0.04 U	0.05 U	0.05 U	0.25	0.04 U	0.04 U
Hexachlorobenzene	0.10 U	0.10 U	0.10 U	0.11 U	0.12 U	0.09 U	0.09 U	0.10 U
Hexachlorocyclopentadiene	0.67 U	0.68 U	0.65 U	0.74 U	0.79 U	0.57 U	0.57 U	0.66 U
Hexachloroethane	2.31 U	2.35 U	2.24 U	2.58 U	2.72 U	1.97 U	1.98 U	2.30 U
Dibenz[ah]anthracene	0.40 U	0.41 U	0.39 U	0.44 U	0.47 U	0.34 U	0.34 U	0.40 U
Diethyl phthalate	0.31 U	0.31 U	0.30 U	0.34 U	0.36 U	9.87	0.26 U	0.31 U
Dimethyl phthalate	0.08 U	0.08 U	0.08 U	0.09 U	0.10 U	0.07 U	0.07 U	0.08 U
Di-n-butyl phthalate	1.67 U	1.70 U	1.62 U	1.86 U	1.97 U	1.43 U	1.43 U	1.66 U
Di-n-octyl phthalate	0.29 U	0.30 U	0.29 U	0.33 U	0.35 U	0.25 U	0.25 U	0.29 U
Fluoranthene	0.81	0.04 U	0.04 U	0.05 U	0.05 U	0.38	0.04 U	0.04 U
Hexachlorobutadiene	1.24 U	1.27 U	1.21 U	1.39 U	1.47 U	1.06 U	1.06 U	1.24 U
Indeno[1,2,3-C,D]pyrene	3.08 U	3.14 U	2.99 U	3.44 U	3.63 U	2.63 U	2.63 U	3.06 U

Field Sample Number ->	17ASB105		17ASB122		17ASB205		17ASB225		17ASB305		17ASB325		17ASB340		48SB4A11	
Lab Analysis Number ->	UB06429		UB06433		UB06435		UB06439		UB06442		UB06446		UB06447		UB06567	
Semivolatile Organics (ug/g)																
Naphthalene	0.95 U		0.97 U		0.92 U		1.06 U		1.12 U		0.81 U		0.81 U		0.94 U	
Nitrobenzene	2.31 U		2.35 U		2.24 U		2.58 U		2.72 U		1.97 U		1.98 U		2.30 U	
N-Nitrosodi-n-propylamine	1.41 U		1.44 U		1.37 U		1.58 U		1.66 U		1.21 U		1.21 U		1.40 U	
N-Nitrosodiphenylamine	0.37 U		0.38 U		0.36 U		0.42 U		0.44 U		0.32 U		0.32 U		1.79	
Pentachlorophenol	0.97 U		0.99 U		0.95 U		1.09 U		1.15 U		0.83 U		0.83 U		0.97 U	
Phenanthrene	1.67		0.04 U		0.04 U		0.05 U		0.05 U		0.65		0.04 U		0.04 U	
Phenol	0.07 U		0.07 U		0.06 U		0.07 U		0.08 U		0.06 U		0.06 U		0.07 U	
Pyrene	1.54		0.11 U		0.10 U		0.12 U		0.13 U		0.50		0.09 U		0.11 U	

Field Sample Number ->	48SB4B21	48SB5A19	48SB5B37	48SS1	48SS2	48SS3	48SS4	48SS5
Lab Analysis Number ->	UB06568	UB06572	UB06573	UB06558	UB06559	UB06560	UB06561	UB06562
Semivolatile Organics (ug/g)								
1,2,4-Trichlorobenzene	0.27 U	1.22 U	0.27 U	0.29 U	0.27 U	0.26 U	0.26 U	0.27 U
1,2-Dichlorobenzene	0.05 U	0.24 U	0.05 U	0.06 U	0.05 U	0.05 U	0.05 U	0.05 U
1,3-Dichlorobenzene	0.05 U	0.24 U	0.05 U	0.06 U	0.05 U	0.05 U	0.05 U	0.05 U
1,4-Dichlorobenzene	0.04 U	0.24 U	0.04 U	0.05 U	0.04 U	0.04 U	0.04 U	0.04 U
2,4,5-Trichlorophenol	0.59 U	2.43 U	0.60 U	0.65 U	0.60 U	0.57 U	0.58 U	0.61 U
2,4,6-Trichlorophenol	0.07 U	0.36 U	0.08 U	0.08 U	0.07 U	0.07 U	0.07 U	0.08 U
2,4-Dichlorophenol	0.08 U	0.36 U	0.08 U	0.09 U	0.08 U	0.08 U	0.08 U	0.08 U
2,4-Dimethylphenol	3.63 U	24.30 U	3.70 U	3.97 U	3.68 U	3.48 U	3.56 U	3.71 U
2,4-Dinitrophenol	5.68 U	24.30 U	5.80 U	6.23 U	5.77 U	5.45 U	5.58 U	5.81 U
2,4-Dinitrotoluene	1.69 U	8.51 U	1.73 U	1.85 U	1.72 U	1.62 U	1.66 U	1.73 U
2,6-Dinitrotoluene	0.39 U	2.43 U	0.39 U	0.42 U	0.39 U	0.37 U	0.38 U	0.40 U
2-Chlorophenol	0.07 U	0.36 U	0.07 U	0.07 U	0.07 U	0.06 U	0.07 U	0.07 U
2-Chloronaphthalene	0.29 U	1.22 U	0.30 U	0.32 U	0.29 U	0.28 U	0.29 U	0.30 U
2-Methylphenol	0.12 U	0.61 U	0.12 U	0.13 U	0.12 U	0.11 U	0.12 U	0.12 U
3,3'-Dichlorobenzidine	1.93 U	9.72 U	1.97 U	2.12 U	1.96 U	1.86 U	1.90 U	1.98 U
4,6-Dinitro-2-cresol	0.97 U	4.86 U	0.99 U	1.06 U	0.98 U	0.93 U	0.95 U	0.99 U
4-BROMOPHENYLPHENYL ETHER	0.05 U	0.24 U	0.05 U	0.05 U	0.05 U	0.05 U	0.05 U	0.05 U
3-METHYL-4-CHLOROPHENOL	1.12 U	6.08 U	1.15 U	1.23 U	1.14 U	1.08 U	1.10 U	1.15 U
4-Methylphenol	0.29 U	1.22 U	0.30 U	0.32 U	0.29 U	0.28 U	0.29 U	0.30 U
4-Nitrophenol	3.99 U	24.30 U	4.07 U	4.37 U	4.05 U	3.83 U	3.92 U	4.08 U
Anthracene	0.86 U	4.86 U	0.88 U	0.94 U	0.87 U	0.82 U	0.84 U	0.88 U
Bis(2-chloroethoxy) methane	0.23 U	1.22 U	0.23 U	0.25 U	0.23 U	0.22 U	0.23 U	0.23 U
Bis(2-chloroisopropyl) ether	0.53 U	2.43 U	0.54 U	0.58 U	0.54 U	0.51 U	0.52 U	0.54 U
Bis(2-chloroethyl) ether	0.44 U	2.43 U	0.44 U	0.48 U	0.44 U	0.42 U	0.43 U	0.44 U
Bis(2-ethylhexyl) phthalate	4.35	48.60	12.33	1.99	1.60	0.56 U	0.57 U	0.59 U
Benzo[a]anthracene	0.05 U	0.24 U	0.05 U	0.05 U	0.05 U	0.05 U	0.05 U	0.05 U
Benzo[a]pyrene	1.45 U	7.29 U	1.48 U	1.59 U	1.47 U	1.39 U	1.43 U	1.48 U
Benzo[b]fluoranthene	0.37 U	2.43 U	0.38 U	0.41 U	0.38 U	0.36 U	0.37 U	0.38 U
Butylbenzyl phthalate	2.18 U	10.94 U	2.22 U	2.38 U	2.21 U	2.09 U	2.14 U	2.22 U
Benzo[k]fluoranthene	0.16 U	0.73 U	0.16 U	0.17 U	0.16 U	0.15 U	0.15 U	0.16 U
Chrysene	0.04 U	0.24 U	0.04 U	0.11	0.04 U	0.04 U	0.09	0.04 U
Hexachlorobenzene	0.10 U	0.49 U	0.10 U	0.11 U	0.10 U	0.09 U	0.10 U	0.10 U
Hexachlorocyclopentadiene	0.63 U	3.65 U	0.64 U	0.69 U	0.64 U	0.60 U	0.62 U	0.64 U
Hexachloroethane	2.18 U	10.94 U	2.22 U	2.38 U	2.21 U	2.09 U	2.14 U	2.22 U
Dibenz[ah]anthracene	0.37 U	2.43 U	0.38 U	0.41 U	0.38 U	0.36 U	0.37 U	0.38 U
Diethyl phthalate	0.29 U	1.22 U	0.30 U	0.32 U	0.29 U	0.28 U	0.29 U	0.30 U
Dimethyl phthalate	0.08 U	0.36 U	0.08 U	0.08 U	0.08 U	0.07 U	0.07 U	0.08 U
Di-n-butyl phthalate	7.26	7.29 U	1.60 U	1.72 U	12.27	1.51 U	1.54 U	1.61 U
Di-n-octyl phthalate	0.28 U	1.22 U	0.28 U	0.30 U	0.28 U	0.27 U	0.27 U	0.28 U
Fluoranthene	0.04 U	0.24 U	0.04 U	0.04 U	0.04 U	0.04 U	0.04 U	0.04 U
Hexachlorobutadiene	1.17 U	6.08 U	1.20 U	1.28 U	1.19 U	1.13 U	1.15 U	1.20 U
Indeno[1,2,3-G,D]pyrene	2.90 U	12.15 U	2.96 U	3.18 U	2.94 U	2.78 U	2.85 U	2.97 U

Field Sample Number ->	48SB4B21	48SB5A19	48SB5B37	48SS1	48SS2	48SS3	48SS4	48SS5
Lab Analysis Number ->	UB06568	UB06572	UB06573	UB06558	UB06559	UB06560	UB06561	UB06562
Semivolatile Organics (ug/g)								
Naphthalene	0.89 U	24.30	0.91 U	0.96 U	0.91 U	0.86 U	0.88 U	0.91 U
Nitrobenzene	2.18 U	10.94 U	2.22 U	2.36 U	2.21 U	2.09 U	2.14 U	2.22 U
N-Nitrosodi-n-propylamine	1.33 U	7.29 U	1.36 U	1.46 U	1.35 U	1.28 U	1.31 U	1.36 U
N-Nitrosodiphenylamine	2.06	1.22 U	0.36 U	0.36 U	0.36 U	0.34 U	0.34 U	0.36 U
Pentachlorophenol	0.92 U	4.86 U	0.94 U	1.01 U	0.93 U	0.88 U	0.90 U	0.94 U
Phenanthrene	0.04 U	12.15	0.04 U	0.36	0.04 U	0.04 U	0.37	0.04 U
Phenol	0.06 U	0.36 U	0.06 U	0.07 U	0.06 U	0.06 U	0.06 U	0.06 U
Pyrene	0.10 U	0.97	0.10 U	0.11 U	0.10 U	0.10 U	0.10 U	0.10 U

Field Sample Number ->	48SS6	48SS8	48MW1A22	48MW1B54	48MW2A42	48MW2B46	48MW3A22	48MW3B32
Lab Analysis Number ->	UB06563	UB06564	UB06575	UB06576	UB06585	UB06586	UC00028	UC00029
Semivolatile Organics (ug/g)								
1,2,4-Trichlorobenzene	0.26 U	0.27 U	0.28 U	0.30 U	0.25 U	0.24 U	0.27 U	0.27 U
1,2-Dichlorobenzene	0.05 U	0.05 U	0.05 U	0.06 U	0.05 U	0.05 U	0.05 U	0.05 U
1,3-Dichlorobenzene	0.05 U	0.05 U	0.05 U	0.06 U	0.05 U	0.05 U	0.05 U	0.05 U
1,4-Dichlorobenzene	0.04 U	0.04 U	0.04 U	0.05 U	0.04 U	0.04 U	0.04 U	0.04 U
2,4,5-Trichlorophenol	0.57 U	0.59 U	0.62 U	0.66 U	0.57 U	0.53 U	0.60 U	0.61 U
2,4,6-Trichlorophenol	0.07 U	0.07 U	0.08 U	0.08 U	0.07 U	0.07 U	0.07 U	0.08 U
2,4-Dichlorophenol	0.08 U	0.08 U	0.08 U	0.09 U	0.08 U	0.07 U	0.08 U	0.08 U
2,4-Dimethylphenol	3.51 U	3.61 U	3.82 U	4.06 U	3.46 U	3.26 U	3.65 U	3.73 U
2,4-Dinitrophenol	5.50 U	5.66 U	5.98 U	6.36 U	5.43 U	5.11 U	5.71 U	5.85 U
2,4-Dinitrotoluene	1.64 U	1.69 U	1.78 U	1.89 U	1.62 U	1.52 U	1.70 U	1.74 U
2,6-Dinitrotoluene	0.37 U	0.39 U	0.41 U	0.43 U	0.37 U	0.35 U	0.39 U	0.40 U
2-Chlorophenol	0.06 U	0.07 U	0.07 U	0.07 U	0.06 U	0.06 U	0.07 U	0.07 U
2-Chloronaphthalene	0.28 U	0.29 U	0.31 U	0.32 U	0.28 U	0.26 U	0.29 U	0.30 U
2-Methylphenol	0.11 U	0.12 U	0.12 U	0.13 U	0.11 U	0.11 U	0.12 U	0.12 U
3,3'-Dichlorobenzidine	1.87 U	1.93 U	2.04 U	2.17 U	1.85 U	1.74 U	1.94 U	1.99 U
4,6-Dinitro-2-cresol	0.94 U	0.96 U	1.02 U	1.08 U	0.92 U	0.87 U	0.97 U	1.00 U
4-BROMOPHENYLPHENYL ETHER	0.05 U	0.05 U	0.05 U	0.06 U	0.05 U	0.04 U	0.05 U	0.05 U
3-METHYL-4-CHLOROPHENOL	1.09 U	1.12 U	1.18 U	1.26 U	1.07 U	1.01 U	1.13 U	1.16 U
4-Methylphenol	0.28 U	0.29 U	0.31 U	0.32 U	0.28 U	0.26 U	0.29 U	0.30 U
4-Nitrophenol	3.86 U	3.98 U	4.20 U	4.47 U	3.81 U	3.59 U	4.01 U	4.10 U
Anthracene	0.83 U	0.86 U	0.90 U	0.96 U	0.82 U	0.77 U	0.86 U	0.88 U
Bis(2-chloroethoxy) methane	0.22 U	0.23 U	0.24 U	0.26 U	0.22 U	0.21 U	0.23 U	0.24 U
Bis(2-chloroisopropyl) ether	0.51 U	0.53 U	0.56 U	0.60 U	0.51 U	0.48 U	0.53 U	0.55 U
Bis(2-chloroethyl) ether	0.42 U	0.43 U	0.46 U	0.49 U	0.42 U	0.39 U	0.44 U	0.45 U
Bis(2-ethylhexyl) phthalate	1.40 U	1.57 U	1.14 U	1.17 U	1.96 U	0.52 U	3.77 U	2.49 U
Benzo[a]anthracene	0.05 U	0.05 U	0.05 U	0.06 U	0.05 U	0.04 U	0.05 U	0.05 U
Benzo[a]pyrene	1.40 U	1.45 U	1.53 U	1.62 U	1.39 U	1.31 U	1.46 U	1.49 U
Benzo[b]fluoranthene	0.36 U	0.37 U	0.39 U	0.42 U	0.36 U	0.34 U	0.38 U	0.39 U
Butylbenzyl phthalate	2.11 U	2.17 U	2.29 U	2.44 U	2.08 U	1.96 U	2.19 U	2.24 U
Benzo[k]fluoranthene	0.15 U	0.16 U	0.17 U	0.18 U	0.15 U	0.14 U	0.16 U	0.16 U
Chrysene	0.08 U	0.09 U	0.04 U	0.04 U	0.04 U	0.03 U	0.04 U	0.04 U
Hexachlorobenzene	0.09 U	0.10 U	0.10 U	0.11 U	0.09 U	0.09 U	0.10 U	0.10 U
Hexachlorocyclopentadiene	0.61 U	0.63 U	0.66 U	0.70 U	0.60 U	0.57 U	0.63 U	0.65 U
Hexachloroethane	2.11 U	2.17 U	2.29 U	2.44 U	2.08 U	1.96 U	2.19 U	2.24 U
Dibenz[ah]anthracene	0.36 U	0.37 U	0.39 U	0.42 U	0.36 U	0.34 U	0.38 U	0.39 U
Diethyl phthalate	0.28 U	0.29 U	0.31 U	0.32 U	0.28 U	0.26 U	0.29 U	0.30 U
Dimethyl phthalate	0.07 U	0.08 U	0.08 U	0.09 U	0.07 U	0.07 U	0.08 U	0.08 U
Di-n-butyl phthalate	1.52 U	1.55 U	1.65 U	1.76 U	1.50 U	1.41 U	1.62 U	1.62 U
Di-n-octyl phthalate	0.27 U	0.28 U	0.29 U	0.31 U	0.27 U	0.25 U	0.28 U	0.29 U
Fluoranthene	0.04 U	0.04 U	0.04 U	0.04 U	0.04 U	0.03 U	0.04 U	0.04 U
Hexachlorobutadiene	1.13 U	1.17 U	1.23 U	1.31 U	1.12 U	1.06 U	1.18 U	1.21 U
Indeno[1,2,3-c,d]pyrene	2.81 U	2.89 U	3.05 U	3.25 U	2.77 U	2.61 U	2.92 U	2.99 U

Field Sample Number ->	48SS6	48SS8	48MW1A22	48MW1B54	48MW2A42	48MW2B46	48MW3A22	48MW3B32
Lab Analysis Number ->	UB06563	UB06564	UB06575	UB06576	UB06585	UB06586	UC00028	UC00029
Semivolatile Organics (ug/g)								
Naphthalene	0.87 U	0.89 U	0.94 U	1.00 U	0.85 U	0.81 U	0.90 U	0.92 U
Nitrobenzene	2.11 U	2.17 U	2.29 U	2.44 U	2.08 U	1.96 U	2.19 U	2.24 U
N-Nitrosodi-n-propylamine	1.29 U	1.33 U	1.40 U	1.49 U	1.27 U	1.20 U	1.34 U	1.37 U
N-Nitrosodiphenylamine	0.34 U	0.35 U	0.37 U	0.39 U	0.33 U	0.32 U	0.35 U	0.36 U
Pentachlorophenol	0.86 U	0.92 U	0.97 U	1.03 U	0.88 U	0.83 U	0.92 U	0.95 U
Phenanthrene	0.33 U	0.04 U	0.04 U	0.04 U	0.04 U	0.03 U	0.04 U	0.04 U
Phenol	0.06 U	0.06 U	0.07 U	0.07 U	0.14 U	0.06 U	0.06 U	0.06 U
Pyrene	0.10 U	0.10 U	0.11 U	0.11 U	0.10 U	0.09 U	0.10 U	0.10 U

Field Sample Number ->	SCSE1		SCSE2		SCSE3	
Lab Analysis Number ->	UC00193		UC00194		UC00195	
Semivolatile Organics (ug/g)						
1,2,4-Trichlorobenzene	0.27 U		0.32 U		0.31 U	
1,2-Dichlorobenzene	0.05 U		0.06 U		0.06 U	
1,3-Dichlorobenzene	0.05 U		0.06 U		0.06 U	
1,4-Dichlorobenzene	0.04 U		0.05 U		0.05 U	
2,4,5-Trichlorophenol	0.60 U		0.72 U		0.70 U	
2,4,6-Trichlorophenol	0.08 U		0.09 U		0.09 U	
2,4-Dichlorophenol	0.08 U		0.10 U		0.09 U	
2,4-Dimethylphenol	3.69 U		4.42 U		4.26 U	
2,4-Dinitrophenol	5.78 U		6.93 U		6.67 U	
2,4-Dinitrotoluene	1.72 U		2.06 U		1.99 U	
2,6-Dinitrotoluene	0.39 U		0.47 U		0.45 U	
2-Chlorophenol	0.07 U		0.08 U		0.08 U	
2-Chloronaphthalene	0.30 U		0.35 U		0.34 U	
2-Methylphenol	0.12 U		0.14 U		0.14 U	
3,3'-Dichlorobenzidine	1.97 U		2.36 U		2.27 U	
4,6-Dinitro-2-cresol	0.98 U		1.18 U		1.13 U	
4-BROMOPHENYLPHENYL ETHER	0.05 U		0.06 U		0.06 U	
3-METHYL-4-CHLOROPHENOL	1.14 U		1.37 U		1.32 U	
4-Methylphenol	0.30 U		0.35 U		0.34 U	
4-Nitrophenol	4.06 U		4.87 U		4.68 U	
Anthracene	0.87 U		1.05 U		1.01 U	
Bis(2-chloroethoxy) methane	0.23 U		0.28 U		0.27 U	
Bis(2-chloroisopropyl) ether	0.54 U		0.65 U		0.62 U	
Bis(2-chloroethyl) ether	0.44 U		0.53 U		0.51 U	
Bis(2-ethylhexyl) phthalate	0.59 U		0.71 U		0.68 U	
Benzo[a]anthracene	0.05 U		0.06 U		0.06 U	
Benzo[a]pyrene	1.46 U		1.77 U		1.70 U	
Benzo[k]fluoranthene	0.38 U		0.46 U		0.44 U	
Butylbenzyl phthalate	2.21 U		2.65 U		2.55 U	
Benzo[k]fluoranthene	0.16 U		0.19 U		0.18 U	
Chrysene	0.04 U		0.22		0.05 U	
Hexachlorobenzene	0.10 U		0.12 U		0.11 U	
Hexachlorocyclopentadiene	0.64 U		0.77 U		0.74 U	
Hexachloroethane	2.21 U		2.65 U		2.55 U	
Dibenz[ah]anthracene	0.38 U		0.46 U		0.44 U	
Diethyl phthalate	0.30 U		0.35 U		0.34 U	
Dimethyl phthalate	0.08 U		0.09 U		0.09 U	
Di-n-butyl phthalate	1.65 U		7.82 J1		5.53 J1	
Di-n-octyl phthalate	0.28 U		0.34 U		0.33 U	
Fluoranthene	0.04 U		0.27		0.16	
Hexachlorobutadiene	1.19 U		1.43 U		1.38 U	
Indeno[1,2,3-C,D]pyrene	2.95 U		3.54 U		3.40 U	

Field Sample Number ->	SCSE1		SCSE2		SCSE3	
Lab Analysis Number ->	UC00193		UC00194		UC00195	
Semivolatile Organics (ug/g)						
Naphthalene	0.91 U		1.09 U		1.05 U	
Nitrobenzene	2.21 U		2.65 U		2.55 U	
N-Nitrosodi-n-propylamine	1.35 U		1.62 U		1.56 U	
N-Nitrosodiphenylamine	0.36 U		0.43 U		0.41 U	
Pentachlorophenol	0.93 U		1.12 U		1.08 U	
Phenanthrene	0.04 U		0.29 U		0.13 U	
Phenol	0.06 U		0.08 U		0.07 U	
Pyrene	0.10 U		0.12 U		0.12 U	

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Field Sample Number ->	17ASB105		17ASB110		17ASB115		17ASB120		17ASB122		17ASB205		17ASB210		17ASB215		17ASB220	
Lab Analysis Number ->	UB06429		UB06430		UB06431		UB06432		UB06433		UB06435		UB06436		UB06437		UB06438	
Explosives (ug/g)																		
2,4,6-Trinitrotoluene	2.04 UJ4		2.02 UJ4		2.19 UJ4		2.21 UJ4		2.14 UJ4		2.88 UJ4		2.10 UJ4		2.00 UJ4		2.15 UJ4	
2,4-Dinitrotoluene	2.55 UJ4		2.53 UJ4		2.73 UJ4		2.77 UJ4		2.67 UJ4		3.60 UJ4		2.63 UJ4		2.51 UJ4		2.69 UJ4	
2,6-Dinitrotoluene	2.04 U		2.02 U		2.19 U		2.21 U		2.14 U		2.88 U		2.10 U		2.00 U		2.15 U	
Cyclotetramethylenetetranitramine	2.04 U		2.02 U		2.19 U		2.21 U		2.14 U		2.88 U		2.10 U		2.00 U		2.15 U	
Cyclonite (RDX)	1.31 UJ4		1.29 UJ4		1.40 UJ4		1.42 UJ4		1.37 UJ4		1.84 UJ4		1.35 UJ4		1.28 UJ4		1.38 UJ4	
TETRYL	2.15 U		2.13 U		2.31 U		2.34 U		2.26 U		3.04 U		2.22 U		2.11 U		2.27 U	

Field Sample Number ->	17ASB225		17ASS3		17ASB305		17ASB310		17ASB315		17ASB320		17ASB325		17ASB340		17BSS1	
Lab Analysis Number ->	UB06439		UB06441		UB06442		UB06443		UB06444		UB06445		UB06446		UB06447		UB06463	
Explosives (ug/g)																		
2,4,6-Trinitrotoluene	2.16	UJ4	2.08	UJ4	2.04	UJ4	2.14	UJ4	2.20	UJ4	2.19	UJ4	2.20	UJ4	2.01	UJ4	2.90	UJ4
2,4-Dinitrotoluene	2.70	UJ4	2.60	UJ4	2.55	UJ4	2.68	UJ4	2.75	UJ4	2.74	UJ4	2.74	UJ4	2.51	UJ4	3.63	UJ4
2,6-Dinitrotoluene	2.16	U	2.08	U	2.04	U	2.14	U	2.20	U	2.19	U	2.20	U	2.01	U	2.90	U
Cyclotetramethylenetetranitramine	2.16	U	2.08	U	2.04	U	2.14	U	2.20	U	2.19	U	2.20	U	2.01	U	2.90	U
Cyclonite (RDX)	1.38	UJ4	1.33	UJ4	1.30	UJ4	1.37	UJ4	1.41	UJ4	1.40	UJ4	1.41	UJ4	1.28	UJ4	1.86	UJ4
TETRYL	2.28	U	2.20	U	2.15	U	2.26	U	2.32	U	2.31	U	2.32	U	2.12	U	3.06	U

Field Sample Number ->	17B552		17CSB105		17CSB110		17CSB114		17CSB205		17CSB210		17CSB215		17CSB240		17DSB105	
Lab Analysis Number ->	UB06464		UB06465		UB06466		UB06467		UB06469		UB06470		UB06471		UB06473		UB06476	
Explosives (ug/g)																		
2,4,6-Trinitrotoluene	2.89	UJ4	2.46	UJ4	2.73	UJ4	2.66	UJ4	2.49	UJ4	2.96	UJ4	2.54	UJ4	3.11	UJ4	2.56	UJ4
2,4-Dinitrotoluene	3.61	UJ4	3.08	UJ4	3.42	UJ4	3.32	UJ4	3.11	UJ4	3.70	UJ4	3.18	UJ4	3.88	UJ4	3.20	UJ4
2,6-Dinitrotoluene	2.89	U	2.46	U	2.73	U	2.66	U	2.49	U	2.96	U	2.54	U	3.11	U	2.56	U
Cyclotetramethylenetetranitramine	2.89	U	2.46	U	2.73	U	2.66	U	2.49	U	2.96	U	2.54	U	3.11	U	2.56	U
Cyclonite (RDX)	1.85	UJ4	1.57	UJ4	1.75	UJ4	1.70	UJ4	1.59	UJ4	1.89	UJ4	1.63	UJ4	1.99	UJ4	1.64	UJ4
TETRYL	3.04	U	2.60	U	2.88	U	2.60	U	2.63	U	3.12	U	2.68	U	3.28	U	2.70	U

Field Sample Number ->	17DSB110		17DSB115		17DSB120		17DSB125		17DSB205		17DSB210		17DSB127		17DSB215		17DSB220	
Lab Analysis Number ->	UB06477		UB06478		UB06479		UB06480		UB06483		UB06484		UB06481		UB06485		UB06486	
Explosives (ug/g)																		
2,4,6-Trinitrotoluene	2.48	UJ4	2.56	UJ4	2.67	UJ4	3.19	UJ4	2.46	UJ4	2.57	UJ4	3.33	UJ4	3.23	UJ4	3.26	UJ4
2,4-Dinitrotoluene	3.09	UJ4	3.21	UJ4	3.34	UJ4	3.99	UJ4	3.08	UJ4	3.21	UJ4	4.16	UJ4	4.04	UJ4	4.08	UJ4
2,6-Dinitrotoluene	2.48	U	2.56	U	2.67	U	3.19	U	2.46	U	2.57	U	3.33	U	3.23	U	3.26	U
Cyclotetramethylenetetranitramine	2.48	U	2.56	U	2.67	U	3.19	U	2.46	U	2.57	U	3.33	U	3.23	U	3.26	U
Cyclonite (RDX)	1.58	UJ4	1.64	UJ4	1.71	UJ4	2.04	UJ4	1.58	UJ4	1.65	UJ4	2.13	UJ4	2.07	UJ4	2.09	UJ4
TETRYL	2.61	U	2.71	U	2.82	U	3.37	U	2.60	U	2.71	U	3.51	U	3.41	U	3.44	U

Field Sample Number ->	17DSB225		17DSB240		SPG3SE1		48SB4A11		48SB4B21		48SS1		48SS2		48SS3		48SS8	
Lab Analysis Number ->	UB06487		UB06488		UC00174		UB06567		UB06568		UB06558		UB06559		UB06560		UB06564	
Explosives (ug/g)																		
2,4,6-Trinitrotoluene	2.83	UJ4	2.52	UJ4	3.13	UJ4	2.55	UJ4	2.42	UJ4	2.65	UJ4	2.45	UJ4	2.32	UJ4	2.41	UJ4
2,4-Dinitrotoluene	3.54	UJ4	3.15	UJ4	3.92	UJ4	3.19	UJ4	3.02	UJ4	3.31	UJ4	3.07	UJ4	2.90	UJ4	3.01	UJ4
2,6-Dinitrotoluene	2.83	U	2.52	U	3.13	U	2.55	U	2.42	U	2.65	U	2.45	U	2.32	U	2.41	U
Cyclotetramethylenetetranitramine	2.83	U	2.52	U	3.13	U	2.55	U	2.42	U	2.65	U	2.45	U	2.32	U	2.41	U
Cyclonite (RDX)	1.81	UJ4	1.61	UJ4	2.01	UJ4	1.63	UJ4	1.55	UJ4	1.70	UJ4	1.57	UJ4	1.48	UJ4	1.54	UJ4
TETRYL	2.99	U	2.66	U	3.31	U	2.69	U	2.55	U	2.79	U	2.59	U	2.45	U	2.54	U

Field Sample Number ->	54SB1A		54SB1B		54SB2A		54SB2B		54SB3A		54SB3B		54SB4A		54SB4B		54SB5A	
Lab Analysis Number ->	UB06593		UB06594		UB06595		UB06596		UB06597		UB06598		UB06599		UB06600		UB06601	
Explosives (ug/g)																		
2,4,6-Trinitrotoluene	2.35 UJ4		2.19 UJ4		4.41 J4		2.45 UJ4		2,988.51 J4		48.42 J4		2.48 UJ4		2.41 UJ4		2.49 UJ4	
2,4-Dinitrotoluene	2.94 UJ4		2.74 UJ4		2.80 UJ4		3.07 UJ4		12.76 J4		3.29 UJ4		3.10 UJ4		3.01 UJ4		3.12 UJ4	
2,6-Dinitrotoluene	2.35 U		2.19 U		2.24 U		2.45 U		2.30 U		2.63 U		2.48 U		2.41 U		2.49 U	
Cyclotetramethylenetetranitramine	2.35 U		2.19 U		2.24 U		2.45 U		4.68		2.63 U		2.48 U		2.41 U		2.49 U	
Cyclonite (RDX)	1.50 UJ4		1.40 UJ4		1.43 UJ4		1.57 UJ4		1.98 J4		1.68 UJ4		1.59 UJ4		1.54 UJ4		1.60 UJ4	
TETRYL	2.48 U		2.31 U		2.37 U		2.59 U		2.43 U		2.78 U		2.61 U		2.54 U		2.63 U	

Field Sample Number ->	54SB5B		54SB6A		54SB6B		54SB7A		54SB7B		54SB8A		54SB8B		54SB9A		54SB9B	
Lab Analysis Number ->	UB06602		UB06642		UB06643		UB06644		UB06645		UB06646		UB06647		UB06603		UB06604	
Explosives (ug/g)																		
2,4,6-Trinitrotoluene	2.55	UJ4	4.71	J4	6,527.78	J4	2.85	J6	2.68	UJ4	2.42	UJ4	2.49	UJ4	48.54	J4	2.51	UJ4
2,4-Dinitrotoluene	3.18	UJ4	25.31	J4	56.67	J4	2.86	UJ4	3.35	UJ4	3.02	UJ4	3.12	UJ4	3.05	UJ4	3.14	UJ4
2,6-Dinitrotoluene	2.55	U	2.44	U	112.50		2.29	U	2.68	U	2.42	U	2.49	U	2.44	U	2.51	U
Cyclotetramethylenetetranitramine	2.55	U	2.44	U	7.28	J9	2.29	U	2.68	U	2.42	U	2.49	U	2.44	U	2.51	U
Cyclonite (RDX)	1.63	UJ4	1.56	UJ4	1.78	UJ4	1.46	UJ4	1.72	UJ4	1.55	UJ4	1.60	UJ4	1.56	UJ4	1.61	UJ4
TETRAIL	2.69	U	2.58	U	2.93	U	2.41	U	2.63	U	2.55	U	2.63	U	2.57	U	2.65	U

Field Sample Number ->	54SB10A		54SB10B		54SB10D		54SB11A		54SB11B		54SB12A		54SB12B		54SB13A		54SB13B	
Lab Analysis Number ->	UB06605		UB06606		UB06607		UB06631		UB06632		UB06633		UB06634		UB06635		UB06636	
Explosives (ug/g)																		
2,4,6-Trinitrotoluene	2.42	UJ4	2.45	UJ4	11.67	J4	2.43	UJ4	2.42	UJ4	2.50	UJ4	2.66	UJ4	2.45	UJ4	2.42	UJ4
2,4-Dinitrotoluene	3.02	UJ4	3.06	UJ4	2.86	UJ4	3.04	UJ4	3.03	UJ4	3.12	UJ4	3.32	UJ4	3.07	UJ4	3.03	UJ4
2,6-Dinitrotoluene	2.42	U	2.45	U	2.29	U	2.43	U	2.42	U	2.50	U	2.66	U	2.45	U	2.42	U
Cyclotetramethylenetetranitramine	2.42	U	2.45	U	2.29	U	2.43	U	2.42	U	2.50	U	2.66	U	2.45	U	2.42	U
Cyclonite (RDX)	1.55	UJ4	1.57	UJ4	1.46	UJ4	1.56	UJ4	1.55	UJ4	1.60	UJ4	1.70	UJ4	1.57	UJ4	1.55	UJ4
TETRYL	2.55	U	2.59	U	2.41	U	2.56	U	2.55	U	2.63	U	2.80	U	2.59	U	2.55	U

Field Sample Number ->	54SB14A		54SB14B		54SB15A		54SB16A		54SB16B		54SB16D		SCSE1		SCSE2		SCSE3	
Lab Analysis Number ->	UB06637		UB06638		UB06648		UB06639		UB06640		UB06641		UC00193		UC00194		UC00195	
Explosives (ug/g)																		
2,4,6-Trinitrotoluene	2.36	UJ4	2.41	UJ4	2.47	UJ4	2.45	UJ4	2.47	UJ4	2.49	UJ4	2.46	UJ4	2.95	UJ4	2.84	UJ4
2,4-Dinitrotoluene	2.95	UJ4	3.01	UJ4	3.09	UJ4	3.06	UJ4	3.09	UJ4	3.11	UJ4	3.08	UJ4	3.69	UJ4	3.55	UJ4
2,6-Dinitrotoluene	2.36	U	2.41	U	2.47	U	2.45	U	2.47	U	2.49	U	2.46	U	2.95	U	2.84	U
Cyclotetramethylenetetranitramine	2.36	U	2.41	U	2.47	U	2.45	U	2.47	U	2.49	U	2.46	U	2.95	U	2.84	U
Cyclonite (RDX)	1.51	UJ4	1.54	UJ4	1.58	UJ4	1.57	UJ4	1.58	UJ4	1.59	UJ4	1.57	UJ4	1.89	UJ4	1.82	UJ4
TETRYL	2.49	U	2.54	U	2.60	U	2.58	U	2.60	U	2.62	U	2.60	U	3.11	U	2.99	U

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Field Sample Number ->	17ASB105		17ASB110		17ASB115		17ASB120		17ASB122		17ASB205		17ASB210		17ASB215		17ASB220		17ASB225	
Lab Analysis Number ->	UB06429		UB06430		UB06431		UB06432		UB06433		UB06435		UB06436		UB06437		UB06438		UB06439	
Metals (ug/g)																				
Arsenic	94.87 J4		9.30 J4		13.50 J4		16.69 J4		3.27 UJ4		7.33 J4		2.99 UJ4		8.98 J4		3.84 UJ4		3.58 UJ4	
Selenium	0.58 UJ4		0.57 UJ4		0.55 UJ4		0.56 UJ4		0.59 UJ4		0.56 UJ4		0.54 UJ4		0.65 UJ4		0.69 UJ4		0.64 UJ4	
Lead	5,256.41 J6		101.39 J6		56.44 J6		273.97 J6		11.79 J6		26.28 J6		14.13 J6		69.06 J6		41.78 J6		77.36 J6	
Silver	42.31 J4		0.39 J4		0.02 UJ4		2.12 J4		0.02 UJ4		0.02 UJ4		0.01 UJ4		0.02 UJ4		0.02 UJ4		0.02 UJ4	
Barium	5,128.21 J1		63.12 J1		69.20 J1		69.36 J1		71.50 J1		64.38 J1		75.69 J1		86.91 J1		134.26 J1		9.56 J1	
Beryllium	1.65 J4		2.22 J4		2.11 J4		1.77 J4		2.13 J4		2.23 J4		2.06 J4		4.52 J4		6.82 J4		0.61 UJ4	
Cadmium	13.72		1.52 U		1.47 U		1.48 U		1.57 U		1.48 U		1.44 U		1.73 U		1.84 U		1.72 U	
Chromium	2,051.28 J6		55.51 J6		54.72 J6		54.92 J6		68.50 J6		46.82 J6		49.70 J6		86.04 J6		122.27 J6		7.56 J6	
Nickel	902.56 J4		24.84 J4		29.20 J4		24.28 J4		28.37 J4		26.15 J4		27.78 J4		56.83 J4		78.96 J4		6.12 J4	
Antimony	77.95		24.84 U		24.05 U		24.41 U		25.62 U		24.41 U		23.47 U		28.20 U		30.11 U		28.08 U	
Thallium	43.97 UJ4		43.47 UJ4		42.09 UJ4		42.71 UJ4		44.84 UJ4		42.71 UJ4		41.08 UJ4		49.35 UJ4		52.69 UJ4		49.14 UJ4	
Mercury	0.29 J4		0.14 J4		0.16 J4		0.11 J4		0.09 J4		0.18 J4		0.06 UJ4		0.12 J4		0.08 UJ4		0.07 UJ4	

Sheet1

Field Sample Number ->	17ASS3		17ASB305		17ASB310		17ASB315		17ASB320		17ASB325		17ASB340		17BSS1		17BSS2		17CSB105	
Lab Analysis Number ->	UB06441		UB06442		UB06443		UB06444		UB06445		UB06446		UB06447		UB06463		UB06464		UB06465	
Metals (ug/g)																				
Arsenic	101.70	J4	6.70	J4	7.51	J4	4.64	J4	3.75	J4	2.74	UJ4	3.30	J4	127.72	J4	18.18	J4	11.98	J4
Selenium	0.54	UJ4	0.68	UJ4	0.66	UJ4	0.61	UJ4	0.49	UJ4	0.49	UJ4	0.49	UJ4	0.65	UJ4	0.65	UJ4	0.55	UJ4
Lead	4,721.55	J6	27.08	J6	23.02	J6	21.83	J6	30.77	J6	9.23	J6	15.70	J6	65.12	J1	128.43	J1	41.82	J1
Silver	2.18	J4	0.02	UJ4	0.02	UJ4	0.02	UJ4	0.01	UJ4	0.01	UJ4	0.01	UJ4	1.89	J4	0.13	J4	0.02	UJ4
Barium	577.48	J1	71.26	J1	126.39	J1	45.16	J1	52.97	J1	54.71	J1	34.58	J1	261.25	J1	99.42	J1	29.40	J1
Beryllium	0.98	J4	3.40	J4	7.39	J4	2.20	J4	0.57	J4	0.77	J4	1.55	J4	1.41	J4	5.61	J4	3.23	J4
Cadmium	4.29		1.82	U	1.76	U	1.64	U	1.32	U	1.32	U	1.32	U	3.12	J4	1.73	UJ4	1.48	UJ4
Chromium	222.76	J6	53.71	J6	79.33	J6	75.99	J6	17.25	J6	22.59	J6	45.44	J6	144.41		76.05		61.87	
Nickel	69.13	J4	34.64	J4	71.26	J4	36.43	J4	6.30	J4	10.90	J4	23.71	J4	40.49	J4	51.80	J4	25.95	J4
Antimony	23.73	U	29.65	U	28.74	U	26.74	U	21.54	U	21.49	U	21.51	U	28.45	UJ4	28.28	UJ4	24.11	UJ4
Thallium	41.53	UJ4	51.89	UJ4	50.29	UJ4	46.79	UJ4	37.69	UJ4	37.61	UJ4	37.65	UJ4	49.78	UJ4	49.49	UJ4	42.19	UJ4
Mercury	0.33	J4	0.18	J4	0.13	J4	0.07	UJ4	0.05	UJ4	0.05	UJ4	0.05	UJ4	0.25	J4	0.07	UJ4	0.06	UJ4

Field Sample Number ->	17CSB110		17CSB114		17CSB205		17CSB210		17CSB215		17CSB240		17DSB105		17DSB110		17DSB115		17DSB120	
Lab Analysis Number ->	UB06466		UB06467		UB06469		UB06470		UB06471		UB06473		UB06476		UB06477		UB06478		UB06479	
Metals (ug/g)																				
Arsenic	3.42	UJ4	3.32	UJ4	3.11	UJ4	3.70	UJ4	4.59	J4	3.88	UJ4	3.20	UJ4	3.09	UJ4	3.21	UJ4	3.34	UJ4
Selenium	0.61	UJ4	0.60	UJ4	0.56	UJ4	0.66	UJ4	0.57	UJ4	0.70	UJ4	0.57	UJ4	0.56	UJ4	0.58	UJ4	0.60	UJ4
Lead	18.44	J1	18.73	J1	12.20	J1	13.68	J1	190.60	J1	17.24	J1	20.08	J1	17.95	J1	26.54	J1	12.36	J1
Silver	0.02	UJ4	0.02	UJ4	0.02	UJ4	0.02	UJ4	0.04	J4	0.02	UJ4	0.03	J4	0.02	UJ4	0.02	UJ4	0.02	UJ4
Barium	78.55	J1	84.33	J1	36.74	J1	70.12	J1	104.70	J1	86.49	J1	68.93	J1	60.40	J1	67.05	J1	69.69	J1
Beryllium	5.19	J4	3.61	J4	1.56	J4	5.77	J4	2.52	J4	6.21	J4	1.83	J4	2.02	J4	3.21	J4	3.04	J4
Cadmium	1.64	UJ4	1.59	UJ4	1.49	UJ4	1.78	UJ4	4.73	J4	1.86	UJ4	1.53	UJ4	1.49	UJ4	1.54	UJ4	1.60	UJ4
Chromium	72.81		59.89		33.62		54.29		71.92		74.38		29.92		43.94		67.82		56.07	
Nickel	46.17	J4	35.33	J4	18.68	J4	46.60	J4	45.62	J4	56.83	J4	14.58	J4	11.21	J4	28.97	J4	45.53	J4
Antimony	26.78	UJ4	26.03	UJ4	24.41	UJ4	28.99	UJ4	24.90	UJ4	30.43	UJ4	25.06	UJ4	24.26	UJ4	25.13	UJ4	26.17	UJ4
Thallium	46.86	UJ4	45.55	UJ4	42.71	UJ4	50.74	UJ4	43.58	UJ4	53.26	UJ4	43.86	UJ4	42.45	UJ4	43.97	UJ4	45.79	UJ4
Mercury	0.10	J4	0.07	UJ4	0.06	UJ4	0.07	UJ4	0.06	UJ4	0.08	UJ4	0.06	UJ4	0.06	UJ4	0.06	UJ4	0.07	UJ4

Field Sample Number ->	17DSB125		17DSB205		17DSB210		17DSB127		17DSB215		17DSB220		17DSB225		17DSB240		SPG3SE1		31MW1A25	
Lab Analysis Number ->	UB06480		UB06483		UB06484		UB06481		UB06485		UB06486		UB06487		UB06488		UC00174		UB06565	
Metals (ug/g)																				
Arsenic	3.99 UJ4		3.08 UJ4		6.32 J4		4.16 UJ4		11.32 J4		4.08 UJ4		3.54 UJ4		8.03 J4		17.40 J4		2.61 UJ4	
Selenium	0.72 UJ4		0.55 UJ4		0.58 UJ4		0.75 UJ4		0.73 UJ4		0.73 UJ4		0.64 UJ4		0.57 UJ4		0.70 UJ4		0.47 UJ4	
Lead	28.23 J1		20.81 J1		17.87 J1		23.46 J1		23.10 J1		11.31 J1		8.43 J1		14.63 J1		548.59 J6		0.63 J6	
Silver	0.02 UJ4		0.02 UJ4		0.02 UJ4		0.07 J4		0.02 UJ4		0.02 UJ4		0.02 UJ4		0.02 UJ4		0.22 J4		0.01 UJ4	
Barium	72.73 J1		65.89 J1		80.98 J1		111.48 J1		142.65 J1		111.91 J1		55.95 J1		68.85 J1		700.63 J1		28.11 J1	
Beryllium	4.77 J4		1.42 J4		2.48 J4		5.89 J4		7.88 J4		5.48 J4		11.84 J4		2.23 J4		4.23 J4		0.94 J4	
Cadmium	1.91 UJ4		1.48 UJ4		1.54 UJ4		2.00 UJ4		1.94 UJ4		1.96 UJ4		1.70 UJ4		1.51 UJ4		1.88 UJ4		1.25 UJ4	
Chromium	86.92		31.28		56.30		77.87		97.09		63.30		77.76		49.18		62.70 J6		18.50 J6	
Nickel	50.40 J4		11.18 J4		28.79 J4		66.39 J4		72.05 J4		57.42 J4		87.82 J4		23.33 J4		52.98 J4		23.62 J4	
Antimony	31.26 UJ4		24.14 UJ4		25.19 UJ4		32.61 UJ4		31.66 UJ4		31.97 UJ4		27.76 UJ4		24.72 UJ4		30.72 UJ4		20.48 UJ4	
Thallium	54.70 UJ4		42.24 UJ4		44.09 UJ4		57.07 UJ4		55.41 UJ4		55.95 UJ4		48.58 UJ4		43.25 UJ4		53.76 UJ4		35.84 UJ4	
Mercury	0.08 UJ4		0.06 UJ4		0.06 UJ4		0.15 J4		0.24 J4		0.08 UJ4		0.07 UJ4		0.06 UJ4		0.13 J4		0.09 UJ4	

Field Sample Number ->	31MW1B35		31MW2A		31MW2B		31MW3A10		31MW3B20		31MW4A12		31MW4B22		31MW4C40		48SS1		48SS2	
Lab Analysis Number ->	UB06566		UB06474		UB06475		UB06516		UB06517		UB06518		UB06519		UB06520		UB06558		UB06559	
Metals (ug/g)																				
Arsenic	2.65	UJ4	3.09	UJ4	4.40	J4	2.92	UJ4	2.78	UJ4	2.87	UJ4	2.71	UJ4	2.90	UJ4	4.53	J4	9.78	J4
Selenium	0.48	UJ4	0.56	UJ4	0.54	UJ4	0.52	UJ4	0.50	UJ4	0.52	UJ4	0.49	UJ4	0.52	UJ4	0.59	UJ4	1.31	UJ4
Lead	7.32	J6	21.16	J1	20.86	J1	31.54	J1	40.00	J1	17.70	J1	13.96	J1	19.98	J1	5.83	J6	196.32	J6
Silver	0.02	J4	0.02	UJ4	0.01	UJ4	0.01	UJ4	0.11	J4	0.01	UJ4	0.01	UJ4	0.01	UJ4	0.02	UJ4	0.03	J4
Barium	58.39	J1	134.90	J1	97.33	J1	134.00	J1	75.10	J1	136.78	J1	82.68	J1	140.53	J1	757.62	J1	100.98	J1
Beryllium	1.18	J4	1.00	J4	1.06	J4	0.95	J4	0.75	J4	1.18	J4	0.83	J4	1.22	J4	2.15	J4	0.91	J4
Cadmium	1.27	UJ4	1.49	UJ4	1.33	UJ4	1.20	UJ4	1.20	UJ4	1.38	UJ4	1.30	UJ4	1.39	UJ4	1.59	UJ4	1.47	UJ4
Chromium	24.10	J6	43.94		34.60		26.80		19.50		43.91		32.03		44.13		7.07	J6	58.65	J6
Nickel	30.89	J4	13.37	J4	22.78	J4	12.60	J4	13.30	J4	20.23	J4	18.18	J4	21.49	J4	11.83	J4	31.17	J4
Antimony	20.81	UJ4	24.26	UJ4	21.78	UJ4	19.60	UJ4	19.60	UJ4	22.53	UJ4	21.21	UJ4	22.76	UJ4	25.96	UJ4	24.05	UJ4
Thallium	36.41	UJ4	42.45	UJ4	38.11	UJ4	34.30	UJ4	34.30	UJ4	39.43	UJ4	37.12	UJ4	39.84	UJ4	45.43	UJ4	42.09	UJ4
Mercury	0.05	UJ4	0.06	UJ4	0.07	J4	0.18	J4	0.06	UJ4	0.06	UJ4	0.05	UJ4	0.06	UJ4	1.47	J4	0.54	J4

Field Sample Number ->	48SS3		48SS4		48SS5		48SS6		48SS8		54SB1A		54SB1B		54SB2A		54SB2B		54SB3A	
Lab Analysis Number ->	UB06560		UB06561		UB06562		UB06563		UB06564		UB06593		UB06594		UB06595		UB06596		UB06597	
Metals (ug/g)																				
Arsenic	2.90 UJ4		4.35 J4		3.09 UJ4		4.46 J4		4.76 J4		2.94 UJ4		2.74 UJ4		3.27 J4		3.07 UJ4		2.87 UJ4	
Selenium	0.52 UJ4		0.79 J4		0.56 UJ4		0.53 UJ4		0.78 J4		0.53 UJ4		0.49 UJ4		0.50 UJ4		0.55 UJ4		0.52 UJ4	
Lead	20.88 J6		25.53 J6		27.19 J6		16.49 J6		38.55 J6		716.80 J6		5.77 J6		2,354.26 J6		14.23 J6		321.64 J6	
Silver	0.03 J4		0.03 J4		0.02 UJ4		0.03 J4		0.02 J4		0.07 J4		0.01 UJ4		0.03 J4		0.03 J4		0.03 J4	
Barium	125.29 J1		135.39 J1		66.63 J1		139.18 J1		110.72 J1		164.51 J1		307.44 J1		224.22 J1		175.46 J1		178.16 J1	
Beryllium	1.01 J4		0.51 UJ4		0.77 J4		0.87 J4		1.31 J4		0.93 J4		0.47 UJ4		1.76 J4		1.33 J4		1.11 J4	
Cadmium	1.39 UJ4		1.43 UJ4		1.48 UJ4		1.40 UJ4		1.45 UJ4		2.40 J4		1.31 UJ4		1.35 UJ4		1.47 UJ4		1.38 UJ4	
Chromium	28.19 J6		17.10 J6		37.45 J6		18.60 J6		37.59 J6		25.38 J6		9.80 J6		27.91 J6		29.45 J6		28.16 J6	
Nickel	7.11 J4		7.17 J4		12.73 J4		6.75 J4		14.22 J4		11.66 J4		6.23 J4		10.25 J4		16.69 J4		13.45 J4	
Antimony	22.74 UJ4		23.28 UJ4		24.23 UJ4		22.92 UJ4		23.61 UJ4		23.03 UJ4		21.44 UJ4		21.97 UJ4		24.05 UJ4		22.53 UJ4	
Thallium	39.79 UJ4		40.74 UJ4		42.40 UJ4		40.12 UJ4		41.33 UJ4		40.31 UJ4		37.53 UJ4		38.45 UJ4		42.09 UJ4		39.43 UJ4	
Mercury	0.06 UJ4		0.59 J4		0.13 J4		0.06 UJ4		0.39 J4		0.09 J4		0.05 UJ4		0.13 J4		0.06 UJ4		5.06 J4	

Field Sample Number ->	54SB3B		54SB4A		54SB4B		54SB5A		54SB5B		54SB6A		54SB6B		54SB7A		54SB7B		54SB8A	
Lab Analysis Number ->	UB06598		UB06599		UB06600		UB06601		UB06602		UB06642		UB06643		UB06644		UB06645		UB06646	
Metals (ug/g)																				
Arsenic	3.29 UJ4		3.10 UJ4		3.01 UJ4		3.12 UJ4		3.18 UJ4		4.08 J4		3.47 UJ4		2.86 UJ4		3.35 UJ4		3.02 UJ4	
Selenium	0.59 UJ4		0.56 UJ4		0.54 UJ4		0.56 UJ4		0.57 UJ4		0.55 UJ4		0.62 UJ4		0.51 UJ4		0.60 UJ4		0.54 UJ4	
Lead	14.74 J6		84.26 J6		8.36 J6		39.90 J6		16.82 J6		3,789.73 J6		430.56 J6		50.29 J6		22.79 J6		229.75 J6	
Silver	0.04 J4		0.04 J4		0.03 J4		0.04 J4		0.05 J4		0.35 J4		0.02 UJ4		0.01 UJ4		0.02 UJ4		0.04 UJ4	
Barium	87.63 J1		313.51 J1		108.30 J1		281.80 J1		244.59 J1		1,077.02 J1		362.50 J1		138.29 J1		420.91 J1		188.63 J1	
Beryllium	0.56 UJ4		1.78 J4		0.51 UJ4		1.55 J4		1.61 J4		1.11 J4		2.43 J4		0.82 J4		2.47 J4		1.15 J4	
Cadmium	1.58 UJ4		1.49 UJ4		1.44 UJ4		1.50 UJ4		1.53 UJ4		11.75 J4		1.67 UJ4		1.37 UJ4		1.61 UJ4		1.45 UJ4	
Chromium	37.76 J6		35.56 J6		21.30 J6		34.54 J6		40.64 J6		136.92 J6		70.14 J6		24.00 J6		57.10 J6		27.69 J6	
Nickel	10.26 J4		21.44 J4		9.19 J4		21.20 J4		24.46 J4		16.99 J4		30.14 J4		12.34 J4		34.72 J4		15.60 J4	
Antimony	25.79 UJ4		24.29 UJ4		23.59 UJ4		24.44 UJ4		24.97 UJ4		23.96 UJ4		27.22 UJ4		22.40 UJ4		26.27 UJ4		23.70 UJ4	
Thallium	45.13 UJ4		42.50 UJ4		41.28 UJ4		42.77 UJ4		43.69 UJ4		41.93 UJ4		47.64 UJ4		39.20 UJ4		45.98 UJ4		41.48 UJ4	
Mercury	0.21 J4		0.06 UJ4		0.06 UJ4		0.06 UJ4		0.06 UJ4		72.13 J4		0.07 UJ4		0.06 UJ4		0.07 UJ4		0.06 UJ4	

Sheet1

Field Sample Number ->	54SB8B		54SB9A		54SB9B		54SB10A		54SB10B		54SB10D		54SB11A		54SB11B		54SB12A	
Lab Analysis Number ->	UB06647		UB06603		UB06604		UB06605		UB06606		UB06607		UB06631		UB06632		UB06633	
Metals (ug/g)																		
Arsenic	3.12	UJ4	3.05	UJ4	3.14	UJ4	4.28	J4	3.06	UJ4	2.86	UJ4	3.04	UJ4	3.03	UJ4	3.12	UJ4
Selenium	0.56	UJ4	0.55	UJ4	0.56	UJ4	0.54	UJ4	0.55	UJ4	0.51	UJ4	0.55	UJ4	0.54	UJ4	0.56	UJ4
Lead	21.20	J6	20.85	J6	15.83	J6	205.56	J6	11.69	J6	13.16	J6	91.13	J6	12.11	J6	21.22	J6
Silver	0.02	UJ4	0.03	UJ4	0.04	J4	0.07	J4	0.03	J4	0.03	J4	0.02	UJ4	0.02	UJ4	0.02	UJ4
Barium	243.14	J1	193.96	J1	201.01	J1	319.23	J1	158.09	J1	141.68	J1	223.57	J1	175.55	J1	235.96	J1
Beryllium	1.72	J4	1.39	J4	1.53	J4	1.81	J4	1.20	J4	1.03	J4	1.49	J4	1.34	J4	1.54	J4
Cadmium	1.50	UJ4	1.46	UJ4	1.51	UJ4	1.45	UJ4	1.47	UJ4	1.37	UJ4	1.46	UJ4	1.45	UJ4	1.50	UJ4
Chromium	40.15	J6	27.93	J6	37.56	J6	33.86	J6	29.78	J6	27.23	J6	33.17	J6	32.93	J6	36.08	J6
Nickel	25.56	J4	17.68	J4	22.61	J4	19.71	J4	18.01	J4	15.45	J4	20.05	J4	18.89	J4	20.10	J4
Antimony	24.44	UJ4	23.90	UJ4	24.62	UJ4	23.70	UJ4	24.62	UJ4	22.43	UJ4	23.82	UJ4	23.73	UJ4	24.47	UJ4
Thallium	42.77	UJ4	41.83	UJ4	43.09	UJ4	41.48	UJ4	42.03	UJ4	39.24	UJ4	41.68	UJ4	41.53	UJ4	42.82	UJ4
Mercury	0.06	UJ4	0.06	UJ4	0.06	UJ4	0.06	UJ4	0.12	J4	0.06	UJ4	0.06	UJ4	0.06	UJ4	0.06	UJ4

Field Sample Number ->	54SB12B		54SB13A		54SB13B		54SB14A		54SB14B		54SB15A		54SB16A		54SB16B		54SB16D	
Lab Analysis Number ->	UB06634		UB06635		UB06636		UB06637		UB06638		UB06648		UB06639		UB06640		UB06641	
Metals (ug/g)																		
Arsenic	3.32	UJ4	3.07	UJ4	3.03	UJ4	2.95	UJ4	3.01	UJ4	3.09	UJ4	3.06	UJ4	3.09	UJ4	3.11	UJ4
Selenium	0.60	UJ4	0.55	UJ4	0.54	UJ4	0.53	UJ4	0.54	UJ4	0.55	UJ4	0.55	UJ4	0.55	UJ4	0.56	UJ4
Lead	13.28	J6	134.97	J6	8.23	J6	36.56	J6	13.25	J6	28.40	J6	31.82	J6	14.81	J6	13.68	J6
Silver	0.02	UJ4	0.07	J4	0.02	UJ4	0.01	UJ4	0.01	UJ4	0.02	UJ4	0.02	UJ4	0.02	UJ4	0.02	UJ4
Barium	248.34	J1	226.99	J1	118.64	J1	153.30	J1	166.27	J1	338.27	J1	231.33	J1	203.70	J1	237.56	J1
Beryllium	1.82	J4	1.42	J4	0.52	UJ4	0.89	J4	1.08	J4	1.93	J4	1.47	J4	1.48	J4	1.77	J4
Cadmium	1.59	UJ4	1.47	UJ4	1.45	UJ4	1.42	UJ4	1.45	UJ4	1.48	UJ4	1.47	UJ4	1.48	UJ4	1.49	UJ4
Chromium	46.48	J6	31.29	J6	32.32	J6	28.52	J6	34.10	J6	45.93	J6	34.27	J6	34.20	J6	43.53	J6
Nickel	26.43	J4	18.90	J4	13.20	J4	10.38	J4	20.12	J4	26.05	J4	20.56	J4	20.12	J4	24.25	J4
Antimony	26.03	UJ4	24.05	UJ4	23.73	UJ4	23.11	UJ4	23.61	UJ4	24.20	UJ4	23.99	UJ4	24.20	UJ4	24.38	UJ4
Thallium	45.55	UJ4	42.09	UJ4	41.53	UJ4	40.45	UJ4	41.33	UJ4	42.35	UJ4	41.98	UJ4	42.35	UJ4	42.66	UJ4
Mercury	0.07	UJ4	0.06	UJ4	0.06	UJ4	0.06	UJ4	0.06	UJ4	0.06	UJ4	0.06	UJ4	0.06	UJ4	0.06	UJ4

Field Sample Number ->	SCSE1		SCSE2		SCSE3	
Lab Analysis Number ->	UC00193		UC00194		UC00195	
Metals (ug/g)						
Arsenic	10.59	J4	9.03	J4	6.70	J4
Selenium	0.55	UJ4	0.66	UJ4	0.64	UJ4
Lead	13.41	J6	95.87	J6	31.21	J6
Silver	0.03	J4	0.18	J4	0.21	J4
Barium	141.45	J1	240.41	J1	262.41	J1
Beryllium	1.38	J4	1.45	J4	1.39	J4
Cadmium	1.48	UJ4	1.77	UJ4	1.70	UJ4
Chromium	27.80	J6	39.53	J6	36.17	J6
Nickel	32.60	J4	26.99	J4	26.10	J4
Antimony	24.11	UJ4	28.91	UJ4	27.80	UJ4
Thallium	42.19	UJ4	50.59	UJ4	48.65	UJ4
Mercury	0.06	UJ4	0.07	UJ4	0.07	UJ4

Field Sample Number ->	48SB4A11		48SB4B21		48SB5A19		48SB5B37		48SS1		48SS2		48SS3		48SS4		48SS5
Lab Analysis Number ->	UB06567		UB06568		UB06572		UB06573		UB06558		UB06559		UB06560		UB06561		UB06562
TOTAL PETROLEUM HYDROCARBONS (ug/g)	12.76 U		12.09 U		4,337.79		12.33 U		13.25 U		12.27 U		11.60 U		14.25		414.09

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Field Sample Number ->	48SS6	48SS8	48MW1A22	48MW1B54	48MW2A42	48MW2B46	48MW3A22	48MW3B32
Lab Analysis Number ->	UB06563	UB06564	UB06575	UB06576	UB06585	UB06586	UC00028	UC00029
TOTAL PETROLEUM HYDROCARBONS (ug/g)	11.70 U	12.05 U	12.72 U	13.53 U	11.55 U	10.88 U	12.15 U	12.44 U

Field Sample Number ->	17ASB1		17ASB2		17ASB3		17CSB1		17CSB1		17CSB2		17DSB2		48SB4		48SB5		54SB1		54SB2	
Lab Analysis Number ->	UB06434		UB06440		UB06448		UB06468		UB06482		UB06472		UB06489		UB06569		UB06574		UB06608		UB06609	
*PH	7.46		7.06		7.63		8.08		7.45		7.19		7.62		4.79		5.31		7.00		6.92	

Field Sample Number ->	17ASB1	17ASB2	17ASB3	17CSB1	17CSB1	17CSB2	17DSB2	48SB4	48SB5	54SB1	54SB2	
Lab Analysis Number ->	UB06434	UB06440	UB06448	UB06468	UB06482	UB06472	UB06489	UB06569	UB06574	UB06608	UB06609	
*PH	7.46	7.06	7.63	8.08	7.45	7.19	7.62	4.75	5.31	7.00	6.92	

DATA SUMMARY TABLES FOR JULY 1995 SAMPLING EVENT

Field Sample Number ->	NRSW1	NRSW2	NRSW3	NRSW4	NRSW5	NRSW6	NRSW8
Lab Analysis Number ->	UC02381	UC02382	UC02383	UC02481	UC02272	UC02482	UC02273
Volatile Organics (ug/L)							
1,1,1-Trichloroethane	1 U	1 U	1 U	1 U	1 U	1 U	1 U
1,1,2-Trichloroethane	1 U	1 U	1 U	1 U	1 U	1 U	1 U
1,1-Dichloroethene	1 U	1 U	1 U	1 U	1 U	1 U	1 U
1,1-Dichloroethane	1 U	1 U	1 U	1 U	1 U	1 U	1 U
*1,2-DICHLOROETHYLENES (Total)	5 U	5 U	5 U	5 U	5 U	5 U	5 U
1,2-Dichloroethane	1 U	1 U	1 U	1 U	1 U	1 U	1 U
1,2-Dichloropropane	1 U	1 U	1 U	1 U	1 U	1 U	1 U
Acetone	8 U	8 U	8 U	8 U	8 U	8 U	8 U
Acrylonitrile	8.4 U	8.4 U	8.4 U	8.4 U	8.4 U	8.4 U	8.4 U
Bromodichloromethane	1 U	1 U	1 U	1 U	1 U	1 U	1 U
Vinyl chloride	12 U	12 U	12 U	12 U	12 U	12 U	12 U
Chloroethane	8 U	8 U	8 U	8 U	8 U	8 U	8 U
Benzene	1 U	1 U	1 U	1 U	1 U	1 U	1 U
Trichlorofluoromethane	1 U	1 U	1 U	1 U	1 U	1 U	1 U
Carbon tetrachloride	1 U	1 U	1 U	1 U	1 U	1 U	1 U
Methylene chloride	1 U	1 U	1 U	1 U	1 U	1 U	1 U
Bromomethane	14 U	14 U	14 U	14 U	14 U	14 U	14 U
Chloromethane	1.2 U	1.2 U	1.2 U	1.2 U	1.2 U	1.2 U	1.2 U
Bromoform	11 U	11 U	11 U	11 U	11 U	11 U	11 U
Chloroform	1 U	1 U	1 U	1 U	1 U	1 U	1 U
Chlorobenzene	1 U	1 U	1 U	1 U	1 U	1 U	1 U
Ethylbenzene	1 U	1 U	1 U	1 U	1 U	1 U	1 U
Toluene	1 U	1 U	1 U	1 U	1 U	1 U	1 U
2-BUTANONE	10 U	10 U	10 U	10 U	10 U	10 U	10 U
4-METHYL-2-PENTANONE	1.4 U	1.4 U	1.4 U	1.4 U	1.4 U	1.4 U	1.4 U
1,1,2,2-Tetrachloroethane	1.5 U	1.5 U	1.5 U	1.5 U	1.5 U	1.5 U	1.5 U
Tetrachloroethene	1 U	1 U	1 U	1 U	1 U	1 U	1 U
Trichloroethene	1 U	1 U	1 U	1 U	1 U	1 U	1 U
XYLENES, TOTAL	2 UJ8	2 UJ8	2 UJ8	2 UJ8	2 UJ8	2 U	2 UJ8

Field Sample Number ->	48MW1	48MW2	48MW3	48MW4	NRSEQ	NRSWTB	NRSWFB
Lab Analysis Number ->	UC02306	UC02305	UC02385	UC02480	UC02264	UC02260	UC02265
Volatile Organics (ug/L)							
1,1,1-Trichloroethane	4.1	0.98	1 U	1 U	1 U	1 U	1 U
1,1,2-Trichloroethane	1 U	1 U	1 U	1 U	1 U	1 U	1 U
1,1-Dichloroethene	1.1	1 U	1 U	1 U	1 U	1 U	1 U
1,1-Dichloroethane	2.3	1 U	1 U	1 U	1 U	1 U	1 U
*1,2-DICHLOROETHYLENES (Total)	5 U	5 U	5 U	5 U	5 U	5 U	5 U
1,2-Dichloroethane	1 U	1 U	1 U	1 U	1 U	1 U	1 U
1,2-Dichloropropane	1 U	1 U	1 U	1 U	1 U	1 U	1 U
Acetone	8 U	8 U	8 U	8 U	8 U	8 U	8 U
Acrylonitrile	8.4 U	8.4 U	8.4 U	8.4 U	8.4 U	8.4 U	8.4 U
Bromodichloromethane	1 U	1 U	1 U	1 U	1 U	1 U	1 U
Vinyl chloride	12 U	12 U	12 U	12 U	12 U	12 U	12 U
Chloroethane	8 U	8 U	8 U	8 U	8 U	8 U	8 U
Benzene	1 U	1 U	1 U	1 U	1 U	1 U	1 U
Trichlorofluoromethane	1 U	1 U	1 U	1 U	1 U	1 U	1 U
Carbon tetrachloride	1 U	92	100	1 U	1 U	1 U	1 U
Methylene chloride	1 U	1.1 U1	1 U	1 U	1 U	4.2	1 U
Bromomethane	14 U	14 U	14 U	14 U	14 U	14 U	14 U
Chloromethane	1.2 U	1.2 U	1.2 U	1.2 U	1.2 U	1.2 U	1.2 U
Bromoform	11 U	11 U	11 U	11 U	11 U	11 U	11 U
Chloroform	1 U	6.7	30	1 U	1 U	1 U	1 U
Chlorobenzene	1 U	1 U	1 U	1 U	1 U	1 U	1 U
Ethylbenzene	1 U	1 U	1 U	1 U	1 U	1 U	1 U
Toluene	1 U	1 U	1 U	1 U	1 U	1 U	1 U
2-BUTANONE	10 U	10 U	10 U	10 U	10 U	10 U	10 U
4-METHYL-2-PENTANONE	1.4 U	1.4 U	1.4 U	1.4 U	1.4 U	1.4 U	1.4 U
1,1,2,2-Tetrachloroethane	1.5 U	1.5 U	1.5 U	1.5 U	1.5 U	1.5 U	1.5 U
Tetrachloroethene	1.2	1 U	1 U	1 U	1 U	1 U	1 U
Trichloroethene	17	11	37	1 U	1 U	1 U	1 U
XYLENES, TOTAL	2 UJ8	2 UJ8	2 UJ8	2 U	2 UJ8	2 UJ8	2 UJ8

Field Sample Number ->	48MWTB	48MWTB2	NRSWTB1	NRSWTB3
Lab Analysis Number ->	UC02307	UC02483	UC02267	UC02386
Volatile Organics (ug/L)				
1,1,1-Trichloroethane	1 U	1 U	1 U	1 U
1,1,2-Trichloroethane	1 U	1 U	1 U	1 U
1,1-Dichloroethene	1 U	1 U	1 U	1 U
1,1-Dichloroethane	1 U	1 U	1 U	1 U
*1,2-DICHLOROETHYLENES (Total)	5 U	5 U	5 U	5 U
1,2-Dichloroethane	1 U	1 U	1 U	1 U
1,2-Dichloropropane	1 U	1 U	1 U	1 U
Acetone	16	54	8 U	8 U
Acrylonitrile	8.4 U	8.4 U	8.4 U	8.4 U
Bromodichloromethane	1 U	1 U	1 U	1 U
Vinyl chloride	12 U	12 U	12 U	12 U
Chloroethane	8 U	8 U	8 U	8 U
Benzene	1 U	1 U	1 U	1 U
Trichlorofluoromethane	1 U	1 U	1 U	1 U
Carbon tetrachloride	1 U	1 U	1 U	1 U
Methylene chloride	2.9	2.6	4.5	1 U
Bromomethane	14 U	14 U	14 U	14 U
Chloromethane	1.2 U	1.2 U	1.2 U	1.2 U
Bromoform	11 U	11 U	11 U	11 U
Chloroform	1 U	1 U	1 U	1 U
Chlorobenzene	1 U	1 U	1 U	1 U
Ethylbenzene	1 U	1 U	1 U	1 U
Toluene	1 U	1 U	1 U	1 U
2-BUTANONE	10 U	10 U	10 U	10 U
4-METHYL-2-PENTANONE	1.4 U	1.4 U	1.4 U	1.4 U
1,1,2,2-Tetrachloroethane	1.5 U	1.5 U	1.5 U	1.5 U
Tetrachloroethene	1 U	1 U	1 U	1 U
Trichloroethene	1 U	1 U	1 U	1 U
XYLENES, TOTAL	2 UJ8	2 U	2 UJ8	2 UJ8

Field Sample Number ->	NRSW1	NRSW2	NRSW3	NRSW4	NRSW5	NRSW6	NRSW8
Lab Analysis Number ->	UC02381	UC02382	UC02383	UC02481	UC02272	UC02482	UC02273
Semivolatile Organics (ug/L)							
1,2,4-Trichlorobenzene	2.4 U	2.4 U	2.4 U	2.4 U	2.4 UJ7	2.4 U	2.4 UJ7
1,2-Dichlorobenzene	1.2 U	1.2 U	1.2 U	1.2 U	1.2 UJ7	1.2 U	1.2 UJ7
1,3-Dichlorobenzene	3.4 U	3.4 U	3.4 U	3.4 U	3.4 UJ7	3.4 U	3.4 UJ7
1,4-Dichlorobenzene	1.5 U	1.5 U	1.5 U	1.5 U	1.5 UJ7	1.5 U	1.5 UJ7
2,4,5-Trichlorophenol	2.8 U	2.8 U	2.8 U	2.8 U	2.8 UJ7	2.8 U	2.8 UJ7
2,4,6-Trichlorophenol	3.6 U	3.6 U	3.6 U	3.6 U	3.6 UJ7	3.6 U	3.6 UJ7
2,4-Dichlorophenol	8.4 U	8.4 U	8.4 U	8.4 U	8.4 UJ7	8.4 U	8.4 UJ7
2,4-Dimethylphenol	4.4 U	4.4 U	4.4 U	4.4 U	4.4 UJ7	4.4 U	4.4 UJ7
2,4-Dinitrophenol	180 U	180 U	180 U	180 U	180 UJ7	180 U	180 UJ7
2,4-Dinitrotoluene	5.8 U	5.8 U	5.8 U	5.8 U	5.8 UJ7	5.8 U	5.8 UJ7
2,6-Dinitrotoluene	6.7 U	6.7 U	6.7 U	6.7 U	6.7 UJ7	6.7 U	6.7 UJ7
2-Chlorophenol	2.8 U	2.8 U	2.8 U	2.8 U	2.8 UJ7	2.8 U	2.8 UJ7
2-Chloronaphthalene	2.6 U	2.6 U	2.6 U	2.6 U	2.6 UJ7	2.6 U	2.6 UJ7
2-Methylphenol	3.6 U	3.6 U	3.6 U	3.6 U	3.6 UJ7	3.6 U	3.6 UJ7
3,3'-Dichlorobenzidine	5 U	5 U	5 U	5 U	5 UJ7	5 U	5 UJ7
4,6-Dinitro-2-cresol	50 U	50 UJ8	50 UJ8	50 U	50 UJ6	50 UJ8	50 UJ6
4-BROMOPHENYLPHENYL ETHER	22 U	22 U	22 U	22 U	22 UJ7	22 U	22 UJ7
3-METHYL-4-CHLOROPHENOL	8.5 U	8.5 U	8.5 U	8.5 U	8.5 UJ7	8.5 U	8.5 UJ7
4-Methylphenol	2.8 U	2.8 U	2.8 U	2.8 U	2.8 UJ7	2.8 U	2.8 UJ7
4-Nitrophenol	96 U	96 U	96 U	96 U	96 UJ7	96 U	96 UJ7
Anthracene	5.2 U	5.2 U	5.2 U	5.2 U	5.2 UJ7	5.2 U	5.2 UJ7
Bis(2-chloroethoxy) methane	6.8 U	6.8 U	6.8 U	6.8 U	6.8 UJ7	6.8 U	6.8 UJ7
Bis(2-chloroisopropyl) ether	5 U	5 U	5 U	5 U	5 UJ7	5 U	5 UJ7
Bis(2-chloroethyl) ether	0.68 U	0.68 U	0.68 U	0.68 U	0.68 UJ7	0.68 U	0.68 UJ7
Bis(2-ethylhexyl) phthalate	7.7 U	7.7 U	7.7 U	7.7 U	7.7 UJ7	7.7 U	7.7 UJ7
Benzo[a]anthracene	9.8 U	9.8 U	9.8 U	9.8 U	9.8 UJ7	9.8 U	9.8 UJ7
Benzo[a]pyrene	14 U	14 U	14 U	14 U	14 UJ7	14 U	14 UJ7
Benzo[b]fluoranthene	10 U	10 U	10 U	10 U	10 UJ7	10 U	10 UJ7
Butylbenzyl phthalate	28 U	28 U	28 U	28 U	28 UJ7	28 U	28 UJ7
Benzo[k]fluoranthene	10 U	10 U	10 U	10 U	10 UJ7	10 U	10 UJ7
Chrysene	7.4 U	7.4 U	7.4 U	7.4 U	7.4 UJ7	7.4 U	7.4 UJ7
Hexachlorobenzene	12 U	12 U	12 U	12 U	12 UJ7	12 U	12 UJ7
Hexachlorocyclopentadiene	54 U	54 U	54 U	54 U	54 UJ7	54 U	54 UJ7
Hexachloroethane	8.3 U	8.3 U	8.3 U	8.3 U	8.3 UJ7	8.3 U	8.3 UJ7
Dibenz[ah]anthracene	12 U	12 U	12 U	12 U	12 UJ7	12 U	12 UJ7
Diethyl phthalate	5.9 U	5.9 U	5.9 U	5.9 U	5.9 UJ7	5.9 U	5.9 UJ7
Dimethyl phthalate	2.2 U	2.2 U	2.2 U	2.2 U	2.2 UJ7	2.2 U	2.2 UJ7
Di-n-butyl phthalate	33 U	33 U	33 U	33 U	33 UJ7	33 U	33 UJ7
Di-n-octyl phthalate	1.5 U	1.5 U	1.5 U	1.5 U	1.5 UJ7	1.5 U	1.5 UJ7
Fluoranthene	24 U	24 U	24 U	24 U	24 UJ7	24 U	24 UJ7

Field Sample Number ->	NRSW1	NRSW2	NRSW3	NRSW4	NRSW5	NRSW6	NRSW8
Lab Analysis Number ->	UC02381	UC02382	UC02383	UC02481	UC02272	UC02482	UC02273
Semivolatile Organics (ug/L)							
Hexachlorobutadiene	8.7 U	8.7 U	8.7 U	8.7 U	8.7 UJ7	8.7 U	8.7 UJ7
Indeno[1,2,3-C,D]pyrene	21 U	21 U	21 U	21 U	21 UJ7	21 U	21 UJ7
Naphthalene	0.5 U	0.5 U	0.5 U	0.5 U	0.5 UJ7	0.5 U	0.5 UJ7
Nitrobenzene	3.7 U	3.7 U	3.7 U	3.7 U	3.7 UJ7	3.7 U	3.7 UJ7
N-Nitrosodi-n-propylamine	6.8 U	6.8 U	6.8 U	6.8 U	6.8 UJ7	6.8 U	6.8 UJ7
N-Nitrosodiphenylamine	3.7 U	3.7 U	3.7 U	3.7 U	3.7 UJ7	3.7 U	3.7 UJ7
Pentachlorophenol	9.1 U	9.1 U	9.1 U	9.1 U	9.1 UJ7	9.1 U	9.1 UJ7
Phenanthrene	9.9 U	9.9 U	9.9 U	9.9 U	9.9 UJ7	9.9 U	9.9 UJ7
Phenol	2.2 U	2.2 U	2.2 U	2.2 U	2.2 UJ7	2.2 U	2.2 UJ7
Pyrene	17 U	17 U	17 U	17 U	17 UJ7	17 U	17 UJ7

Field Sample Number ->	NRSEEQ		NRSWFB	
Lab Analysis Number ->	UC02264		UC02265	
Semivolatile Organics (ug/L)				
1,2,4-Trichlorobenzene	2.4	UJ7	2.4	UJ7
1,2-Dichlorobenzene	1.2	UJ7	1.2	UJ7
1,3-Dichlorobenzene	3.4	UJ7	3.4	UJ7
1,4-Dichlorobenzene	1.5	UJ7	1.5	UJ7
2,4,5-Trichlorophenol	2.8	UJ7	2.8	UJ7
2,4,6-Trichlorophenol	3.6	UJ7	3.6	UJ7
2,4-Dichlorophenol	8.4	UJ7	8.4	UJ7
2,4-Dimethylphenol	4.4	UJ7	4.4	UJ7
2,4-Dinitrophenol	180	UJ7	180	UJ7
2,4-Dinitrotoluene	5.8	UJ7	5.8	UJ7
2,6-Dinitrotoluene	6.7	UJ7	6.7	UJ7
2-Chlorophenol	2.8	UJ7	2.8	UJ7
2-Chloronaphthalene	2.6	UJ7	2.6	UJ7
2-Methylphenol	3.6	UJ7	3.6	UJ7
3,3'-Dichlorobenzidine	5	UJ7	5	UJ7
4,6-Dinitro-2-cresol	50	UJ6	50	UJ6
4-BROMOPHENYLPHENYL ETHER	22	UJ7	22	UJ7
3-METHYL-4-CHLOROPHENOL	8.5	UJ7	8.5	UJ7
4-Methylphenol	2.8	UJ7	2.8	UJ7
4-Nitrophenol	96	UJ7	96	UJ7
Anthracene	5.2	UJ7	5.2	UJ7
Bis(2-chloroethoxy) methane	6.8	UJ7	6.8	UJ7
Bis(2-chloroisopropyl) ether	5	UJ7	5	UJ7
Bis(2-chloroethyl) ether	0.68	UJ7	0.68	UJ7
Bis(2-ethylhexyl) phthalate	7.7	UJ7	7.7	UJ7
Benzo[a]anthracene	9.8	UJ7	9.8	UJ7
Benzo[a]pyrene	14	UJ7	14	UJ7
Benzo[b]fluoranthene	10	UJ7	10	UJ7
Butylbenzyl phthalate	28	UJ7	28	UJ7
Benzo[k]fluoranthene	10	UJ7	10	UJ7
Chrysene	7.4	UJ7	7.4	UJ7
Hexachlorobenzene	12	UJ7	12	UJ7
Hexachlorocyclopentadiene	54	UJ7	54	UJ7
Hexachloroethane	8.3	UJ7	8.3	UJ7
Dibenz[ah]anthracene	12	UJ7	12	UJ7
Diethyl phthalate	5.9	UJ7	5.9	UJ7
Dimethyl phthalate	2.2	UJ7	2.2	UJ7
Di-n-butyl phthalate	33	UJ7	33	UJ7
Di-n-octyl phthalate	1.5	UJ7	1.5	UJ7
Fluoranthene	24	UJ7	24	UJ7

Field Sample Number ->	NRSEEQ		NRSWFB	
Lab Analysis Number ->	UC02264		UC02265	
Semivolatile Organics (ug/L)				
Hexachlorobutadiene	8.7	UJ7	8.7	UJ7
Indeno[1,2,3-C,D]pyrene	21	UJ7	21	UJ7
Naphthalene	0.5	UJ7	0.5	UJ7
Nitrobenzene	3.7	UJ7	3.7	UJ7
N-Nitrosodi-n-propylamine	6.8	UJ7	6.8	UJ7
N-Nitrosodiphenylamine	3.7	UJ7	3.7	UJ7
Pentachlorophenol	9.1	UJ7	9.1	UJ7
Phenanthrene	9.9	UJ7	9.9	UJ7
Phenol	2.2	UJ7	2.2	UJ7
Pyrene	17	UJ7	17	UJ7

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Field Sample Number ->	NRSW1		NRSW2		NRSW3		NRSW4		NRSW5		NRSW6		54MW1	
Lab Analysis Number ->	UC02381		UC02382		UC02383		UC02481		UC02272		UC02482		UC02223	
Explosives (ug/L)														
2,4,6-Trinitrotoluene	0.426 U		0.426 U		0.426 U		0.426 U		0.426 U		0.426 U		0.426 U	
2,4-Dinitrotoluene	0.397 U		0.397 U		0.397 U		0.397 U		0.397 U		0.397 U		0.397 U	
2,6-Dinitrotoluene	0.6 U		0.6 U		0.6 U		0.6 U		0.6 U		0.6 U		0.6 U	
Cyclotetramethylenetetranitramine	0.533 U		0.533 U		0.533 U		0.533 U		0.533 U		0.533 U		0.533 U	
Cyclonite (RDX)	0.416 U		0.416 U		0.416 U		0.416 U		0.416 U		0.416 U		0.416 U	
TETRYL	0.631 U		0.631 U		0.631 U		0.631 U		0.631 U		0.631 U		0.631 U	

Field Sample Number ->	54MW2		54MW3		NRSW8		NRSEEQ		NRSWFB		54MWEQ	
Lab Analysis Number ->	UC02271		UC02270		UC02273		UC02264		UC02265		UC02266	
Explosives (ug/L)												
2,4,6-Trinitrotoluene	17.5 U		0.426 U		0.426 U		0.426 U		0.426 U		0.426 U	
2,4-Dinitrotoluene	0.397 U		0.397 U		0.397 U		0.397 U		0.397 U		0.397 U	
2,6-Dinitrotoluene	0.6 U		0.6 U		0.6 U		0.6 U		0.6 U		0.6 U	
Cyclotetramethylenetetranitramine	4.63		3.18 J10		0.533 U		0.533 U		0.533 U		0.533 U	
Cyclonite (RDX)	0.416 UJ8		0.416 U		0.416 U		0.416 U		0.416 U		0.416 U	
TETRYL	0.631 U		0.631 U		0.631 U		0.631 U		0.631 U		0.631 U	

Field Sample Number ->	NRSW1		NRSW2		NRSW3		NRSW4		NRSW5		NRSW6		54MW1		54MW2	
Lab Analysis Number ->	UC02381		UC02382		UC02383		UC02481		UC02272		UC02482		UC02223		UC02271	
Total Metals (ug/L)																
Arsenic	2.35 U		2.35 U		2.35 U		2.35 U		2.35 U		2.35 U		20.7		2.35 U	
Mercury	0.1 U		0.1 U		0.1 U		0.1 U		0.1 U		0.1 U		0.1 U		0.1 U	
Lead	4.47 U		4.47 U		4.47 U		8.79		4.47 U		4.47 U		16.6		9.31	
Selenium	2.53 U		2.53 U		2.53 U		2.53 U		2.53 U		2.53 U		2.53 U		2.53 U	
Silver	0.333 U		0.333 U		0.333 U		0.333 U		0.333 U		0.333 U		0.333 U		0.333 U	
Barium	24.9		25.1		24.9		26.3		21.1		24.8		1060		144	
Beryllium	1.12 U		1.12 U		1.12 U		1.12 U		1.12 U		1.12 U		20		3.19	
Cadmium	6.78 U		6.78 U		6.78 U		6.78 U		6.78 U		6.78 U		6.78 U		6.78 U	
Chromium	16.8 U		16.8 U		16.8 U		16.8 U		16.8 U		16.8 U		66.7		16.8 U	
Nickel	32.1 U		32.1 U		32.1 U		32.1 U		32.1 U		32.1 U		37.4		32.1 U	
Antimony	60 U		60 U		60 U		60 U		60 U		60 U		110		60 U	
Thallium	125 U		125 U		125 U		125 U		125 U		125 U		125 U		125 U	

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Field Sample Number ->	54MW3		NRSW8		17PZ1		17MW2		17MW3		40MW3		31MW1		31MW2	
Lab Analysis Number ->	UC02270		UC02273		UC02304		UC02303		UC02387		UC02384		UC02221		UC02215	
Total Metals (ug/L)																
Arsenic	2.35 U		2.35 U		2.35 U		2.35 U		2.35 U		2.35 U		2.35 U		7.44	
Mercury	0.1 U		0.1 U		0.1 U		0.1 U		0.1 U		0.1 U		0.1 U		0.1 U	
Lead	4.47 U		4.47 U		4.47 U		4.47 U		6.3		4.47 U		7.58		41.8	
Selenium	2.53 U		2.53 U		2.53 U		3.63		2.53 U		2.53 U		2.53 U		2.53 U	
Silver	0.333 U		0.333 U		0.333 U		0.333 U		0.333 U		0.333 U		0.333 U		0.333 U	
Barium	175		21.1		106		63.6		174		54.5		300		183	
Beryllium	4.09		1.12 U		4.55		4.03		1.12 U		1.12 U		5.16		6	
Cadmium	6.78 U		6.78 U		6.78 U		6.78 U		6.78 U		6.78 U		6.78 U		6.78 U	
Chromium	16.8 U		16.8 U		16.8 U		16.8 U		16.8 U		16.8 U		16.8 U		97.3	
Nickel	32.1 U		32.1 U		32.1 U		32.1 U		32.1 U		32.1 U		32.1 U		49.9	
Antimony	60 U		60 U		60 U		60 U		60 U		60 U		60 U		60 U	
Thallium	125 U		125 U		125 U		125 U		125 U		125 U		125 U		125 U	

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Field Sample Number ->	31MW3		31MW4		48MW1		48MW2		48MW3		48MW4		NRSEEQ		NRSWFB	
Lab Analysis Number ->	UC02217		UC02219		UC02306		UC02305		UC02385		UC02480		UC02264		UC02265	
Total Metals (ug/L)																
Arsenic	2.35 U		2.35 U		2.35 U		2.35 U		2.35 U		2.35 U		2.35 U		2.35 U	
Mercury	0.138		0.142		0.1 U		0.1 U		0.1 U		0.1 U		0.1 U		0.1 U	
Lead	36.2		11.3		4.47 U		9.29		4.47 U		12.4		4.47 U		4.47 U	
Selenium	2.53 U		2.53 U		2.72		2.53 U		2.53 U		2.53 U		2.53 U		2.53 U	
Silver	0.333 U		0.333 U		0.333 U		0.333 U		0.333 U		0.333 U		0.333 U		0.333 U	
Barium	257		137		81		1070		70.7		299		2.82 U		2.82 U	
Beryllium	5.24		5.26		4.16		10.7		1.12 U		1.12 U		1.12 U		1.12 U	
Cadmium	6.78 U		6.78 U		6.78 U		6.78 U		6.78 U		6.78 U		6.78 U		6.78 U	
Chromium	89.1		31.6		16.8 U		42.8		16.8 U		16.8 U		16.8 U		16.8 U	
Nickel	58.4		32.1 U		32.1 U		32.1 U		32.1 U		32.1 U		32.1 U		32.1 U	
Antimony	60 U		60 U		60 U		60 U		60 U		60 U		60 U		60 U	
Thallium	125 U		125 U		125 U		125 U		125 U		125 U		125 U		125 U	

Field Sample Number ->	54MWEQ		FBLK1		EQBLK	
Lab Analysis Number ->	UC02266		UC02353		UC02354	
Total Metals (ug/L)						
Arsenic	2.35 U		2.35 U		2.35 U	
Mercury	0.1 U		0.1 U		0.1 U	
Lead	4.47 U		4.47 U		4.47 U	
Selenium	2.53 U		2.53 U		2.53 U	
Silver	0.333 U		0.333 U		0.333 U	
Barium	2.82 U		2.82 U		2.82 U	
Beryllium	1.12 U		1.12 U		1.12 U	
Cadmium	6.78 U		6.78 U		6.78 U	
Chromium	16.8 U		16.8 U		16.8 U	
Nickel	32.1 U		32.1 U		32.1 U	
Antimony	60 U		60 U		60 U	
Thallium	125 U		125 U		125 U	

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Field Sample Number ->	54MW1F	54MW2F	54MW3F	17P21F	17MW2F	17MW3F	40MW3F
Lab Analysis Number ->	UC02224	UC02275	UC02274	UC02320	UC02319	UC02390	UC02388
Dissolved Metals (ug/L)							
Arsenic	15.1	2.35 U	2.35 U	2.35 U	2.35 U	2.35 U	2.35 U
Mercury	0.1 U	0.1 U	0.1 U	0.1 U	0.1 U	0.1 U	0.1 U
Lead	6.33	4.47 U	4.47 U	4.47 U	4.47 U	4.47 U	4.47 U
Selenium	2.53 U	2.53 U	2.53 U	2.53 U	2.53 U	2.53 U	2.53 U
Silver	0.333 U	0.333 U	0.333 U	0.333 U	0.333 U	0.333 U	0.333 U
Barium	519	89.5	106	110	63.2	164	31
Beryllium	13.2	2.96	2.82	4.28	4.26	1.12 U	1.12 U
Cadmium	6.78 U	6.78 U	6.78 U	6.78 U	6.78 U	6.78 U	6.78 U
Chromium	26.6	16.8 U	16.8 U	16.8 U	16.8 U	16.8 U	16.8 U
Nickel	32.1 U	32.1 U	32.1 U	32.1 U	32.1 U	32.1 U	32.1 U
Antimony	97.5	60 U	60 U	60 U	60 U	60 U	60 U
Thallium	125 U	125 U	125 U	125 U	125 U	125 U	125 U

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Field Sample Number ->	31MW1F		31MW2F		31MW3F		31MW4F		48MW1F		48MW2F		48MW3F	
Lab Analysis Number ->	UC02222		UC02216		UC02218		UC02220		UC02322		UC02321		UC02389	
Dissolved Metals (ug/L)														
Arsenic	2.35	U	2.35	U	2.35	U	2.35	U	2.35	U	2.35	U	2.35	U
Mercury	0.1	U	0.1	U	0.1	U	0.1	U	0.1	U	0.1	U	0.1	U
Lead	4.47	U	4.47	U	4.47	U	4.47	U	4.47	U	4.47	U	4.47	U
Selenium	2.53	U	5.4		2.53	U	2.53	U	2.53	U	2.53	U	2.53	U
Silver	0.333	U	0.333	U	0.333	U	0.333	U	0.333	U	0.333	U	0.333	U
Barium	264		27		24.7		19.7		69.7		816		69.8	
Beryllium	3.98		1.63		1.86		1.12	U	4.05		2.69		1.12	U
Cadmium	6.78	U	6.78	U	6.78	U	6.78	U	6.78	U	6.78	U	6.78	U
Chromium	16.8	U	16.8	U	16.8	U	16.8	U	16.8	U	16.8	U	16.8	U
Nickel	32.1	U	32.1	U	32.1	U	32.1	U	32.1	U	32.1	U	32.1	U
Antimony	60	U	60	U	60	U	60	U	60	U	60	U	60	U
Thallium	125	U	125	U	125	U	125	U	125	U	125	U	125	U

Field Sample Number ->	48MW4F	54MWEQF
Lab Analysis Number ->	UC02484	UC02268
Dissolved Metals (ug/L)		
Arsenic	2.35 U	2.35 U
Mercury	0.1 U	0.1 U
Lead	4.47 U	4.47 U
Selenium	2.53 U	2.53 U
Silver	0.333 U	0.333 U
Barium	295	2.82 U
Beryllium	1.12 U	1.12 U
Cadmium	6.78 U	6.78 U
Chromium	16.8 U	16.8 U
Nickel	32.1 U	32.1 U
Antimony	60 U	60 U
Thallium	125 U	125 U

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Field Sample Number ->	NRSW1		NRSW2		NRSW3		NRSW4		NRSW5		NRSW6		54MW1	
Lab Analysis Number ->	UC02381		UC02382		UC02383		UC02481		UC02272		UC02482		UC02223	
*TOTAL ORGANIC CARBON (ug/L)	2180		2320		2080		1960		1810		2310		1170	
Chloride (ug/L)	3740		3600		3660		3800		3870		3960			

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Field Sample Number ->	54MW2		54MW3		NRSW8		NRSEEQ		NRSWFB		54MWEQ	
Lab Analysis Number ->	UC02271		UC02270		UC02273		UC02264		UC02265		UC02266	
*TOTAL ORGANIC CARBON (ug/L)	1000	UJ7	1000	UJ7	1870	J7	1000	U	1000	U	1000	U
Chloride (ug/L)					3840	J7			278	U		

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Field Sample Number ->	NRSW1		NRSW2		NRSW3		NRSW4		NRSW5		NRSW6		54MW1	
Lab Analysis Number ->	UC02381		UC02382		UC02383		UC02462		UC02272		UC02482		UC02223	
*TOTAL ORGANIC HALOGENS (ug/L)	10 U		10 U		10 U		10 U		10 U		10 U		10.8	

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Field Sample Number ->	54MW2		54MW3		NRSW8		NRSEEQ		NRSWFB		54MWEQ	
Lab Analysis Number ->	UC02271		UC02270		UC02273		UC02264		UC02265		UC02266	
*TOTAL ORGANIC HALOGENS (ug/L)	13	J7	10	UJ7	10	UJ7	10	U	10	U	10	U

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Field Sample Number ->	NRSW1		NRSW2		NRSW3		NRSW4		NRSW5		NRSW6		NRSW8		NRSWF8	
Lab Analysis Number ->	UC02381		UC02382		UC02383		UC02481		UC02272		UC02482		UC02273		UC02265	
*TOTAL HARDNESS (ug/L)	42700		42800		43200		44600		47800		51300		47700		818	U

Field Sample Number ->	NRSE1		NRSE1		NRSE2		NRSE3		NRSE4		NRSE4		NRSE5		NRSE6		NRSE8	
Lab Analysis Number ->	UC02261		UC02391		UC02392		UC02393		UC02269		UC02485		UC02276		UC02486		UC02277	
Volatile Organics (ug/g)																		
1,1,1-Trichloroethane	0.42 U		0.37 U		0.32 U		0.33 U		0.22 U		0.26 U		0.28 U		0.31 U		0.27 U	
1,1,2-Trichloroethane	0.69 U		0.61 U		0.52 U		0.55 U		0.37 U		0.43 U		0.45 U		0.50 U		0.45 U	
1,1-Dichloroethene	0.56 U		0.50 U		0.43 U		0.45 U		0.30 U		0.35 U		0.37 U		0.41 U		0.37 U	
1,1-Dichloroethane	1.03 U		0.91 U		0.78 U		0.82 U		0.55 U		0.64 U		0.67 U		0.75 U		0.67 U	
*1,2-DICHLOROETHYLENES (Total)	0.67 U		0.59 U		0.51 U		0.53 U		0.36 U		0.42 U		0.44 U		0.49 U		0.44 U	
1,2-Dichloroethane	0.67 U		0.59 U		0.51 U		0.53 U		0.36 U		0.42 U		0.44 U		0.49 U		0.44 U	
1,2-Dichloropropane	1.11 U		0.98 U		0.84 U		0.88 U		0.59 U		0.69 U		0.73 U		0.81 U		0.72 U	
Acetone	6.90 U		6.12 U		5.23 U		5.50 U		3.69 U		4.29 U		4.54 U		5.04 U		4.51 U	
Acrylonitrile	4.18 U		3.71 U		3.17 U		3.33 U		2.23 U		2.60 U		2.75 U		3.05 U		2.73 U	
Bromodichloromethane	0.42 U		0.37 U		0.32 U		0.33 U		0.22 U		0.26 U		0.28 U		0.31 U		0.27 U	
Vinyl chloride	3.77 U		3.34 U		2.85 U		3.00 U		2.01 U		2.34 U		2.48 U		2.75 U		2.46 U	
Chloroethane	1.34 U		1.19 U		1.01 U		1.07 U		0.72 U		0.83 U		0.88 U		0.98 U		0.87 U	
Benzene	0.21 U		0.19 U		0.16 U		0.17 U		0.11 U		0.13 U		0.14 U		0.15 U		0.14 U	
Trichlorofluoromethane	0.48 U		0.43 U		0.36 U		0.38 U		0.26 U		0.30 U		0.32 U		0.35 U		0.31 U	
Carbon tetrachloride	0.65 U		0.58 U		0.49 U		0.52 U		0.35 U		0.40 U		0.43 U		0.47 U		0.42 U	
Methylene chloride	9.21 U		8.16 U		6.97 U		7.33 U		4.92 U		5.71 U		6.05 U		6.72 U		6.01 U	
Bromomethane	0.54 U		0.48 U		0.41 U		0.43 U		0.29 U		0.34 U		0.36 U		0.40 U		0.36 U	
Chloromethane	2.01 U		1.78 U		1.52 U		1.60 U		1.07 U		1.25 U		1.32 U		1.47 U		1.31 U	
Bromoform	0.42 U		0.37 U		0.32 U		0.33 U		0.22 U		0.25 U		0.28 U		0.31 U		0.27 U	
Chloroform	0.50 U		0.45 U		0.38 U		0.40 U		0.27 U		0.31 U		0.33 U		0.37 U		0.33 U	
Chlorobenzene	0.21 U		0.19 U		0.16 U		0.17 U		0.11 U		0.13 U		0.14 U		0.15 U		0.14 U	
Ethylbenzene	0.40 U		0.35 U		0.30 U		0.32 U		0.21 U		0.25 U		0.26 U		0.29 U		0.26 U	
Toluene	0.21 U		0.19 U		0.16 U		0.17 U		0.11 U		0.13 U		0.14 U		0.15 U		0.14 U	
2-BUTANONE	9.00 U		7.98 U		6.81 U		7.17 U		4.80 U		5.58 U		5.91 U		6.56 U		5.87 U	
4-METHYL-2-PENTANONE	1.32 U		1.17 U		1.00 U		1.05 U		0.70 U		0.82 U		0.87 U		0.96 U		0.86 U	
1,1,2,2-Tetrachloroethane	0.42 U		0.37 U		0.32 U		0.33 U		0.22 U		0.26 U		0.28 U		0.31 U		0.27 U	
Tetrachloroethylene	0.33 U		0.30 U		0.25 U		0.27 U		0.18 U		0.21 U		0.22 U		0.24 U		0.22 U	
Trichloroethylene	0.48 U		0.43 U		0.36 U		0.38 U		0.26 U		0.30 U		0.32 U		0.35 U		0.31 U	
XYLENES, TOTAL	1.63 UJ8		1.45 UJ8		1.24 UJ8		1.30 UJ8		0.87 UJ8		1.01 UJ8		1.07 UJ8		1.19 U		1.07 UJ8	

Field Sample Number ->	NRSE1	NRSE2	NRSE3	NRSE4	NRSE5	NRSE6	NRSE8
Lab Analysis Number ->	UC02391	UC02392	UC02393	UC02485	UC02276	UC02486	UC02277
Semivolatile Organics (ug/g)							
1,2,4-Trichlorobenzene	0.41 U	0.35 U	0.37 U	0.29 U	0.30 UJ7	0.34 U	0.30 UJ7
1,2-Dichlorobenzene	0.08 U	0.07 U	0.07 U	0.05 U	0.06 UJ7	0.06 U	0.06 UJ7
1,3-Dichlorobenzene	0.08 U	0.07 U	0.07 U	0.05 U	0.06 UJ7	0.06 U	0.06 UJ7
1,4-Dichlorobenzene	0.06 U	0.05 U	0.06 U	0.04 U	0.05 UJ7	0.05 U	0.05 UJ7
2,4,5-Trichlorophenol	0.91 U	0.78 U	0.82 U	0.64 U	0.67 UJ7	0.75 U	0.67 UJ7
2,4,6-Trichlorophenol	0.11 U	0.10 U	0.10 U	0.08 U	0.08 UJ7	0.09 U	0.08 UJ7
2,4-Dichlorophenol	0.12 U	0.10 U	0.11 U	0.08 U	0.09 UJ7	0.10 U	0.09 UJ7
2,4-Dimethylphenol	5.57 U	4.75 U	5.00 U	3.90 U	4.13 UJ7	4.58 U	4.10 UJ7
2,4-Dinitrophenol	8.72 U	7.45 U	7.83 U	6.10 U	6.46 UJ7	7.18 U	6.42 UJ7
2,4-Dinitrotoluene	2.60 U	2.22 U	2.33 U	1.82 U	1.93 UJ7	2.14 U	1.91 UJ7
2,6-Dinitrotoluene	0.59 U	0.51 U	0.53 U	0.42 U	0.44 UJ7	0.49 U	0.44 UJ7
2-Chlorophenol	0.10 U	0.09 U	0.09 U	0.07 U	0.08 UJ7	0.08 U	0.08 UJ7
2-Chloronaphthalene	0.45 U	0.38 U	0.40 U	0.31 U	0.33 UJ7	0.37 U	0.33 UJ7
2-Methylphenol	0.18 U	0.16 U	0.16 U	0.13 U	0.13 UJ7	0.15 U	0.13 UJ7
3,3'-Dichlorobenzidine	2.97 U	2.54 U	2.67 U	2.08 U	2.20 UJ7	2.44 U	2.19 UJ7
4,6-Dinitro-2-cresol	1.48 U	1.27 U	1.33 U	1.04 U	1.10 UJ7	1.22 U	1.09 UJ7
4-BROMOPHENYLPHENYL ETHER	0.08 U	0.06 U	0.07 U	0.05 U	0.06 UJ7	0.06 U	0.06 UJ7
3-METHYL-4-CHLOROPHENOL	1.73 U	1.47 U	1.55 U	1.21 U	1.28 UJ7	1.42 U	1.27 UJ7
4-Methylphenol	0.45 U	0.38 U	0.40 U	0.31 U	0.33 UJ7	0.37 U	0.33 UJ7
4-Nitrophenol	6.12 U	5.23 U	5.50 U	4.29 U	4.54 UJ7	5.04 U	4.51 UJ7
Anthracene	1.32 U	1.13 U	1.16 U	0.92 U	0.98 UJ7	1.08 U	0.97 UJ7
Bis(2-chloroethoxy) methane	0.35 U	0.30 U	0.32 U	0.25 U	0.26 UJ7	0.29 U	0.26 UJ7
Bis(2-chloroisopropyl) ether	0.82 U	0.70 U	0.73 U	0.57 U	0.61 UJ7	0.67 U	0.60 UJ7
Bis(2-chloroethyl) ether	0.67 U	0.57 U	0.60 U	0.47 U	0.50 UJ7	0.55 U	0.49 UJ7
Bis(2-ethylhexyl) phthalate	0.89 U	0.76 U	0.80 U	6.62	0.66 UJ7	0.73 U	0.66 UJ7
Benzo[a]anthracene	0.58	0.32	0.72	0.05 U	0.17 UJ7	0.40	0.06 UJ7
Benzo[a]pyrene	2.23 U	1.90 U	2.06 U	1.56 U	1.65 UJ7	1.83 U	1.64 UJ7
Benzo[b]fluoranthene	0.58 U	0.49 U	0.52 U	0.40 U	0.43 UJ7	0.47 U	0.42 UJ7
Butylbenzyl phthalate	3.34 U	2.85 U	3.00 U	2.34 U	2.48 UJ7	2.75 U	2.46 UJ7
Benzo[k]fluoranthene	0.24 U	0.21 U	0.22 U	0.17 U	0.18 UJ7	0.20 U	0.18 UJ7
Chrysene	1.67	0.35	0.68	0.04 U	0.19 UJ7	0.53	0.14 UJ7
Hexachlorobenzene	0.15 U	0.13 U	0.13 U	0.10 U	0.11 UJ7	0.12 U	0.11 UJ7
Hexachlorocyclopentadiene	0.96 U	0.82 U	0.87 U	0.68 U	0.72 UJ7	0.79 U	0.71 UJ7
Hexachloroethane	3.34 U	2.85 U	3.00 U	2.34 U	2.48 UJ7	2.75 U	2.46 UJ7
Dibenz[ah]anthracene	0.58 U	0.49 U	0.52 U	0.40 U	0.43 UJ7	0.47 U	0.42 UJ7
Diethyl phthalate	0.45 U	0.38 U	0.40 U	6.23	0.33 UJ7	0.37 U	0.33 UJ7
Dimethyl phthalate	0.12 U	0.10 U	0.11 U	8.31	0.09 UJ7	0.10 U	0.09 UJ7
Di-n-butyl phthalate	2.41 U	2.06 U	2.17 U	12.99	1.79 UJ7	1.98 U	1.78 UJ7
Di-n-octyl phthalate	0.43 U	0.36 U	0.38 U	0.30 U	0.32 UJ7	0.35 U	0.31 UJ7
Fluoranthene	0.54 U	0.30	0.80	0.08	0.22 UJ7	0.50	0.13 UJ7
Hexachlorobutadiene	1.80 U	1.54 U	1.62 U	1.26 U	1.33 UJ7	1.48 U	1.33 UJ7
Indeno[1,2,3-C,D]pyrene	4.45 U	3.80 U	4.00 U	3.12 U	3.30 UJ7	3.66 U	3.28 UJ7

Field Sample Number ->	NRSE1	NRSE2	NRSE3	NRSE4	NRSE5	NRSE6	NRSE8
Lab Analysis Number ->	UC02391	UC02392	UC02393	UC02485	UC02276	UC02486	UC02277
Semivolatile Organics (ug/g)							
Naphthalene	1.37 U	1.17 U	1.23 U	0.96 U	1.02 UJ7	1.13 U	1.01 UJ7
Nitrobenzene	3.34 U	2.85 U	3.00 U	2.34 U	2.48 UJ7	2.75 U	2.46 UJ7
N-Nitrosodi-n-propylamine	2.04 U	1.74 U	1.83 U	1.43 U	1.51 UJ7	1.68 U	1.50 UJ7
N-Nitrosodiphenylamine	0.54 U	0.46 U	0.48 U	2.60	0.40 UJ7	0.44 U	0.40 UJ7
Pentachlorophenol	1.41 U	1.20 U	1.27 U	0.99 U	1.05 UJ7	1.16 U	1.04 UJ7
Phenanthrene	0.76	0.51	0.82	0.04 U	0.22 UJ7	0.35	0.19 UJ7
Phenol	0.10 U	0.08 U	0.09 U	0.07 U	0.07 UJ7	0.08 U	0.07 UJ7
Pyrene	0.80	0.40	1.00	0.11 U	0.29 UJ7	0.76	0.11 UJ7

Field Sample Number ->	NRSE1		NRSE2		NRSE3		NRSE4		NRSE5		NRSE6		NRSE8	
Lab Analysis Number ->	UC02391		UC02392		UC02393		UC02485		UC02276		UC02486		UC02277	
Explosives (ug/g)														
2,4,6-Trinitrotoluene	3.71 U		3.17 U		3.33 U		2.60 U		28.89 J10		3.05 U		2.73 U	
2,4-Dinitrotoluene	4.64 U		3.96 U		4.17 U		3.25 U		3.44 U		3.82 U		3.42 U	
2,6-Dinitrotoluene	3.71 U		3.17 U		3.33 U		2.60 U		2.75 U		3.05 U		2.73 U	
Cyclotetramethylenetetranitramine	3.71 U		3.17 U		3.33 U		2.60 U		2.75 U		3.05 U		2.73 U	
Cyclonite (RDX)	2.37 U		2.03 U		2.13 U		1.66 U		1.76 U		1.95 U		1.75 U	
TETRYL	3.91 U		3.34 U		3.52 U		2.74 U		2.90 U		3.22 U		2.88 U	

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Field Sample Number ->	NRSE1		NRSE2		NRSE3		NRSE4		NRSE5		NRSE6		NRSE8		BG1BUC3	
Lab Analysis Number ->	UC02391		UC02392		UC02393		UC02485		UC02276		UC02486		UC02277		UC02308	
Metals (ug/g)																
Arsenic	4.64 U		3.96 U		4.17 U		3.25 U		6.92		3.82 U		7.83		11.47	
Selenium	0.83 U		0.71 U		1.85		0.58 U		0.62 U		0.69 U		0.61 U		0.56 U	
Lead	148.42 J1		136.29 J1		200.00 J1		4,415.58 J1		220.08 J1		141.99 J1		245.90 J1		21.32 J1	
Silver	0.14		0.09		0.15		0.10		0.10		0.11		0.07		0.08 J9	
Barium	226.35 J1		151.82 J1		415.00 J1		97.14 J1		178.82 J1		109.77 J1		187.16 J1		46.88 J1	
Beryllium	0.79 U		0.68 U		3.03		0.99		1.31		0.65 U		1.31		1.42	
Cadmium	2.23 U		1.90 U		2.00 U		1.56 U		1.65 U		1.83 U		1.64 U		1.50 U	
Chromium	46.20 J1		32.01 J1		77.33 J1		37.53 J1		31.50 J1		24.89 J1		33.88 J1		50.75 J1	
Nickel	25.05		15.72		41.83		13.25		15.82		12.49		14.89		30.17	
Antimony	36.36 U		31.06 U		32.67 U		25.45 U		26.96 U		29.92 U		26.78 U		24.44 U	
Thallium	63.64 U		54.36 U		57.17 U		44.55 U		47.18 U		52.37 U		46.86 U		42.77 U	
Mercury	0.09 U		0.08 U		0.08 U		0.16 U		0.07 U		0.08 U		0.07 U		0.21	

Field Sample Number ->	BG1CUC8		BG2BUC5		BG2CUC11		BG3BUC3		BG3CUC22		BG4BUC5		BG4CUC17		BG5BUC3	
Lab Analysis Number ->	UC02309		UC02310		UC02311		UC02355		UC02356		UC02357		UC02358		UC02312	
Metals (ug/g)																
Arsenic	6.96		11.61		9.69		14.41		2.74 U		4.34		3.11 U		2.64 U	
Selenium	0.54 U		0.53 U		0.57 U		0.54 U		0.49 U		0.55 U		0.56 U		0.47 U	
Lead	15.25 J1		27.90 J1		20.03 J1		228.09 J1		11.82 J1		20.44 J1		18.03 J1		5.20 J1	
Silver	0.08 J9		0.01 U		0.02 U		0.05		0.01 U		0.02 U		0.02 U		0.01 U	
Barium	73.00 J1		31.44 J1		85.20 J1		286.92 J1		107.99 J1		244.53 J1		205.22 J1		36.18 J1	
Beryllium	2.92		0.99		3.33		1.81		0.82		1.46		1.58		0.45 U	
Cadmium	1.45 U		1.42 U		1.53 U		1.44 U		1.31 U		1.46 U		1.49 U		1.27 U	
Chromium	57.26 J1		51.54 J1		47.96 J1		58.10		31.29		55.96		50.12		30.70 J1	
Nickel	36.32		13.36		38.01		22.81		16.19		25.30		28.36		5.15	
Antimony	23.73 U		23.17 U		25.00 U		23.53 U		21.44 U		23.84 U		24.38 U		20.68 U	
Thallium	41.53 U		40.54 U		43.75 U		41.18 U		37.53 U		41.73 U		42.66 U		36.18 U	
Mercury	0.23		0.17		0.19		0.06 U		0.05 U		0.06 U		0.06 U		0.05 U	

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Field Sample Number ->	BG5CUC8		BG6BUC5		BG6CUC12		BG7BUC5		BG7CUC22		BG8BUC5		BG8CUC10		BG1BBL4	
Lab Analysis Number ->	UC02313		UC02314		UC02315		UC02316		UC02317		UC02318		UC02323		UC02324	
Metals (ug/g)																
Arsenic	8.10		8.42		8.92		3.85 U		5.50		3.26 U		3.19 U		3.11 U	
Selenium	0.61 U		0.70 U		0.67 U		0.69 U		0.62 U		0.59 U		0.57 U		0.56 U	
Lead	24.90 J1		33.18 J1		12.46 J1		17.72 J1		13.37 J1		21.93 J1		9.63 J1		13.45 J1	
Silver	0.02 U		0.02 U		0.02 U		0.02 U		0.02 U		0.02 U		0.08 J9		0.02 U	
Barium	82.08 J1		62.95 J1		70.51 J1		99.08 J1		95.46 J1		74.54 J1		62.63 J1		97.88 J1	
Beryllium	1.96		1.31		2.75		2.33		4.10		1.11		0.94		0.53 U	
Cadmium	1.64 U		1.86 U		1.80 U		1.85 U		1.65 U		1.57 U		1.53 U		1.49 U	
Chromium	54.45 J1		40.47 J1		41.47 J1		46.07 J1		52.82 J1		37.86 J1		39.41 J1		38.98 J1	
Nickel	42.68		30.23		37.87		29.89		47.04		18.93		16.45		9.98	
Antimony	26.81 U		30.39 U		29.34 U		30.20 U		26.96 U		25.59 U		25.00 U		24.41 U	
Thallium	46.92 U		53.18 U		51.35 U		52.85 U		47.18 U		44.78 U		43.75 U		42.71 U	
Mercury	0.07 U		0.21		0.07 U		0.08 U		0.07 U		0.07 U		0.06 U		0.06 U	

Field Sample Number ->	BG1CBL10		BG2BBL5		BG2CBL17		BG3BBL3		BG3CBL22		BG4BBL5		BG4CBL10		BG1BWL5	
Lab Analysis Number ->	UC02325		UC02326		UC02327		UC02359		UC02360		UC02361		UC02362		UC02328	
Metals (ug/g)																
Arsenic	3.06 U		3.06 U		12.44		2.99 U		3.14 U		5.62		3.02 U		3.03 U	
Selenium	0.55 U		0.55 U		0.57 U		0.54 U		0.56 U		0.54 U		0.54 U		0.54 U	
Lead	14.32 J1		10.85 J1		43.37 J1		20.93 J1		16.48 J1		23.10 J1		22.13 J1		11.31 J1	
Silver	0.02 U		0.02 U		0.02 U		0.01 U		0.02 U		0.01 U		0.01 U		0.02 U	
Barium	122.28 J1		88.60 J1		131.38 J1		209.33 J1		197.48 J1		74.61 J1		90.21 J1		144.07 J1	
Beryllium	1.49		0.52 U		2.42		1.47		2.13		0.51 U		0.52 U		1.53	
Cadmium	1.47 U		1.47 U		2.47		1.44 U		1.51 U		1.44 U		1.45 U		1.45 U	
Chromium	41.49 J1		44.61 J1		45.41 J1		38.28		52.58		47.77		33.13		43.10 J1	
Nickel	18.12		11.34		36.22		14.83		36.23		14.20		15.11		21.07	
Antimony	23.99 U		24.02 U		25.00 U		23.45 U		24.65 U		23.59 U		23.70 U		23.73 U	
Thallium	41.98 U		42.03 U		43.75 U		41.03 U		43.14 U		41.28 U		41.48 U		41.53 U	
Mercury	0.06 U		0.09		0.11		0.06 U		0.06 U		0.06 U		0.11		0.06 U	

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Field Sample Number ->	BG1CWL8		BG2BWL4		BG2CWL12		BG3BWL3		BG3CWL22		BG4BWL4		BG4CWL17		BG5BWL3	
Lab Analysis Number ->	UC02329		UC02330		UC02331		UC02332		UC02333		UC02363		UC02364		UC02365	
Metals (ug/g)																
Arsenic	4.82		3.00 U		3.06 U		2.91 U		3.01 U		3.73		2.72 U		2.99 U	
Selenium	0.54 U		0.54 U		0.55 U		0.52 U		0.54 U		0.54 U		0.49 U		0.54 U	
Lead	16.81 J1		12.14 J1		15.18 J1		23.19 J1		10.83 J1		24.94 J1		13.82 J1		19.76 J1	
Silver	0.01 U		0.01 U		0.02 U		0.55		0.01 U		0.01 U		0.01 U		0.01 U	
Barium	102.06 J1		110.70 J1		80.78 J1		79.72 J1		100.24 J1		195.44 J1		79.22 J1		186.83 J1	
Beryllium	0.91		1.00		0.84		0.69		0.89		1.49		0.80		1.56	
Cadmium	1.45 U		1.44 U		1.47 U		1.40 U		1.44 U		1.44 U		1.31 U		1.44 U	
Chromium	37.97 J1		34.01 J1		39.17 J1		32.63 J1		33.94 J1		49.16		28.29		54.85	
Nickel	13.78		13.46		9.57		10.56		15.28		26.74		14.25		26.59	
Antimony	23.70 U		23.56 U		23.99 U		22.84 U		23.59 U		23.50 U		21.33 U		23.47 U	
Thallium	41.48 U		41.23 U		41.98 U		39.98 U		41.28 U		41.13 U		37.32 U		41.08 U	
Mercury	0.10		0.06 U		0.09		0.07		0.06 U		0.06 U		0.05 U		0.06 U	

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Field Sample Number ->	BG5CWL8		BG6BWL4		BG6CWL17		BG4CUCD		BG4BBLD		BG5CWL8	
Lab Analysis Number ->	UC02366		UC02367		UC02368		UC02369		UC02370		UC02371	
Metals (ug/g)												
Arsenic	3.04	U	4.14		3.52		3.05	U	5.47		3.02	U
Selenium	0.55	U	0.55	U	0.51	U	0.55	U	0.54	U	0.54	U
Lead	22.96	J1	23.67	J1	18.58	J1	19.24	J1	17.60	J1	22.37	J1
Silver	0.02	U	0.02	U	0.01	U	0.02	U	0.01	U	0.01	U
Barium	174.97	J1	166.46	J1	55.63	J1	144.95	J1	76.65	J1	175.33	J1
Beryllium	1.51		1.58		0.67		1.50		0.51	U	1.46	
Cadmium	1.46	U	1.48	U	1.35	U	1.46	U	1.44	U	1.45	U
Chromium	47.63		48.83		26.58		53.11		42.04		48.85	
Nickel	27.34		26.76		13.18		26.43		14.61		27.93	
Antimony	23.82	U	24.17	U	22.07	U	23.87	U	23.47	U	23.70	U
Thallium	41.68	U	42.29	U	38.63	U	41.78	U	41.08	U	41.48	U
Mercury	0.06	U	0.06	U	0.06	U	0.06	U	0.19		0.06	U

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Field Sample Number ->	BG1BBL4		BG1BUC3		BG1CBL10		BG2CBL17		BG3CWL22		BG4BBL5		BG4BBLD		BG4CUC17	
Lab Analysis Number ->	UC02324		UC02308		UC02325		UC02327		UC02333		UC02361		UC02370		UC02358	
Other Parameters (ug/g)																
Extractable Organic Halides (total)																
*TOTAL ORGANIC CARBON	4,246.58		1,246.88	U	1,223.99	U	1,275.51	U	1,203.37	U	2,250.30		14,610.80		1,666.67	

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Field Sample Number ->	BG4CUCD		BG5BWL3		BG5CWL8		BG6BWL4		BG8BUC5		BG8CUC10		NRSE1		NRSE2	
Lab Analysis Number ->	UC02369		UC02365		UC02366		UC02367		UC02318		UC02323		UC02391		UC02392	
Other Parameters (ug/g)																
Extractable Organic Halides (total)													185.53 U		158.48 U	
*TOTAL ORGANIC CARBON	1,778.32		3,365.27		1,980.56		2,157.83		1,305.48 U		1,275.51 U		91,651.20		58,478.60	

Field Sample Number ->	NRSE3		NRSE4		NRSE5		NRSE6		NRSE8	
Lab Analysis Number ->	UC02393		UC02485		UC02276		UC02486		UC02277	
Other Parameters (ug/g)										
Extractable Organic Halides (total)	166.67 U		129.87 U		81.53 U		152.67 U		61.97 U	
*TOTAL ORGANIC CARBON	36,333.30		9,831.17		11,251.70		22,595.40		20,218.60	

Field Sample Number ->	BG1BUC3	BG4CUC17	BG8BUC5	BG8CUC10	BG1BBL4	BG1CBL10	BG2CBL17	BG4BBL5	BG3CWL22		
Lab Analysis Number ->	UC02308	UC02358	UC02318	UC02323	UC02324	UC02325	UC02327	UC02361	UC02333		
Corrossivity	4.67	7.49	5.08	5.09	5.49	5.47	5.97	7.33	6.93		

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Field Sample Number ->	BG5BWL3		BG5CWL8		BG6BWL4		BG4CUCD		BG4BBLD	
Lab Analysis Number ->	UC02365		UC02366		UC02367		UC02369		UC02370	
Corrossivity	6.99		6.21		7.03		7.51		7.13	



Alliant Techsystems Inc.
Radford Army Ammunition Plant
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Radford, VA 24141-0100

February 19, 1997

97-815-063

U. S. Environmental Protection Agency
Region III
841 Chestnut Building
Philadelphia, PA 19109-4431

Attention: Ms. Mary Beck, 3HW90

Re: Radford Army Ammunition Plant, Submittal of revised Appendix H of the Draft RCRA
Facility Investigation Report

Enclosed are three copies, with signed certification, of the revised Appendix H, Summary Statistics for Background Distributions, of the Draft RCRA Facility investigation (RGFI) report for Solid Waste management Units 17, 31, 48, and 54, Radford Army Ammunition Plant. A preliminary copy was delivered to you Thursday, February 20, 1997.

The certification statement is Attachment 1. The revisions to Appendix H are based on the review comments from the USEPA and discussed in a telephone conversation between Parsons ES, USAEC and USEPA on June 18, 1996. A copy of these comments and the responses are included as Attachment 2. Attachment 3 includes a brief explanation of the changes that were made and all of the pages of Appendix H that were affected by this revision. Attachment 4 includes the revised version of Appendix H. Please entirely replace Appendix H in Volume II of RFI Report for Solid Waste management Units 17, 31, 48, and 54 with Attachment 4.

The certified copies of this submittal will be delivered to you Friday, February 21, 1997. AEC is currently reviewing the Draft RFI Report for Solid Waste Management Units 17, 31, 48, and 54 to determine which sections will be affected by the revision to Appendix H.

Sincerely:

A handwritten signature in cursive script, appearing to read "C. A. Jake".

C. A. Jake
Environmental Affairs Supervisor

JJRedder:V\815-063
Enclosures

c: Robert Thomson, P.E., EPA Region III (2)
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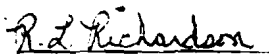
Leslie Romanchik
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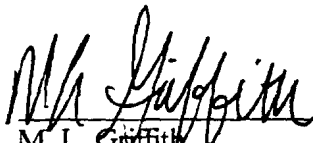
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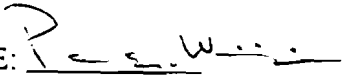
ATTACHMENT 1

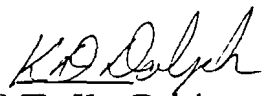
CERTIFICATION

Concerning the following documents, submitted, February 20, 1997:

1. EPA comments dated April 22, 1996 and Parsons Engineering Science, Inc. responses.
2. Revisions made to Appendix H
3. Revised Appendix H of the Draft RCRA Facility Investigation Report for Solid Waste Management Units 17, 31, 48, and 54.

I certify under penalty of law that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gather and evaluate the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I am aware that there are significant penalties for submitting false information, including the possibility of fines and imprisonment for knowing violations.

SIGNATURE: 
PRINTED NAME: Paul Wojciechowski
TITLE: LTC, CM, Commanding
Radford AAP

SIGNATURE: 
PRINTED NAME: Ken Dolph
TITLE: Resident Manager
Alliant Techsystems Inc.

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ATTACHMENT 2

USEPA COMMENTS DATED APRIL 22, 1996

AND

PARSONS ENGINEERING SCIENCE, INC. RESPONSES

RESPONSE TO USEPA REGION III

USEPA comments on the *Draft RCRA Facility Investigation Report for Solid Waste Management Units 17, 31, 48 and 54 Radford Army Ammunition Plant, Radford, Virginia*, Parsons Engineering Science, Inc., January 1996.

Part I. Response to Draft Comments on RAAP Plan for Establishing Background Soil Concentrations and for Evaluating SWMU Data Against Background, by James R. Brown, U.S. EPA, Office of Solid Waste (5303W). These comments were responded to on June 18, 1996 in a conference call involving Jim Brown (U.S. EPA), Mary Beck (U.S. EPA), Rob Davie (U.S. AEC), John Segna (Parsons ES), and Tim Schmitt (Parsons ES).

Comment 2a:

Arsenic Soil C Shapiro-Wilk test--The wrong coefficients are used. The sample size is 8, so the following coefficients ($a_{(n-i+1)}$) should be used: 0.6052, 0.3164, 0.1743, 0.0561.

Response:

Concur. The wrong coefficients were used for the SWMU 17a and SWMU 17bcd arsenic soil horizon C Shapiro-Wilk tests. The analysis was performed again using the correct coefficients. However, the results of the test did not change.

Comment 2b:

For all Shapiro-Wilk test results, passing the test at the 1% significance level would suffice (Parsons Engineering used 5%). This allows more of the data sets to pass the test on the original scale, and therefore obviates the need for data transformations in many cases.

Response:

Parsons ES used the more conservative 5% significance level and it does not appear useful to change the significance level of the Shapiro Wilk test now. Parsons ES believes that the transformed data more accurately represents the natural distribution of metals in soil, which are typically assumed to be lognormally distributed.

Comment 2c:

Chromium Soil B--An incorrect interpretation is made for the Shapiro Wilk normality test. The calculated W exceeds the critical W, so the correct conclusion should be that the lognormally transformed data meet the assumption of normality (Parsons Engineering declares incorrectly that the lognormally transformed data do not meet the assumption of normality). The same incorrect conclusions were given for Lead horizon B.

Response:

Concur. Parsons ES incorrectly interpreted the Shapiro-Wilk test results for SWMU 17a and 17bcd for chromium and for lead in soil horizon B. These corrections have been made, but the corrections did not effect the results of the tolerance limit comparisons.

Comment 2d:

The Normal Tolerance limits are incorrect. Parsons Engineering did not seem to multiply the tolerance factor (K) by the standard deviation. I observed this in the data set that I checked (Barium horizon b: which calculated the upper tolerance limit by adding to the mean the kappa factor without first multiplying the kappa factor by the standard deviation). It appears as though all other normal tolerance limits were calculated the same way. The poisson based tolerance limit calculations appear to be correct.

Response:

Concur. The normal tolerance limits were recalculated using the correct formula. The results remain the same for all analyses with the exception that there are no longer exceedances for barium or lead in SWMU 17a, soil horizon B.

Comment 3:

The tail area probability "tests" provided for the sediments data are not very revealing. What criteria are used to evaluate samples? Was the Shapiro-Wilk test used to determine whether the normal or lognormal tail area probabilities would be calculated?

Response:

Concur. Parsons ES chose the tail area probability comparison as a crude estimate of differences between sediment metals SWMU samples vs. background based on the limited number of background and SWMU sediment metals samples to be collected.

ATTACHMENT 3**REVISIONS MADE TO APPENDIX H**

ATTACHMENT 3

Appendix H was reevaluated based on the comments from the USEPA included as Attachment 2. The changes that were required based on these comments are included in this Attachment, and summarized below.

- The Shapiro-Wilk Goodness of Fit Test was recalculated for one distribution.
- The Shapiro-Wilk Goodness of Fit Test was re-interpreted for two distributions regarding their fit to normal and lognormal distributions.
- A Table "Summary of Tolerance Limits" has been added to Appendix H.
- Thirty two (32) upper tolerance limits were recalculated for various constituents at each of the SWMUs. The upper tolerance limit was recalculated for all of the constituents listed on the Summary of Tolerance Limits Table which have a "normal" tolerance limit type.
- The revised calculations of the upper tolerance limits are shown on individual sheets. These sheets also show the reevaluation of the site data based on the revised tolerance limits.

SHAPIRO-WILK GOODNESS OF FIT TEST

1. Order samples from smallest to largest in column x(i)
2. Order samples from largest to smallest in column x(n-i+1)
3. Compute K as the greatest integer less than or equal to N/2. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column a(n-i+1).
5. Sum the values in column b(i) and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W, the distribution is non-normal. Transform and re-test.

i	x(i)	x(n-i+1)	x(n-i+1)-x(i)	a(n-i+1)	b(i)
1	0.31	2.27	1.95628369	0.6052	1.1839429
2	0.44	2.19	1.74361013	0.3164	0.5516782
3	0.47	2.09	1.62	0.1743	0.2826903
4	1.70	1.94	0.24	0.0561	0.0132077
5	1.94	1.70			2.0315191
6	2.09	0.47			
7	2.19	0.44			
8	2.27	0.31			

std dev = 0.6510165

N = 8

K = 4

b = 2.0315191

W = 1.3911045

Critical W = 0.748

Result = Lognormally transformed data meets assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST

1. Order samples from smallest to largest in column x(i)
2. Order samples from largest to smallest in column x(n-i+1)
3. Compute K as the greatest integer less than or equal to N/2. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column a(n-i+1).
5. Sum the values in column b(i) and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W, the distribution is non-normal. Transform and re-test.

i	x(i)	x(n-i+1)	x(n-i+1)-x(i)	a(n-i+1)	b(i)
1	3.42	4.06	0.63808253	0.6052	0.3861675
2	3.63	4.02	0.39078734	0.3164	0.1236451
3	3.70	3.94	0.2418529	0.1743	0.042155
4	3.83	3.93	0.09669377	0.0561	0.0054245
5	3.93	3.83	-0.09669377		0
6	3.94	3.70	-0.2418529		0
7	4.02	3.63			0.5573921
8	4.06	3.42			

std dev = 0.217995

N = 8

K = 4

b = 0.5573921

W = 0.9339647

Critical W = 0.818

Result = Lognormally transformed data meets assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST

1. Order samples from smallest to largest in column $x(i)$
2. Order samples from largest to smallest in column $x(n-i+1)$
3. Compute K as the greatest integer less than or equal to $N/2$. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column $a(n-i+1)$.
5. Sum the values in column $b(i)$ and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W , the distribution is non-normal. Transform and re-test.

i	$x(i)$	$x(n-i+1)$	$x(n-i+1)-x(i)$	$a(n-i+1)$	$b(i)$
1	1.65	5.43	3.78100599	0.6052	2.2882648
2	2.87	3.50	0.62722638	0.3164	0.1984544
3	3.02	3.33	0.31108885	0.1743	0.0542228
4	3.06	3.09	0.0282268	0.0561	0.0015835
5	3.09	3.06	-0.0282268		0
6	3.33	3.02	-0.31108885		0
7	3.50	2.87	-0.62722638		2.5425256
8	5.43	1.65	-3.78100599		

std dev = 1.0448547

N = 8

K = 4

b = 2.5425256

W = 0.8459035

Critical W = 0.818

Result = Lognormally transformed data meets assumption of normality

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**SUMMARY OF TOLERANCE LIMITS
RADFORD ARMY AMMUNITION PLANT**

Soil Horizon	Soil Series	Constituent	Upper	Tolerance	Exceedance?
			Limit	Limit Type	
SWMU 17A	B	Antimony	21.0	Poisson	Yes
SWMU 17A	B	Arsenic	5.5	Poisson	Yes
SWMU 17A	B	Barium	9.7	Normal	No
SWMU 17A	B	Beryllium	4.5	Poisson	No
SWMU 17A	B	Cadmium	3.5	Poisson	Yes
SWMU 17A	B	Chromium	5.1	Normal	Yes
SWMU 17A	B	Lead	8.7	Normal	No
SWMU 17A	B	Mercury	1.5	Poisson	No
SWMU 17A	B	Nickel	6.0	Normal	Yes
SWMU 17A	B	Selenium	2.5	Poisson	No
SWMU 17A	B	Silver	1.5	Poisson	Yes
SWMU 17A	B	Thallium	33.5	Poisson	No
SWMU 17A	C	Antimony	21.5	Poisson	No
SWMU 17A	C	Arsenic	11.5	Poisson	Yes
SWMU 17A	C	Barium	6.9	Normal	No
SWMU 17A	C	Beryllium	2.7	Normal	No
SWMU 17A	C	Cadmium	3.5	Poisson	No
SWMU 17A	C	Chromium	5.0	Normal	No
SWMU 17A	C	Lead	4.2	Normal	Yes
SWMU 17A	C	Mercury	1.5	Poisson	No
SWMU 17A	C	Nickel	5.4	Normal	No
SWMU 17A	C	Selenium	2.5	Poisson	No
SWMU 17A	C	Silver	1.5	Poisson	Yes
SWMU 17A	C	Thallium	33.5	Poisson	No
SWMU 17BCD	B	Antimony	21.0	Poisson	No
SWMU 17BCD	B	Arsenic	5.5	Poisson	Yes
SWMU 17BCD	B	Barium	9.7	Normal	No
SWMU 17BCD	B	Beryllium	4.5	Poisson	No
SWMU 17BCD	B	Cadmium	3.5	Poisson	No
SWMU 17BCD	B	Chromium	5.1	Normal	No
SWMU 17BCD	B	Lead	8.7	Normal	No
SWMU 17BCD	B	Mercury	1.5	Poisson	No
SWMU 17BCD	B	Nickel	6.0	Normal	No
SWMU 17BCD	B	Selenium	2.5	Poisson	No
SWMU 17BCD	B	Silver	1.5	Poisson	No
SWMU 17BCD	B	Thallium	33.5	Poisson	No
SWMU 17BCD	C	Antimony	21.5	Poisson	No
SWMU 17BCD	C	Arsenic	11.5	Poisson	No
SWMU 17BCD	C	Barium	6.9	Normal	No
SWMU 17BCD	C	Beryllium	2.3	Normal	Yes
SWMU 17BCD	C	Cadmium	3.5	Poisson	Yes
SWMU 17BCD	C	Chromium	5.0	Normal	No
SWMU 17BCD	C	Lead	4.2	Normal	Yes
SWMU 17BCD	C	Mercury	1.5	Poisson	No
SWMU 17BCD	C	Nickel	5.4	Normal	No
SWMU 17BCD	C	Selenium	2.5	Poisson	No
SWMU 17BCD	C	Silver	1.5	Poisson	No
SWMU 17BCD	C	Thallium	33.5	Poisson	No

SUMMARY OF TOLERANCE LIMITS RADFORD ARMY AMMUNITION PLANT

Soil Horizon	Soil Series	Constituent	Upper	Tolerance	Exceedance?
			Limit	Limit Type	
SWMU 31	C	Antimony	20.5	Poisson	No
SWMU 31	C	Arsenic	7.0	Poisson	No
SWMU 31	C	Barium	7.1	Normal	No
SWMU 31	C	Beryllium	.5	Normal	No
SWMU 31	C	Cadmium	3.5	Poisson	No
SWMU 31	C	Chromium	4.8	Normal	No
SWMU 31	C	Lead	4.1	Normal	No
SWMU 31	C	Mercury	2.0	Poisson	No
SWMU 31	C	Nickel	4.3	Normal	No
SWMU 31	C	Selenium	2.5	Poisson	No
SWMU 31	C	Silver	1.5	Poisson	No
SWMU 31	C	Thallium	31.5	Poisson	No
SWMU 54	B	Antimony	20.5	Poisson	No
SWMU 54	B	Arsenic	6.5	Poisson	No
SWMU 54	B	Barium	7.4	Normal	No
SWMU 54	B	Beryllium	5.0	Poisson	No
SWMU 54	B	Cadmium	3.5	Poisson	Yes
SWMU 54	B	Chromium	5.0	Normal	No
SWMU 54	B	Lead	4.7	Normal	Yes
SWMU 54	B	Mercury	1.5	Poisson	Yes
SWMU 54	B	Nickel	5.0	Normal	No
SWMU 54	B	Selenium	2.5	Poisson	No
SWMU 54	B	Silver	2.0	Poisson	No
SWMU 54	B	Thallium	32.0	Poisson	No
SWMU 54	C	Antimony	20.5	Poisson	No
SWMU 54	C	Arsenic	7.0	Poisson	No
SWMU 54	C	Barium	7.1	Normal	No
SWMU 54	C	Beryllium	.5	Normal	Yes
SWMU 54	C	Cadmium	3.5	Poisson	No
SWMU 54	C	Chromium	4.8	Normal	No
SWMU 54	C	Lead	4.1	Normal	Yes
SWMU 54	C	Mercury	2.0	Poisson	No
SWMU 54	C	Nickel	4.3	Normal	No
SWMU 54	C	Selenium	2.5	Poisson	No
SWMU 54	C	Silver	1.5	Poisson	No
SWMU 54	C	Thallium	31.5	Poisson	No

Barium horizon B

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Normal Tolerance Limit (K) Calculation for Barium soil horizon B, SWMU 17A

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	4.39
Where		std. dev.	0.83
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	6.399951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17ASB105	8.54	9.7019594	5128.21	16349.61	No
17ASB205	4.16	9.7019594	64.38	16349.61	No
17ASB305	4.27	9.7019594	71.26	16349.61	No

Barium horizon C

Normal Tolerance Limit (K) Calculation for Barium soil horizon C

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	4.51
Where		std. dev.	0.37
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	6.519951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17ASB110	4.15	6.9223819	63.12	1014.7341	No
17ASB210	4.33	6.9223819	75.69	1014.7341	No
17ASB310	4.84	6.9223819	126.39	1014.7341	No
17ASB115	4.24	6.9223819	69.20	1014.7341	No
17ASB215	4.46	6.9223819	86.91	1014.7341	No
17ASB315	3.81	6.9223819	45.16	1014.7341	No
17ASB120	4.24	6.9223819	69.36	1014.7341	No
17ASB220	4.90	6.9223819	134.25	1014.7341	No
17ASB320	3.97	6.9223819	52.97	1014.7341	No
17ASB122	4.27	6.9223819	71.50	1014.7341	No
17ASB225	2.26	6.9223819	9.56	1014.7341	No
17ASB325	4.00	6.9223819	54.71	1014.7341	No
17ASB340	3.54	6.9223819	34.58	1014.7341	No

Beryllium horizon C

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Normal Tolerance Limit (K) Calculation for Beryllium soil horizon C, SWMU 17A

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	0.7
Where		std. dev.	0.59
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	2.709951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17ASB110	0.80	2.2988711	2.22	9.962929	No
17ASB210	0.72	2.2988711	2.06	9.962929	No
17ASB310	2.00	2.2988711	7.39	9.962929	No
17ASB115	0.75	2.2988711	2.11	9.962929	No
17ASB215	1.51	2.2988711	4.52	9.962929	No
17ASB315	0.79	2.2988711	2.20	9.962929	No
17ASB120	0.57	2.2988711	1.77	9.962929	No
17ASB220	1.92	2.2988711	6.82	9.962929	No
17ASB320	-0.56	2.2988711	0.57	9.962929	No
17ASB122	0.76	2.2988711	2.13	9.962929	No
17ASB225	-1.17	2.2988711	0.31	9.962929	No
17ASB325	-0.26	2.2988711	0.77	9.962929	No
17ASB340	0.44	2.2988711	1.55	9.962929	No

Chromium soil B

Normal Tolerance Limit (K) Calculation for Chromium soil horizon B, SWMU 17A

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	3.82
Where		std. dev.	0.22
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	5.829951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17ASB105	7.63	5.1025892	2051.28	164.44715	Yes
17ASB205	3.85	5.1025892	46.82	164.44715	No
17ASB305	3.98	5.1025892	53.71	164.44715	No

Chromium soil C

Normal Tolerance Limit (K) Calculation for Chromium soil horizon C, SWMU 17A

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	3.83
Where		std. dev.	0.2
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	5.839951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17ASB110	4.02	4.9979902	55.51	148.11518	No
17ASB210	3.91	4.9979902	49.70	148.11518	No
17ASB310	4.37	4.9979902	79.33	148.11518	No
17ASB115	4.00	4.9979902	54.72	148.11518	No
17ASB215	4.45	4.9979902	86.04	148.11518	No
17ASB315	4.33	4.9979902	75.99	148.11518	No
17ASB120	4.01	4.9979902	54.92	148.11518	No
17ASB220	4.81	4.9979902	122.27	148.11518	No
17ASB320	2.85	4.9979902	17.25	148.11518	No
17ASB122	4.23	4.9979902	68.50	148.11518	No
17ASB225	2.02	4.9979902	7.56	148.11518	No
17ASB325	3.12	4.9979902	22.59	148.11518	No
17ASB340	3.82	4.9979902	45.44	148.11518	No

Lead horizon B

Normal Tolerance Limit (K) Calculation for Lead soil horizon B, SWMU 17A

$K = \text{average} + t(N-1, \alpha) * \text{SQRT}(1 + (1/N))$		average	3.24
Where		std. dev.	1.04
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	5.249951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17ASB105	8.57	8.6999491	5256.41	6002.6065	No
17ASB205	3.27	8.6999491	26.28	6002.6065	No
17ASB305	3.30	8.6999491	27.08	6002.6065	No

Lead horizon C

Normal Tolerance Limit (K) Calculation for Lead soil horizon C, SWMU 17A

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	2.71
Where		std. dev.	0.31
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	4.719951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17ASB110	4.62	4.1731848	101.39	64.921888	Yes
17ASB210	2.65	4.1731848	14.13	64.921888	No
17ASB310	3.14	4.1731848	23.02	64.921888	No
17ASB115	4.03	4.1731848	56.44	64.921888	No
17ASB215	4.24	4.1731848	69.06	64.921888	Yes
17ASB315	3.08	4.1731848	21.83	64.921888	No
17ASB120	5.61	4.1731848	273.97	64.921888	Yes
17ASB220	3.73	4.1731848	41.78	64.921888	No
17ASB320	3.43	4.1731848	30.77	64.921888	No
17ASB122	2.47	4.1731848	11.79	64.921888	No
17ASB225	4.35	4.1731848	77.36	64.921888	Yes
17ASB325	2.22	4.1731848	9.23	64.921888	No
17ASB340	2.75	4.1731848	15.70	64.921888	No

Nickel horizon B

Normal Tolerance Limit (K) Calculation for Nickel soil horizon B, SWMU 17A

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	2.97
Where		std. dev.	0.61
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	4.979951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17ASB105	6.81	6.0077701	902.56	406.5757	Yes
17ASB205	3.26	6.0077701	26.15	406.5757	No
17ASB305	3.55	6.0077701	34.64	406.5757	No

Nickel horizon C

Normal Tolerance Limit (K) Calculation for Nickel soil horizon C, SWMU 17A

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	3.24
Where		std. dev.	0.42
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	5.249951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17ASB110	3.21	5.4449794	24.84	231.59252	No
17ASB210	3.32	5.4449794	27.78	231.59252	No
17ASB310	4.27	5.4449794	71.26	231.59252	No
17ASB115	3.37	5.4449794	29.20	231.59252	No
17ASB215	4.04	5.4449794	56.83	231.59252	No
17ASB315	3.60	5.4449794	36.43	231.59252	No
17ASB120	3.19	5.4449794	24.28	231.59252	No
17ASB220	4.37	5.4449794	78.96	231.59252	No
17ASB320	1.84	5.4449794	6.30	231.59252	No
17ASB122	3.35	5.4449794	28.37	231.59252	No
17ASB225	1.81	5.4449794	6.12	231.59252	No
17ASB325	2.39	5.4449794	10.90	231.59252	No
17ASB340	3.17	5.4449794	23.71	231.59252	No

Barium horizon B

Normal Tolerance Limit (K) Calculation for Barium soil horizon B, SWMU 17BCD

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	4.39
Where		std. dev.	0.83
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	6.399951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17CSB105	3.38	9.7019594	29.40	16349.61	No
17CSB205	3.60	9.7019594	36.74	16349.61	No
17DSB105	4.23	9.7019594	68.93	16349.61	No
17DSB205	4.19	9.7019594	65.89	16349.61	No

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Barium horizon C

Normal Tolerance Limit (K) Calculation for Barium soil horizon C, SWMU 17BCD

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	4.51
Where		std. dev.	0.37
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	6.519951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17CSB110	4.36	6.9223819	78.55	1014.7341	No
17CSB210	4.25	6.9223819	70.12	1014.7341	No
17DSB110	4.10	6.9223819	60.40	1014.7341	No
17DSB210	4.39	6.9223819	80.98	1014.7341	No
17CSB114	4.43	6.9223819	84.33	1014.7341	No
17CSB215	4.65	6.9223819	104.70	1014.7341	No
17DSB115	4.21	6.9223819	67.05	1014.7341	No
17DSB215	4.96	6.9223819	142.65	1014.7341	No
17DSB120	4.24	6.9223819	69.69	1014.7341	No
17DSB220	4.72	6.9223819	111.91	1014.7341	No
17DSB125	4.29	6.9223819	72.73	1014.7341	No
17DSB225	4.02	6.9223819	55.95	1014.7341	No
17DSB127	4.71	6.9223819	111.48	1014.7341	No
17CSB240	4.46	6.9223819	86.49	1014.7341	No
17DSB240	4.23	6.9223819	68.85	1014.7341	No

Beryllium horizon C

Normal Tolerance Limit (K) Calculation for Beryllium soil horizon C, SWMU 17BCD

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	0.70
Where		std. dev.	0.59
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	2.709951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17CSB110	1.65	2.2988711	5.19	9.962929	No
17CSB210	1.75	2.2988711	5.77	9.962929	No
17DSB110	0.70	2.2988711	2.02	9.962929	No
17DSB210	0.91	2.2988711	2.48	9.962929	No
17CSB114	1.28	2.2988711	3.61	9.962929	No
17CSB215	0.92	2.2988711	2.52	9.962929	No
17DSB115	1.16	2.2988711	3.21	9.962929	No
17DSB215	2.06	2.2988711	7.88	9.962929	No
17DSB120	1.11	2.2988711	3.04	9.962929	No
17DSB220	1.70	2.2988711	5.48	9.962929	No
17DSB125	1.56	2.2988711	4.77	9.962929	No
17DSB225	2.47	2.2988711	11.84	9.962929	Yes
17DSB127	1.77	2.2988711	5.89	9.962929	No
17CSB240	1.83	2.2988711	6.21	9.962929	No
17DSB240	0.80	2.2988711	2.23	9.962929	No

Chromium horizon B

Normal Tolerance Limit (K) Calculation for Chromium soil horizon B, SWMU 17BCD

K = average + t((N-1), alpha) * SQRT(1 + (1/N))		average	3.82
Where		std. dev.	0.22
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	5.829951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17CSB105	4.13	5.1025892	61.87	164.44715	No
17CSB205	3.52	5.1025892	33.62	164.44715	No
17DSB105	3.40	5.1025892	29.92	164.44715	No
17DSB205	3.44	5.1025892	31.28	164.44715	No

Chromium horizon C

Normal Tolerance Limit (K) Calculation for Chromium soil horizon C, SWMU 17A

K =average+ t((N-1),alpha)*SQRT(1+(1/N))		average	3.83
Where		std. dev.	0.2
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	5.839951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17CSB110	4.29	4.9979902	72.81	148.11518	No
17CSB210	3.99	4.9979902	54.29	148.11518	No
17DSB110	3.78	4.9979902	43.94	148.11518	No
17DSB210	4.03	4.9979902	56.30	148.11518	No
17CSB114	4.09	4.9979902	59.89	148.11518	No
17CSB215	4.28	4.9979902	71.92	148.11518	No
17DSB115	4.22	4.9979902	67.82	148.11518	No
17DSB215	4.58	4.9979902	97.09	148.11518	No
17DSB120	4.03	4.9979902	56.07	148.11518	No
17DSB220	4.15	4.9979902	63.30	148.11518	No
17DSB125	4.47	4.9979902	86.92	148.11518	No
17DSB225	4.35	4.9979902	77.76	148.11518	No
17DSB127	4.36	4.9979902	77.87	148.11518	No
17CSB240	4.31	4.9979902	74.38	148.11518	No
17DSB240	3.90	4.9979902	49.18	148.11518	No

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Lead horizon B

Normal Tolerance Limit (K) Calculation for Lead soil horizon B, SWMU 17BCD

K =average+ t((N-1),alpha)*SQRT(1+(1/N))		average	3.24
Where		std. dev.	1.04
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	5.249951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17CSB105	3.73	8.6999491	41.82	6002.6065	No
17CSB205	2.50	8.6999491	12.20	6002.6065	No
17DSB105	3.00	8.6999491	20.08	6002.6065	No
17DSB205	3.04	8.6999491	20.81	6002.6065	No

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Lead horizon C

Normal Tolerance Limit (K) Calculation for Lead soil horizon C, SWMU 17BCD

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	2.71
Where		std. dev.	0.31
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	4.719951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17CSB110	2.91	4.1731848	18.44	64.921888	No
17CSB210	2.62	4.1731848	13.68	64.921888	No
17DSB110	2.89	4.1731848	17.95	64.921888	No
17DSB210	2.88	4.1731848	17.87	64.921888	No
17CSB114	2.93	4.1731848	18.73	64.921888	No
17CSB215	5.25	4.1731848	190.60	64.921888	Yes
17DSB115	3.28	4.1731848	26.54	64.921888	No
17DSB215	3.14	4.1731848	23.10	64.921888	No
17DSB120	2.51	4.1731848	12.36	64.921888	No
17DSB220	2.43	4.1731848	11.31	64.921888	No
17DSB125	3.34	4.1731848	28.23	64.921888	No
17DSB225	2.13	4.1731848	8.43	64.921888	No
17DSB127	3.16	4.1731848	23.46	64.921888	No
17CSB240	2.85	4.1731848	17.24	64.921888	No
17DSB240	2.68	4.1731848	14.63	64.921888	No

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Nickel horizon B

Normal Tolerance Limit (K) Calculation for Nickel soil horizon B, SWMU 17BCD

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	2.97
Where		std. dev.	0.61
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	4.979951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17CSB105	3.26	6.0077701	25.95	406.5757	No
17CSB205	2.93	6.0077701	18.68	406.5757	No
17DSB105	2.68	6.0077701	14.58	406.5757	No
17DSB205	2.41	6.0077701	11.18	406.5757	No

Nickel horizon C

Normal Tolerance Limit (K) Calculation for Nickel soil horizon C, SWMU 17BCD

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	3.24
Where		std. dev.	0.42
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	5.249951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17CSB110	3.83	5.4449794	46.17	231.59252	No
17CSB210	3.84	5.4449794	46.60	231.59252	No
17DSB110	2.79	5.4449794	16.21	231.59252	No
17DSB210	3.36	5.4449794	28.79	231.59252	No
17CSB114	3.56	5.4449794	35.33	231.59252	No
17CSB215	3.82	5.4449794	45.62	231.59252	No
17DSB115	3.37	5.4449794	28.97	231.59252	No
17DSB215	4.28	5.4449794	72.05	231.59252	No
17DSB120	3.82	5.4449794	45.53	231.59252	No
17DSB220	4.05	5.4449794	57.42	231.59252	No
17DSB125	3.92	5.4449794	50.40	231.59252	No
17DSB225	4.48	5.4449794	87.82	231.59252	No
17DSB127	4.20	5.4449794	66.39	231.59252	No
17CSB240	4.04	5.4449794	56.83	231.59252	No
17DSB240	3.15	5.4449794	23.33	231.59252	No

Barium horizon C

Normal Tolerance Limit (K) Calculation for Barium soil horizon C, SWMU 31

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	4.53
Where		std. dev.	0.38
t =	Critical value of Student's t distribution	t	2.015
N =	Sample size	N	6
alpha =	Probability level test is conducted at (here, 0.05)	K	6.7064488

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
31MW3A1	4.90	7.0784505	134.00	1186.1292	No
31MW2A	4.90	7.0784505	134.90	1186.1292	No
31MW4A1	4.92	7.0784505	136.78	1186.1292	No
31MW3B2	4.32	7.0784505	75.10	1186.1292	No
31MW2B	4.58	7.0784505	97.33	1186.1292	No
31MW4B2	4.42	7.0784505	82.68	1186.1292	No
31MW1A2	3.34	7.0784505	28.11	1186.1292	No
31MW1B3	4.07	7.0784505	58.39	1186.1292	No
31MW4C4	4.95	7.0784505	140.53	1186.1292	No

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Beryllium C

Normal Tolerance Limit (K) Calculation for Beryllium soil horizon C, SWMU 31

K = average + t((N-1), alpha) * SQRT(1 + (1/N))		average	-0.09993
Where		std. dev.	0.27
t =	Critical value of Student's t distribution	t	2.015
N =	Sample size	N	6
alpha =	Probability level test is conducted at (here, 0.05)	K	2.0765188

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
31MW3A1	-0.05	0.4607301	0.95	1	No
31MW2A	0.00	0.4607301	1.00	1	Yes
31MW4A1	0.17	0.4607301	1.18	1	Yes
31MW3B2	-0.29	0.4607301	0.75	1	No
31MW2B	0.06	0.4607301	1.06	1	Yes
31MW4B2	-0.19	0.4607301	0.83	1	No
31MW1A2	-0.06	0.4607301	0.94	1	No
31MW1B3	0.16	0.4607301	1.18	1	Yes
31MW4C4	0.20	0.4607301	1.22	1	Yes

Chromium horizon C

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Normal Tolerance Limit (K) Calculation for Chromium soil horizon C, SWMU 31

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	3.55
Where		std. dev.	0.22
t =	Critical value of Student's t distribution	t	2.015
N =	Sample size	N	6
alpha =	Probability level test is conducted at (here, 0.05)	K	5.7264488

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
31MW3A1	3.29	4.8098187	26.80	122.70937	No
31MW2A	3.78	4.8098187	43.94	122.70937	No
31MW4A1	3.78	4.8098187	43.91	122.70937	No
31MW3B2	2.97	4.8098187	19.50	122.70937	No
31MW2B	3.53	4.8098187	34.00	122.70937	No
31MW4B2	3.47	4.8098187	32.03	122.70937	No
31MW1A2	2.92	4.8098187	18.50	122.70937	No
31MW1B3	3.18	4.8098187	24.10	122.70937	No
31MW4C4	3.79	4.8098187	44.13	122.70937	No

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Lead horizon C

Normal Tolerance Limit (K) Calculation for Lead soil horizon C, SWMU 31

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	2.77
Where		std. dev.	0.26
t =	Critical value of Student's t distribution	t	2.015
N =	Sample size	N	6
alpha =	Probability level test is conducted at (here, 0.05)	K	4.9464488

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
31MW3A1	3.45	4.0560767	31.54	57.747305	No
31MW2A	3.05	4.0560767	21.16	57.747305	No
31MW4A1	2.87	4.0560767	17.70	57.747305	No
31MW3B2	3.69	4.0560767	40.00	57.747305	No
31MW2B	3.04	4.0560767	20.86	57.747305	No
31MW4B2	2.64	4.0560767	13.96	57.747305	No
31MW1A2	-0.46	4.0560767	0.63	57.747305	No
31MW1B3	1.99	4.0560767	7.32	57.747305	No
31MW4C4	2.99	4.0560767	19.98	57.747305	No

Nickel horizon C

Normal Tolerance Limit (K) Calculation for Nickel soil horizon C, SWMU 31

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	2.69
Where		std. dev.	0.34
t =	Critical value of Student's t distribution	t	2.015
N =	Sample size	N	6
alpha =	Probability level test is conducted at (here, 0.05)	K	4.8664488

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
31MW3A10	2.53	4.3445926	12.60	77.060635	No
31MW2A	2.59	4.3445926	13.37	77.060635	No
31MW4A12	3.01	4.3445926	20.23	77.060635	No
31MW3B20	2.59	4.3445926	13.30	77.060635	No
31MW2B	3.13	4.3445926	22.78	77.060635	No
31MW4B22	2.90	4.3445926	18.18	77.060635	No
31MW1A25	3.16	4.3445926	23.62	77.060635	No
31MW1B35	3.43	4.3445926	30.89	77.060635	No
31MW4C40	3.07	4.3445926	21.49	77.060635	No

Barium horizon B

Normal Tolerance Limit (K) Calculation for Barium soil horizon B, SWMU 54

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	4.95
Where		std. dev.	0.35
t =	Critical value of Student's t distribution	t	2.015
N =	Sample size	N	6
alpha =	Probability level test is conducted at (here, 0.05)	K	7.1264488

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
54SB10A	5.77	7.4442571	319.23	1710.0144	No
54SB11A	5.41	7.4442571	223.57	1710.0144	No
54SB12A	5.46	7.4442571	235.96	1710.0144	No
54SB13A	5.42	7.4442571	226.99	1710.0144	No
54SB14A	5.03	7.4442571	153.30	1710.0144	No
54SB16A	5.44	7.4442571	231.33	1710.0144	No
54SB1A	5.10	7.4442571	164.51	1710.0144	No
54SB2A	5.41	7.4442571	224.22	1710.0144	No
54SB3A	5.18	7.4442571	178.16	1710.0144	No
54SB4A	5.75	7.4442571	313.51	1710.0144	No
54SB5A	5.64	7.4442571	281.80	1710.0144	No
54SB6A	6.98	7.4442571	1077.02	1710.0144	No
54SB7A	4.93	7.4442571	138.29	1710.0144	No
54SB8A	5.24	7.4442571	188.63	1710.0144	No

Barium horizon C

Normal Tolerance Limit (K) Calculation for Barium soil horizon C, SWMU 54

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	4.53
Where		std. dev.	0.38
t =	Critical value of Student's t distribution	t	2.015
N =	Sample size	N	6
alpha =	Probability level test is conducted at (here, 0.05)	K	6.7064488
Limit =	Avg. + K(std. dev.)		

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
54SB15A	5.82	7.0784505	338.27	1186.1292	No
54SB9A	5.27	7.0784505	193.90	1186.1292	No
54SB16B	5.32	7.0784505	203.70	1186.1292	No
54SB14B	5.11	7.0784505	166.27	1186.1292	No
54SB6B	5.89	7.0784505	362.50	1186.1292	No
54SB10B	5.06	7.0784505	158.09	1186.1292	No
54SB11B	5.17	7.0784505	175.54	1186.1292	No
54SB12B	5.51	7.0784505	248.34	1186.1292	No
54SB2B	5.17	7.0784505	175.46	1186.1292	No
54SB3B	4.47	7.0784505	87.63	1186.1292	No
54SB4B	4.68	7.0784505	108.30	1186.1292	No
54SB5B	5.50	7.0784505	244.59	1186.1292	No
54SB7B	6.04	7.0784505	420.91	1186.1292	No
54SB8B	5.49	7.0784505	243.14	1186.1292	No
54SB9B	5.30	7.0784505	201.01	1186.1292	No
54SB10D	4.95	7.0784505	141.88	1186.1292	No
54SB13B	4.78	7.0784505	118.64	1186.1292	No
54SB1B	5.73	7.0784505	307.44	1186.1292	No
54SB16D	5.47	7.0784505	237.56	1186.1292	No

Beryllium horizon B

Poisson-based Tolerance Limit (K) Calculation for Beryllium soil horizon B, SWMU 54

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

$T_n =$ Poisson count of background

$n =$ Background sample size

alpha = Probability level test is conducted at (here, 0.05)

Tn	7.83
2Tn+2	17.66
Chi Square (2Tn+2)	28.4343
n	6
Lambda Tn	2.369525
2(Lambda Tn)	4.73905
Chi Square 0.05[2K+2] >=	4.73905
[2K+2] = 12	
K = 5	

FSampNo	Value	Limit	Limit Exceeded?
54SB10A	1.81	5	No
54SB11A	1.49	5	No
54SB12A	1.54	5	No
54SB13A	1.42	5	No
54SB14A	0.89	5	No
54SB16A	1.47	5	No
54SB1A	0.93	5	No
54SB2A	1.76	5	No
54SB3A	1.11	5	No
54SB4A	1.78	5	No
54SB5A	1.55	5	No
54SB6A	1.11	5	No
54SB7A	0.82	5	No
54SB8A	1.15	5	No

Chromium horizon B

Normal Tolerance Limit (K) Calculation for Chromium soil horizon B, SWMU 54

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	3.76
Where		std. dev.	0.21
t =	Critical value of Student's t distribution	t	2.015
N =	Sample size	N	6
alpha =	Probability level test is conducted at (here, 0.05)	K	5.9364488

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
54SB10A	3.52	5.0066542	33.86	149.40403	No
54SB11A	3.50	5.0066542	33.17	149.40403	No
54SB12A	3.59	5.0066542	36.08	149.40403	No
54SB13A	3.44	5.0066542	31.29	149.40403	No
54SB14A	3.02	5.0066542	20.52	149.40403	No
54SB16A	3.53	5.0066542	34.27	149.40403	No
54SB1A	3.23	5.0066542	25.38	149.40403	No
54SB2A	3.33	5.0066542	27.91	149.40403	No
54SB3A	3.34	5.0066542	28.16	149.40403	No
54SB4A	3.57	5.0066542	35.56	149.40403	No
54SB5A	3.54	5.0066542	34.54	149.40403	No
54SB6A	4.92	5.0066542	136.92	149.40403	No
54SB7A	3.18	5.0066542	24.00	149.40403	No
54SB8A	3.32	5.0066542	27.69	149.40403	No

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Chromium horizon C

Normal Tolerance Limit (K) Calculation for Chromium soil horizon C, SWMU 54

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	3.55
Where		std. dev.	0.22
t =	Critical value of Student's t distribution	t	2.015
N =	Sample size	N	6
alpha =	Probability level test is conducted at (here, 0.05)	K	5.7264488

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
54SB15A	3.83	4.8098187	45.93	122.70937	No
54SB9A	3.33	4.8098187	27.93	122.70937	No
54SB16B	3.53	4.8098187	34.20	122.70937	No
54SB14B	3.53	4.8098187	34.10	122.70937	No
54SB6B	4.25	4.8098187	70.14	122.70937	No
54SB10B	3.39	4.8098187	29.78	122.70937	No
54SB11B	3.49	4.8098187	32.93	122.70937	No
54SB12B	3.84	4.8098187	46.48	122.70937	No
54SB2B	3.38	4.8098187	29.45	122.70937	No
54SB3B	3.63	4.8098187	37.76	122.70937	No
54SB4B	3.06	4.8098187	21.30	122.70937	No
54SB5B	3.70	4.8098187	40.64	122.70937	No
54SB7B	4.04	4.8098187	57.10	122.70937	No
54SB8B	3.69	4.8098187	40.15	122.70937	No
54SB9B	3.63	4.8098187	37.56	122.70937	No
54SB10D	3.30	4.8098187	27.23	122.70937	No
54SB13B	3.48	4.8098187	32.32	122.70937	No
54SB1B	2.28	4.8098187	9.80	122.70937	No
54SB16D	3.77	4.8098187	43.53	122.70937	No

Lead horizon B

Normal Tolerance Limit (K) Calculation for Lead soil horizon B, SWMU 54

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	2.91
Where		std. dev.	0.35
t =	Critical value of Student's t distribution	t	2.015
N =	Sample size	N	6
alpha =	Probability level test is conducted at (here, 0.05)	K	5.0864488

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
54SB10A	5.33	4.6902571	205.56	108.88117	Yes
54SB11A	4.51	4.6902571	91.13	108.88117	No
54SB12A	3.06	4.6902571	21.22	108.88117	No
54SB13A	4.91	4.6902571	134.97	108.88117	Yes
54SB14A	3.60	4.6902571	36.56	108.88117	No
54SB16A	3.46	4.6902571	31.82	108.88117	No
54SB1A	6.57	4.6902571	716.80	108.88117	Yes
54SB2A	7.76	4.6902571	2354.26	108.88117	Yes
54SB3A	5.77	4.6902571	321.84	108.88117	Yes
54SB4A	4.43	4.6902571	84.26	108.88117	No
54SB5A	3.69	4.6902571	39.90	108.88117	No
54SB6A	8.24	4.6902571	3789.73	108.88117	Yes
54SB7A	3.92	4.6902571	50.29	108.88117	No
54SB8A	5.44	4.6902571	229.75	108.88117	Yes

Lead horizon C

Normal Tolerance Limit (K) Calculation for Lead soil horizon C

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	2.77
Where		std. dev.	0.26
t =	Critical value of Student's t distribution	t	2.015
N =	Sample size	N	6
alpha =	Probability level test is conducted at (here, 0.05)	K	4.9464488

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
54SB15A	3.35	4.0560767	28.40	57.747305	No
54SB9A	3.04	4.0560767	20.85	57.747305	No
54SB16B	2.70	4.0560767	14.81	57.747305	No
54SB14B	2.58	4.0560767	13.25	57.747305	No
54SB6B	6.07	4.0560767	430.56	57.747305	Yes
54SB10B	2.46	4.0560767	11.69	57.747305	No
54SB11B	2.49	4.0560767	12.11	57.747305	No
54SB12B	2.59	4.0560767	13.28	57.747305	No
54SB2B	2.66	4.0560767	14.23	57.747305	No
54SB3B	2.69	4.0560767	14.74	57.747305	No
54SB4B	2.12	4.0560767	8.36	57.747305	No
54SB5B	2.82	4.0560767	16.82	57.747305	No
54SB7B	3.13	4.0560767	22.79	57.747305	No
54SB8B	3.05	4.0560767	21.20	57.747305	No
54SB9B	2.76	4.0560767	15.83	57.747305	No
54SB10D	2.58	4.0560767	13.16	57.747305	No
54SB13B	2.11	4.0560767	8.23	57.747305	No
54SB1B	1.75	4.0560767	5.77	57.747305	No
54SB16D	2.62	4.0560767	13.68	57.747305	No

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Nickel horizon B

Normal Tolerance Limit (K) Calculation for Nickel soil horizon B, SWMU 54

$K = \text{average} + t(N-1, \alpha) * \text{SQRT}(1 + (1/N))$		average	2.98
Where		std. dev.	0.4
t =	Critical value of Student's t distribution	t	2.015
N =	Sample size	N	6
alpha =	Probability level test is conducted at (here, 0.05)	K	5.1564488

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
54SB10A	2.98	5.0425795	19.71	154.86898	No
54SB11A	3.00	5.0425795	20.05	154.86898	No
54SB12A	3.00	5.0425795	20.10	154.86898	No
54SB13A	2.94	5.0425795	18.90	154.86898	No
54SB14A	2.52	5.0425795	12.38	154.86898	No
54SB16A	3.02	5.0425795	20.56	154.86898	No
54SB1A	2.46	5.0425795	11.66	154.86898	No
54SB2A	2.33	5.0425795	10.25	154.86898	No
54SB3A	2.60	5.0425795	13.45	154.86898	No
54SB4A	3.07	5.0425795	21.44	154.86898	No
54SB5A	3.05	5.0425795	21.20	154.86898	No
54SB6A	2.83	5.0425795	16.99	154.86898	No
54SB7A	2.51	5.0425795	12.34	154.86898	No
54SB8A	2.75	5.0425795	15.60	154.86898	No

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Nickel horizon C

Normal Tolerance Limit (K) Calculation for Nickel soil horizon C, SWMU 54

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	2.69
Where		std. dev.	0.34
t =	Critical value of Student's t distribution	t	2.015
N =	Sample size	N	6
alpha =	Probability level test is conducted at (here, 0.05)	K	4.8664488

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
54SB15A	3.26	4.3445926	26.05	77.060635	No
54SB9A	2.87	4.3445926	17.68	77.060635	No
54SB16B	3.00	4.3445926	20.12	77.060635	No
54SB14B	3.00	4.3445926	20.12	77.060635	No
54SB6B	3.41	4.3445926	30.14	77.060635	No
54SB10B	2.89	4.3445926	18.01	77.060635	No
54SB11B	2.94	4.3445926	18.89	77.060635	No
54SB12B	3.27	4.3445926	26.43	77.060635	No
54SB2B	2.81	4.3445926	16.69	77.060635	No
54SB3B	2.33	4.3445926	10.26	77.060635	No
54SB4B	2.22	4.3445926	9.19	77.060635	No
54SB5B	3.20	4.3445926	24.46	77.060635	No
54SB7B	3.55	4.3445926	34.72	77.060635	No
54SB8B	3.24	4.3445926	25.56	77.060635	No
54SB9B	3.12	4.3445926	22.61	77.060635	No
54SB10D	2.74	4.3445926	15.45	77.060635	No
54SB13B	2.58	4.3445926	13.20	77.060635	No
54SB1B	1.83	4.3445926	6.23	77.060635	No
54SB16D	3.19	4.3445926	24.25	77.060635	No

ATTACHMENT 4

REVISED APPENDIX H OF THE

DRAFT RCRA FACILITY INVESTIGATION (RFI) REPORT FOR

SOLID WASTE MANAGEMENT UNITS 17, 31, 48, AND 54

RADFORD ARMY AMMUNITION PLANT

APPENDIX H
SUMMARY STATISTICS FOR BACKGROUND DISTRIBUTIONS

**SUMMARY STATISTICS
FOR
BACKGROUND DISTRIBUTIONS**

Background, Urban Complex Soil Type

Soil Type	Urban Complex		Urban Complex		Urban Complex		Urban Complex		Urban Complex	
Soil Horizon	B	C	B	C	B	C	B	C	B	C
Metal	Antimony		Arsenic		Barium		Beryllium		Cadmium	
Mean	12.62	12.67	6.89	5.46	110.31	97.76	1.33	2.30	0.78	0.78
Standard Error	0.60	0.42	1.85	1.24	35.00	16.18	0.22	0.41	0.04	0.03
Median	12.07	12.50	6.38	6.23	68.74	83.64	1.37	2.36	0.74	0.77
Standard Deviation	1.71	1.19	5.24	3.50	98.99	45.75	0.61	1.17	0.10	0.07
Sample Variance	2.92	1.42	27.42	12.27	9798.59	2093.11	0.37	1.37	0.01	0.01
Kurtosis	-0.44	0.49	-1.93	-2.05	0.06	5.74	1.26	-1.17	-0.53	0.54
Skewness	0.71	0.11	0.23	-0.21	1.30	2.30	-0.25	0.13	0.74	0.09
Range	4.86	3.95	13.09	8.32	255.47	142.60	2.10	3.28	0.29	0.24
Minimum	10.34	10.72	1.32	1.37	31.44	62.63	0.23	0.82	0.64	0.66
Maximum	15.20	14.67	14.41	9.69	286.91	205.22	2.33	4.10	0.93	0.90
Sum	100.94	101.34	55.13	43.70	882.51	782.09	10.67	18.39	6.20	6.23
Count	8	8	8	8	8	8	8	8	8	8
Confidence Level(95.000%)	1.19	0.83	3.63	2.43	68.59	31.70	0.42	0.81	0.07	0.05

Background, Urban Complex Soil Type

Soil Type	Urban Complex		Urban Complex		Urban Complex		Urban Complex		Urban Complex	
Soil Horizon	B	C	B	C	B	C	B	C	B	C
Metal	Chromium		Lead		Mercury		Nickel		Selenium	
Mean	46.43	46.85	46.97	15.69	0.10	0.08	21.98	32.87	0.29	0.29
Standard Error	3.35	3.11	26.03	1.78	0.03	0.03	3.21	4.07	0.01	0.01
Median	48.41	49.04	21.63	14.31	0.04	0.04	24.06	37.10	0.28	0.29
Standard Deviation	9.48	8.78	73.63	5.03	0.09	0.08	9.08	11.52	0.04	0.03
Sample Variance	89.79	77.16	5421.13	25.26	0.01	0.01	82.37	132.64	0.00	0.00
Kurtosis	-0.83	-0.35	7.72	0.09	-1.95	0.45	0.11	-0.97	-0.54	0.28
Skewness	-0.46	-0.71	2.76	0.83	0.71	1.50	-0.97	-0.63	0.66	0.25
Range	27.41	25.97	222.89	15.27	0.18	0.20	25.08	30.85	0.11	0.09
Minimum	30.70	31.29	5.20	9.63	0.03	0.03	5.15	16.19	0.24	0.25
Maximum	58.10	57.26	228.09	24.90	0.21	0.23	30.23	47.04	0.35	0.34
Sum	371.44	374.78	375.78	125.48	0.76	0.63	175.85	262.93	2.34	2.34
Count	8	8	8	8	8	8	8	8	8	8
Confidence Level(95.000%)	6.57	6.09	51.02	3.48	0.06	0.06	6.29	7.98	0.03	0.02

Background, Urban Complex Soil Type

Soil Type	Urban Complex		Urban Complex	
Soil Horizon	B	C	B	C
Metal	Silver		Thallium	
Mean	0.02	0.03	22.08	22.17
Standard Error	0.01	0.01	1.06	0.74
Median	0.01	0.01	21.13	21.88
Standard Deviation	0.03	0.03	2.99	2.08
Sample Variance	0.00	0.00	8.96	4.34
Kurtosis	2.15	-0.01	-0.44	0.49
Skewness	1.76	1.43	0.71	0.12
Range	0.08	0.08	8.50	6.91
Minimum	0.01	0.01	18.09	18.77
Maximum	0.08	0.08	26.59	25.68
Sum	0.18	0.22	176.62	177.36
Count	8	8	8	8
Confidence Level(95.000%)	0.02	0.02	2.07	1.44

Background, Wheeling Loam Soil Type

Soil Type	Wheeling Loam		Wheeling Loam		Wheeling Loam		Wheeling Loam		Wheeling Loam	
Soil Horizon	B	C	B	C	B	C	B	C	B	C
Metal	Antimony		Arsenic		Barium		Beryllium		Cadmium	
Mean	11.78	11.55	2.31	2.38	147.20	98.82	1.30	0.94	0.72	0.70
Standard Error	0.09	0.23	0.52	0.59	18.41	16.72	0.15	0.12	0.01	0.02
Median	11.77	11.83	1.51	1.53	155.26	90.51	1.51	0.87	0.72	0.73
Standard Deviation	0.22	0.55	1.27	1.45	45.09	40.95	0.37	0.29	0.01	0.05
Sample Variance	0.05	0.30	1.60	2.10	2032.89	1677.24	0.14	0.09	0.00	0.00
Kurtosis	1.85	-0.75	-1.60	0.09	-1.08	3.05	-0.18	4.43	1.33	-0.80
Skewness	-0.37	-1.09	1.01	1.29	-0.57	1.52	-1.23	1.96	-0.44	-1.07
Range	0.67	1.33	2.68	3.46	115.72	119.34	0.89	0.84	0.04	0.11
Minimum	11.42	10.67	1.46	1.36	79.72	55.63	0.69	0.67	0.70	0.63
Maximum	12.09	12.00	4.14	4.82	195.44	174.97	1.58	1.51	0.74	0.74
Sum	70.65	69.27	13.85	14.26	883.22	592.90	7.83	5.62	4.33	4.21
Count	6	6	6	6	6	6	6	6	6	6
Confidence Level(95.000%)	0.17	0.44	1.01	1.16	36.08	32.77	0.30	0.23	0.01	0.04

Background, Wheeling Loam Soil Type

Soil Type	Wheeling Loam		Wheeling Loam		Wheeling Loam		Wheeling Loam		Wheeling Loam	
Soil Horizon	B	C	B	C	B	C	B	C	B	C
Metal	Chromium		Lead		Mercury		Nickel		Selenium	
Mean	43.76	35.60	19.17	16.36	0.04	0.05	20.86	15.57	0.27	0.27
Standard Error	3.64	3.17	2.46	1.70	0.01	0.01	2.96	2.48	0.00	0.00
Median	45.96	35.95	21.48	15.99	0.03	0.03	23.83	14.02	0.27	0.27
Standard Deviation	8.91	7.75	6.02	4.18	0.02	0.03	7.25	6.09	0.01	0.01
Sample Variance	79.41	60.14	36.27	17.44	0.00	0.00	52.60	37.04	0.00	0.00
Kurtosis	-1.70	-0.32	-1.97	0.44	6.00	-1.65	-1.76	4.23	2.50	-0.45
Skewness	-0.28	0.43	-0.67	0.46	2.45	1.01	-0.71	1.85	0.00	-0.67
Range	22.22	21.05	13.63	12.13	0.04	0.07	16.20	17.77	0.02	0.03
Minimum	32.63	26.58	11.31	10.83	0.03	0.03	10.56	9.57	0.26	0.25
Maximum	54.85	47.63	24.94	22.96	0.07	0.10	26.76	27.34	0.28	0.28
Sum	262.59	213.57	115.02	98.18	0.22	0.31	125.17	93.41	1.62	1.61
Count	6	6	6	6	6	6	6	6	6	6
Confidence Level(95.000%)	7.13	6.20	4.82	3.34	0.01	0.03	5.80	4.87	0.01	0.01

Background, Wheeling Loam Soil Type

Soil Type	Wheeling Loam		Wheeling Loam	
Soil Horizon	B	C	B	C
Metal	Silver		Thallium	
Mean	0.10	0.01	20.61	20.20
Standard Error	0.09	0.00	0.15	0.39
Median	0.01	0.01	20.60	20.69
Standard Deviation	0.22	0.00	0.38	0.97
Sample Variance	0.05	0.00	0.14	0.93
Kurtosis	6.00	-1.88	1.86	-0.72
Skewness	2.45	0.97	-0.39	-1.10
Range	0.55	0.01	1.16	2.33
Minimum	0.01	0.01	19.99	18.66
Maximum	0.55	0.01	21.15	20.99
Sum	0.59	0.04	123.64	121.19
Count	6	6	6	6
Confidence Level(95.000%)	0.18	0.00	0.30	0.77

Background, Braddock Loam Soil Type

Soil Type	Braddock Loam		Braddock Loam		Braddock Loam		Braddock Loam		Braddock Loam	
Soil Horizon	B	C	B	C	B	C	B	C	B	C
Metal	Antimony		Arsenic		Barium		Beryllium		Cadmium	
Mean	11.94	12.17	2.55	4.26	117.61	135.34	0.57	1.58	0.73	1.18
Standard Error	0.11	0.15	1.02	2.73	30.95	22.52	0.30	0.48	0.01	0.43
Median	11.91	12.17	1.55	1.55	93.24	126.83	0.27	1.81	0.73	0.75
Standard Deviation	0.22	0.30	2.05	5.45	61.89	45.04	0.60	0.96	0.02	0.86
Sample Variance	0.05	0.09	4.18	29.72	3830.75	2028.46	0.36	0.92	0.00	0.75
Kurtosis	-1.88	-3.38	4.00	4.00	3.55	1.97	4.00	0.67	-3.90	4.00
Skewness	0.55	0.06	2.00	2.00	1.86	1.06	2.00	-1.13	0.37	2.00
Range	0.49	0.65	4.12	10.93	134.72	107.28	1.21	2.16	0.03	1.74
Minimum	11.72	11.85	1.50	1.51	74.61	90.21	0.26	0.26	0.72	0.73
Maximum	12.21	12.50	5.62	12.44	209.33	197.48	1.47	2.42	0.75	2.47
Sum	47.74	48.68	10.21	17.05	470.42	541.34	2.26	6.30	2.93	4.70
Count	4	4	4	4	4	4	4	4	4	4
Confidence Level(95.000%)	0.22	0.29	2.00	5.34	60.65	44.14	0.59	0.94	0.01	0.85

Background, Braddock Loam Soil Type

Soil Type	Braddock Loam		Braddock Loam		Braddock Loam		Braddock Loam		Braddock Loam	
Soil Horizon	B	C	B	C	B	C	B	C	B	C
Metal	Chromium		Lead		Mercury		Nickel		Selenium	
Mean	42.41	43.15	17.08	24.07	0.05	0.07	12.59	26.42	0.28	0.28
Standard Error	2.28	4.05	2.93	6.64	0.02	0.02	1.16	5.69	0.00	0.00
Median	41.79	43.45	17.19	19.30	0.03	0.07	12.77	27.17	0.28	0.28
Standard Deviation	4.56	8.11	5.86	13.28	0.03	0.05	2.31	11.39	0.01	0.01
Sample Variance	20.82	65.70	34.40	176.28	0.00	0.00	5.34	129.69	0.00	0.00
Kurtosis	-3.64	0.41	-4.42	2.69	4.00	-6.00	-4.03	-5.66	-6.00	1.50
Skewness	0.38	-0.20	-0.05	1.65	2.00	0.00	-0.23	-0.06	0.00	0.00
Range	9.50	19.45	12.26	29.05	0.06	0.08	4.86	21.11	0.01	0.02
Minimum	38.28	33.13	10.85	14.32	0.03	0.03	9.98	15.11	0.27	0.27
Maximum	47.77	52.58	23.10	43.37	0.09	0.11	14.83	36.23	0.28	0.29
Sum	169.64	172.61	68.33	96.29	0.18	0.28	50.34	105.68	1.10	1.12
Count	4	4	4	4	4	4	4	4	4	4
Confidence Level(95.000%)	4.47	7.94	5.75	13.01	0.03	0.05	2.27	11.16	0.01	0.01

Background, Braddock Loam Soil Type

Soil Type	Braddock Loam		Braddock Loam	
Soil Horizon	B	C	B	C
Metal	Silver		Thallium	
Mean	0.01	0.01	20.89	21.30
Standard Error	0.00	0.00	0.19	0.26
Median	0.01	0.01	20.83	21.28
Standard Deviation	0.00	0.00	0.38	0.52
Sample Variance	0.00	0.00	0.15	0.27
Kurtosis	-6.00	NA	-2.10	-3.37
Skewness	0.00	NA	0.55	0.10
Range	0.01	0.00	0.84	1.14
Minimum	0.01	0.01	20.52	20.74
Maximum	0.01	0.01	21.36	21.88
Sum	0.03	0.04	83.54	85.18
Count	4	4	4	4
Confidence Level(95.000%)	0.00	NA	0.37	0.51

**POSITIVE RESULTS
FOR
BACKGROUND SAMPLES**

**POSITIVE RESULTS TABLE OF BACKGROUND SOIL SAMPLES
RADFORD ARMY AMMUNITION PLANT**

Field Sample Number	BG1BBL4	BG1BUC3	BG1BW15	BG1CBL10	BG1CUC8	BG1CWL8	BG2BBL5	BG2BBL5
METALS (ug/g)								
Arsenic		11.47			6.96	4.82		11.61
Lead	13.45 J1	21.32 J1	11.31 J1	14.32 J1	15.25 J1	16.81 J1	10.85 J1	27.90 J1
Silver		0.08 J9			0.08 J9			
Barium	97.88 J1	46.88 J1	144.07 J1	122.28 J1	73.00 J1	102.06 J1	88.60 J1	31.44 J1
Beryllium		1.42	1.53	1.49	2.92	0.91		0.99
Cadmium								
Chromium	38.98 J1	50.75 J1	43.10 J1	41.49 J1	57.26 J1	37.97 J1	44.61 J1	51.54 J1
Nickel	9.98	30.17	21.07	18.12	36.32	13.78	11.34	13.36
Mercury		0.21			0.23	0.10	0.09	0.17
OTHER								
Total Organic Carbon (ug/g)	4246.58	1246.88		1223.99				
pH	5.49	4.67		5.47				

**POSITIVE RESULTS TABLE OF BACKGROUND SOIL SAMPLES
RADFORD ARMY AMMUNITION PLANT**

Field Sample Number	BG2BWL4	BG2CBL17	BG2CUC11	BG2CWL12	BG3BBL3	BG3BUC3	BG3BWL3	BG3CBL22
METALS (ug/g)								
Arsenic		12.44	9.69			14.41		
Lead	12.14 J1	43.37 J1	20.03 J1	15.18 J1	20.93 J1	228.09 J1	23.19 J1	16.48 J1
Silver						0.05	0.55	
Barium	110.70 J1	131.38 J1	85.20 J1	80.78 J1	209.33 J1	286.92 J1	79.72 J1	197.48 J1
Beryllium	1.00	2.42	3.33	0.84	1.47	1.81	0.69	2.13
Cadmium		2.47						
Chromium	34.01 J1	45.41 J1	47.96 J1	39.17 J1	38.28	58.10	32.63 J1	52.58
Nickel	13.46	36.22	38.01	9.57	14.83	22.81	10.56	36.23
Mercury		0.11	0.19	0.09			0.07	
OTHER								
Total Organic Carbon (ug/g)		1275.51						
pH		5.97						

**POSITIVE RESULTS TABLE OF BACKGROUND SOIL SAMPLES
RADFORD ARMY AMMUNITION PLANT**

Field Sample Number	BG3CUC22	BG3CWL22	BG4BBL5	BG4BBLD*	BG4BUC5	BG4BWL4	BG4CBL10	BG4CUC17
METALS (ug/g)								
Arsenic			5.62	5.47	4.34	3.73		
Lead	11.82 J1	10.83 J1	23.10 J1	17.60 J1	20.44 J1	24.94 J1	22.13 J1	18.03 J1
Silver								
Barium	107.99 J1	100.24 J1	74.61 J1	76.65 J1	244.53 J1	195.44 J1	90.21 J1	205.22 J1
Beryllium	0.82	0.89			1.46	1.49		1.58
Cadmium								
Chromium	31.29	33.94 J1	47.77	42.04	55.96	49.16	33.13	50.12
Nickel	16.19	15.28	14.20	14.61	25.30	26.74	15.11	28.36
Mercury				0.19			0.11	
OTHER								
Total Organic Carbon (ug/g)		1203.37	2250.30	14610.80				1666.67
pH		6.93	7.33	7.13				7.49

* BG4BBLD is a duplicate sample of BG4BBL5

**POSITIVE RESULTS TABLE OF BACKGROUND SOIL SAMPLES
RADFORD ARMY AMMUNITION PLANT**

Field Sample Number	BG4CUCD*	BG4CWL17	BG5BUC3	BG5BWL3	BG5CUC8	BG5CWL8	BG5CWLD*	BG6BUC5
METALS (ug/g)								
Arsenic					8.10			8.42
Lead	19.24 J1	13.82 J1	5.20 J1	19.76 J1	24.90 J1	22.96 J1	22.37 J1	33.18 J1
Silver								
Barium	144.95 J1	79.22 J1	36.18 J1	186.83 J1	82.08 J1	174.97 J1	175.33 J1	62.95 J1
Beryllium	1.50	0.80		1.56	1.96	1.51	1.46	1.31
Cadmium								
Chromium	53.11	28.29	30.70 J1	54.85	54.45 J1	47.63	48.85	40.47 J1
Nickel	26.43	14.25	5.15	26.59	42.68	27.34	27.93	30.23
Mercury								0.21
OTHER								
Total Organic Carbon (ug/g)	1778.32			3365.27		1980.56		
pH	7.51			6.99		6.21		

* BG4CUCD is a duplicate sample of BG4CUC17

* BG5CWLD is a duplicate sample of BG5CWL8

**POSITIVE RESULTS TABLE OF BACKGROUND SOIL SAMPLES
RADFORD ARMY AMMUNITION PLANT**

Field Sample Number	BG6BWL4	BG6CUC12	BG6CWL17	BG7BUC5	BG7CUC22	BG8BUC5	BG8CUC10
METALS (ug/g)							
Arsenic	4.14	8.92	3.52		5.50		
Lead	23.67 J1	12.46 J1	18.58 J1	17.72 J1	13.37 J1	21.93 J1	9.63 J1
Silver							0.08 J9
Barium	166.46 J1	70.51 J1	55.63 J1	99.08 J1	95.46 J1	74.54 J1	62.63 J1
Beryllium	1.58	2.75	0.67	2.33	4.10	1.11	0.94
Cadmium							
Chromium	48.83	41.47 J1	26.58	46.07 J1	52.82 J1	37.86 J1	39.41 J1
Nickel	26.76	37.87	13.18	29.89	47.04	18.93	16.45
Mercury							
OTHER							
Total Organic Carbon (ug/g)	2157.83					1305.48	1275.51
pH	7.03					5.08	5.09

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**SUMMARY OF TOLERANCE LIMITS
RADFORD ARMY AMMUNITION PLANT**

Soil Horizon	Soil Series	Constituent	Upper	Tolerance	Exceedance?
			Limit	Limit Type	
SWMU 17A	B	Antimony	21.0	Poisson	Yes
SWMU 17A	B	Arsenic	5.5	Poisson	Yes
SWMU 17A	B	Barium	9.7	Normal	No
SWMU 17A	B	Beryllium	4.5	Poisson	No
SWMU 17A	B	Cadmium	3.5	Poisson	Yes
SWMU 17A	B	Chromium	5.1	Normal	Yes
SWMU 17A	B	Lead	8.7	Normal	No
SWMU 17A	B	Mercury	1.5	Poisson	No
SWMU 17A	B	Nickel	6.0	Normal	Yes
SWMU 17A	B	Selenium	2.5	Poisson	No
SWMU 17A	B	Silver	1.5	Poisson	Yes
SWMU 17A	B	Thallium	33.5	Poisson	No
SWMU 17A	C	Antimony	21.5	Poisson	No
SWMU 17A	C	Arsenic	11.5	Poisson	Yes
SWMU 17A	C	Barium	6.9	Normal	No
SWMU 17A	C	Beryllium	2.7	Normal	No
SWMU 17A	C	Cadmium	3.5	Poisson	No
SWMU 17A	C	Chromium	5.0	Normal	No
SWMU 17A	C	Lead	4.2	Normal	Yes
SWMU 17A	C	Mercury	1.5	Poisson	No
SWMU 17A	C	Nickel	5.4	Normal	No
SWMU 17A	C	Selenium	2.5	Poisson	No
SWMU 17A	C	Silver	1.5	Poisson	Yes
SWMU 17A	C	Thallium	33.5	Poisson	No
SWMU 17BCD	B	Antimony	21.0	Poisson	No
SWMU 17BCD	B	Arsenic	5.5	Poisson	Yes
SWMU 17BCD	B	Barium	9.7	Normal	No
SWMU 17BCD	B	Beryllium	4.5	Poisson	No
SWMU 17BCD	B	Cadmium	3.5	Poisson	No
SWMU 17BCD	B	Chromium	5.1	Normal	No
SWMU 17BCD	B	Lead	8.7	Normal	No
SWMU 17BCD	B	Mercury	1.5	Poisson	No
SWMU 17BCD	B	Nickel	6.0	Normal	No
SWMU 17BCD	B	Selenium	2.5	Poisson	No
SWMU 17BCD	B	Silver	1.5	Poisson	No
SWMU 17BCD	B	Thallium	33.5	Poisson	No
SWMU 17BCD	C	Antimony	21.5	Poisson	No
SWMU 17BCD	C	Arsenic	11.5	Poisson	No
SWMU 17BCD	C	Barium	6.9	Normal	No
SWMU 17BCD	C	Beryllium	2.3	Normal	Yes
SWMU 17BCD	C	Cadmium	3.5	Poisson	Yes
SWMU 17BCD	C	Chromium	5.0	Normal	No
SWMU 17BCD	C	Lead	4.2	Normal	Yes
SWMU 17BCD	C	Mercury	1.5	Poisson	No
SWMU 17BCD	C	Nickel	5.4	Normal	No
SWMU 17BCD	C	Selenium	2.5	Poisson	No
SWMU 17BCD	C	Silver	1.5	Poisson	No
SWMU 17BCD	C	Thallium	33.5	Poisson	No

**SUMMARY OF TOLERANCE LIMITS
RADFORD ARMY AMMUNITION PLANT**

Soil Horizon	Soil Series	Constituent	Upper	Tolerance	Exceedance?
			Tolerance Limit		
SWMU 31	C	Antimony	20.5	Poisson	No
SWMU 31	C	Arsenic	7.0	Poisson	No
SWMU 31	C	Barium	7.1	Normal	No
SWMU 31	C	Beryllium	.5	Normal	No
SWMU 31	C	Cadmium	3.5	Poisson	No
SWMU 31	C	Chromium	4.8	Normal	No
SWMU 31	C	Lead	4.1	Normal	No
SWMU 31	C	Mercury	2.0	Poisson	No
SWMU 31	C	Nickel	4.3	Normal	No
SWMU 31	C	Selenium	2.5	Poisson	No
SWMU 31	C	Silver	1.5	Poisson	No
SWMU 31	C	Thallium	31.5	Poisson	No
SWMU 54	B	Antimony	20.5	Poisson	No
SWMU 54	B	Arsenic	6.5	Poisson	No
SWMU 54	B	Barium	7.4	Normal	No
SWMU 54	B	Beryllium	5.0	Poisson	No
SWMU 54	B	Cadmium	3.5	Poisson	Yes
SWMU 54	B	Chromium	5.0	Normal	No
SWMU 54	B	Lead	4.7	Normal	Yes
SWMU 54	B	Mercury	1.5	Poisson	Yes
SWMU 54	B	Nickel	5.0	Normal	No
SWMU 54	B	Selenium	2.5	Poisson	No
SWMU 54	B	Silver	2.0	Poisson	No
SWMU 54	B	Thallium	32.0	Poisson	No
SWMU 54	C	Antimony	20.5	Poisson	No
SWMU 54	C	Arsenic	7.0	Poisson	No
SWMU 54	C	Barium	7.1	Normal	No
SWMU 54	C	Beryllium	.5	Normal	Yes
SWMU 54	C	Cadmium	3.5	Poisson	No
SWMU 54	C	Chromium	4.8	Normal	No
SWMU 54	C	Lead	4.1	Normal	Yes
SWMU 54	C	Mercury	2.0	Poisson	No
SWMU 54	C	Nickel	4.3	Normal	No
SWMU 54	C	Selenium	2.5	Poisson	No
SWMU 54	C	Silver	1.5	Poisson	No
SWMU 54	C	Thallium	31.5	Poisson	No

SHAPIRO-WILK GOODNESS OF FIT TEST
UNISON-URBAN LAND COMPLEX SOIL TYPE
FOR SMWU 17A, 17BCD

Arsenic soil B

SHAPIRO-WILK GOODNESS OF FIT TEST

1. Order samples from smallest to largest in column x(i)
2. Order samples from largest to smallest in column x(n-i+1)
3. Compute K as the greatest integer less than or equal to N/2. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column a(n-i+1).
5. Sum the values in column b(i) and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W, the distribution is non-normal. Transform and re-test.

i	x(i)	x(n-i+1)	x(n-i+1)-x(i)	a(n-i+1)	b(i)
1	1.47	2.67	1.20004806	0.6646	0.7975519
2	2.13	2.45	0.32125697	0.2413	0.0775193
3	2.44	2.44	0	0	0
4	2.45	2.13	-0.32125697	0	0
5	2.67	1.47	-1.20004806		0
					0.8750712

std dev = 0.4678917

N = 5

K = 2

b = 0.8750712

W = 0.8744522

Critical W = 0.762

Result = Lognormally transformed data meets assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST

1. Order samples from smallest to largest in column x(i)
2. Order samples from largest to smallest in column x(n-i+1)
3. Compute K as the greatest integer less than or equal to N/2. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column a(n-i+1).
5. Sum the values in column b(i) and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W, the distribution is non-normal. Transform and re-test.

i	x(i)	x(n-i+1)	x(n-i+1)-x(i)	a(n-i+1)	b(i)
1	0.31	2.27	1.95628369	0.6052	1.1839429
2	0.44	2.19	1.74361013	0.3164	0.5516782
3	0.47	2.09	1.62	0.1743	0.2826903
4	1.70	1.94	0.24	0.0561	0.0132077
5	1.94	1.70			2.0315191
6	2.09	0.47			
7	2.19	0.44			
8	2.27	0.31			

std dev = 0.6510165

N = 8

K = 4

b = 2.0315191

W = 1.3911045

Critical W = 0.748

Result = Lognormally transformed data meets assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST

1. Order samples from smallest to largest in column x(i)
2. Order samples from largest to smallest in column x(n-i+1)
3. Compute K as the greatest integer less than or equal to N/2. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column a(n-i+1).
5. Sum the values in column b(i) and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W, the distribution is non-normal. Transform and re-test.

i	x(i)	x(n-i+1)	x(n-i+1)-x(i)	a(n-i+1)	b(i)
1	3.45	5.66	2.21103812	0.6052	1.3381203
2	3.59	5.50	1.91077368	0.3164	0.6045688
3	3.85	4.60	0.74823143	0.1743	0.1304167
4	4.14	4.31	0.1691042	0.0561	0.0094867
5	4.31	4.14	-0.1691042		0
6	4.60	3.85	-0.74823143		0
7	5.50	3.59			2.0825925
8	5.66	3.45			

std dev = 0.825904

N = 8

K = 4

b = 2.0825925

W = 0.9083463

Critical W = 0.818

Result = Lognormally transformed data meets assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST ON UNTRANSFORMED DATA

1. Order samples from smallest to largest in column $x(i)$
2. Order samples from largest to smallest in column $x(n-i+1)$
3. Compute K as the greatest integer less than or equal to $N/2$. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column $a(n-i+1)$.
5. Sum the values in column $b(i)$ and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W , the distribution is non-normal. Transform and re-test.

i	$x(i)$	$x(n-i+1)$	$x(n-i+1)-x(i)$	$a(n-i+1)$	$b(i)$
1	31.44	286.91	255.472706	0.6052	154.61208
2	36.18	244.53	208.344111	0.3164	65.920077
3	46.88	99.08	52.1927007	0.1743	9.0971877
4	62.95	74.54	11.5973445	0.0561	0.650611
5	74.54	62.95	-11.5973445		0
6	99.08	46.88	-52.1927007		0
7	244.53	36.18			230.27996
8	286.91	31.44			

std dev = 98.987826

N = 8

K = 4

b = 230.27996

W = 0.7731267

Critical W = 0.818

Result = Untransformed data does not meet assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST

1. Order samples from smallest to largest in column $x(i)$
2. Order samples from largest to smallest in column $x(n-i+1)$
3. Compute K as the greatest integer less than or equal to $N/2$. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column $a(n-i+1)$.
5. Sum the values in column $b(i)$ and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W , the distribution is non-normal. Transform and re-test.

i	$x(i)$	$x(n-i+1)$	$x(n-i+1)-x(i)$	$a(n-i+1)$	$b(i)$
1	4.14	5.32	1.18689622	0.6052	0.7183096
2	4.26	4.68	0.43	0.3164	0.1348717
3	4.29	4.56	0.39151697	0.1743	0.0682414
4	4.41	4.45	0.1510293	0.0561	0.0084727
5	4.45	4.41	0		0
6	4.56	4.29	-0.1510293		0
7	4.68	4.26	-0.39151697		0.9298954
8	5.32	4.14	-1.18689622		

std dev = 0.3705519
 N = 8
 K = 4
 b = 0.9298954
 W = 0.8996471
 Critical W = 0.818
 Result = Lognormally transformed data meets assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST ON UNTRANSFORMED DATA

1. Order samples from smallest to largest in column $x(i)$
2. Order samples from largest to smallest in column $x(n-i+1)$
3. Compute K as the greatest integer less than or equal to $N/2$. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column $a(n-i+1)$.
5. Sum the values in column $b(i)$ and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W , the distribution is non-normal. Transform and re-test.

i	$x(i)$	$x(n-i+1)$	$x(n-i+1)-x(i)$	$a(n-i+1)$	$b(i)$
1	62.63	205.22	142.596332	0.6052	86.2993
2	70.51	107.99	37.48	0.3164	11.858004
3	73.00	95.46	34.9844433	0.1743	6.0977885
4	82.08	85.20	13.381456	0.0561	0.7506997
5	85.20	82.08	0		0
6	95.46	73.00	-13.381456		0
7	107.99	70.51	-34.9844433		105.00579
8	205.22	62.63	-142.596332		

std dev = 45.750472
 N = 8
 K = 4
 b = 105.00579
 W = 0.7525534
 Critical W = 0.818
 Result = Untransformed data does not meet assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST

1. Order samples from smallest to largest in column $x(i)$
2. Order samples from largest to smallest in column $x(n-i+1)$
3. Compute K as the greatest integer less than or equal to $N/2$. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column $a(n-i+1)$.
5. Sum the values in column $b(i)$ and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W , the distribution is non-normal. Transform and re-test.

i	$x(i)$	$x(n-i+1)$	$x(n-i+1)-x(i)$	$a(n-i+1)$	$b(i)$
1	-1.47	0.84	2.31410815	0.6052	1.4004983
2	-0.01	0.59	0.60433255	0.3164	0.1912108
3	0.11	0.38	0.27193205	0.1743	0.0473978
4	0.27	0.35	0.08040585	0.0561	0.0045108
5	0.35	0.27	-0.08040585		0
6	0.38	0.11	-0.27193205		0
7	0.59	-0.01			1.6436176
8	0.84	-1.47			

std dev = 0.7006256

N = 8

K = 4

b = 1.6436176

W = 0.7861973

Critical W = 0.818

Result = Lognormally transformed data does not meet assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST ON UNTRANSFORMED DATA

1. Order samples from smallest to largest in column $x(i)$
2. Order samples from largest to smallest in column $x(n-i+1)$
3. Compute K as the greatest integer less than or equal to $N/2$. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column $a(n-i+1)$.
5. Sum the values in column $b(i)$ and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W , the distribution is non-normal. Transform and re-test.

i	$x(i)$	$x(n-i+1)$	$x(n-i+1)-x(i)$	$a(n-i+1)$	$b(i)$
1	0.23	2.33	2.09665633	0.6052	1.2688964
2	0.99	1.81	0.82218136	0.3164	0.2601382
3	1.11	1.46	0.34758245	0.1743	0.0605836
4	1.31	1.42	0.10981842	0.0561	0.0061608
5	1.42	1.31	-0.10981842		0
6	1.46	1.11	-0.34758245		0
7	1.81	0.99			1.595779
8	2.33	0.23			

std dev = 0.6123102
 N = 8
 K = 4
 b = 1.595779
 W = 0.9702964
 Critical W = 0.818
 Result = Untransformed data meets assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST

1. Order samples from smallest to largest in column $x(i)$
2. Order samples from largest to smallest in column $x(n-i+1)$
3. Compute K as the greatest integer less than or equal to $N/2$. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring.
Put into column $a(n-i+1)$.
5. Sum the values in column $b(i)$ and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W , the distribution is non-normal. Transform and re-test.

i	$x(i)$	$x(n-i+1)$	$x(n-i+1)-x(i)$	$a(n-i+1)$	$b(i)$
1	-0.20	1.41	1.61117965	0.6052	0.9750859
2	-0.06	1.20	1.26587534	0.3164	0.400523
3	0.46	1.07	0.61	0.1743	0.106953
4	0.67	1.01	0.55605981	0.0561	0.031195
5	1.01	0.67	0		0
6	1.07	0.46	-0.55605981		0
7	1.20	-0.06	-1.13396618		1.5137568
8	1.41	-0.20	-1.403124		

std dev = 0.5911619
 N = 8
 K = 4
 b = 1.5137568
 W = 0.9367016
 Critical W = 0.818
 Result = Lognormally transformed data meets assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST ON UNTRANSFORMED DATA

1. Order samples from smallest to largest in column $x(i)$
2. Order samples from largest to smallest in column $x(n-i+1)$
3. Compute K as the greatest integer less than or equal to $N/2$. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column $a(n-i+1)$.
5. Sum the values in column $b(i)$ and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W , the distribution is non-normal. Transform and re-test.

i	$x(i)$	$x(n-i+1)$	$x(n-i+1)-x(i)$	$a(n-i+1)$	$b(i)$
1	0.82	4.10	3.28065635	0.6052	1.9854532
2	0.94	3.33	2.390306	0.3164	0.7562928
3	1.58	2.92	1.34	0.1743	0.2332262
4	1.96	2.75	1.17488913	0.0561	0.0659113
5	2.75	1.96	0		0
6	2.92	1.58	-1.17488913		0
7	3.33	0.94	-1.97890012		3.0408836
8	4.10	0.82	-2.51070074		

std dev = 1.169182
 N = 8
 K = 4
 b = 3.0408836
 W = 0.9663564
 Critical W = 0.818
 Result = Untransformed data meets assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST

1. Order samples from smallest to largest in column $x(i)$
2. Order samples from largest to smallest in column $x(n-i+1)$
3. Compute K as the greatest integer less than or equal to $N/2$. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring.
Put into column $a(n-i+1)$.
5. Sum the values in column $b(i)$ and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W , the distribution is non-normal. Transform and re-test.

i	$x(i)$	$x(n-i+1)$	$x(n-i+1)-x(i)$	$a(n-i+1)$	$b(i)$
1	3.42	4.06	0.63808253	0.6052	0.3861675
2	3.63	4.02	0.39078734	0.3164	0.1236451
3	3.70	3.94	0.2418529	0.1743	0.042155
4	3.83	3.93	0.09669377	0.0561	0.0054245
5	3.93	3.83	-0.09669377		0
6	3.94	3.70	-0.2418529		0
7	4.02	3.63			0.5573921
8	4.06	3.42			

std dev = 0.217995

N = 8

K = 4

b = 0.5573921

W = 0.9339647

Critical W = 0.818

Result = Lognormally transformed data meets assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST ON UNTRANSFORMED DATA

1. Order samples from smallest to largest in column $x(i)$
2. Order samples from largest to smallest in column $x(n-i+1)$
3. Compute K as the greatest integer less than or equal to $N/2$. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column $a(n-i+1)$.
5. Sum the values in column $b(i)$ and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W , the distribution is non-normal. Transform and re-test.

i	$x(i)$	$x(n-i+1)$	$x(n-i+1)-x(i)$	$a(n-i+1)$	$b(i)$
1	30.70	58.10	27.4070408	0.6052	16.586741
2	37.86	55.96	18.1020624	0.3164	5.7274925
3	40.47	51.54	11.0715316	0.1743	1.929768
4	46.07	50.75	4.67725354	0.0561	0.2623939
5	50.75	46.07	-4.67725354		0
6	51.54	40.47	-11.0715316		0
7	55.96	37.86	-18.1020624		24.506396
8	58.10	30.70	-27.4070408		

std dev = 9.4759327
 N = 8
 K = 4
 b = 24.506396
 W = 0.9554697
 Critical W = 0.818
 Result = Untransformed data meets assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST

1. Order samples from smallest to largest in column $x(i)$
2. Order samples from largest to smallest in column $x(n-i+1)$
3. Compute K as the greatest integer less than or equal to $N/2$. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column $a(n-i+1)$.
5. Sum the values in column $b(i)$ and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W , the distribution is non-normal. Transform and re-test.

i	$x(i)$	$x(n-i+1)$	$x(n-i+1)-x(i)$	$a(n-i+1)$	$b(i)$
1	3.44	4.05	0.6043394	0.6052	0.3657462
2	3.67	4.00	0.32310627	0.3164	0.1022308
3	3.72	3.97	0.24738981	0.1743	0.04312
4	3.87	3.91	0.04	0.0561	0.0024772
5	3.91	3.87	-0.04		0
6	3.97	3.72	-0.25		0
7	4.00	3.67	-0.32		0.5135743
8	4.05	3.44	-0.60		

std dev = 0.2032647

N = 8

K = 4

b = 0.5135743

W = 0.9119788

Critical W = 0.818

Result = Lognormally transformed data meets assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST ON UNTRANSFORMED DATA

1. Order samples from smallest to largest in column $x(i)$
2. Order samples from largest to smallest in column $x(n-i+1)$
3. Compute K as the greatest integer less than or equal to $N/2$. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column $a(n-i+1)$.
5. Sum the values in column $b(i)$ and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W , the distribution is non-normal. Transform and re-test.

i	$x(i)$	$x(n-i+1)$	$x(n-i+1)-x(i)$	$a(n-i+1)$	$b(i)$
1	31.29	57.26	25.9728944	0.6052	15.718796
2	39.41	54.45	15.0326981	0.3164	4.7563457
3	41.47	52.82	11.3527362	0.1743	1.9787819
4	47.96	50.12	2.17	0.0561	0.1214677
5	50.12	47.96	-2.17		0
6	52.82	41.47	-11.35		0
7	54.45	39.41	-15.03		22.575391
8	57.26	31.29	-25.97		

std dev = 8.7839255
 N = 8
 K = 4
 b = 22.575391
 W = 0.9436159
 Critical W = 0.818
 Result = Untransformed data meets assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST

1. Order samples from smallest to largest in column x(i)
2. Order samples from largest to smallest in column x(n-i+1)
3. Compute K as the greatest integer less than or equal to N/2. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column a(n-i+1).
5. Sum the values in column b(i) and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W, the distribution is non-normal. Transform and re-test.

i	x(i)	x(n-i+1)	x(n-i+1)-x(i)	a(n-i+1)	b(i)
1	1.65	5.43	3.78100599	0.6052	2.2882648
2	2.87	3.50	0.62722638	0.3164	0.1984544
3	3.02	3.33	0.31108885	0.1743	0.0542228
4	3.06	3.09	0.0282268	0.0561	0.0015835
5	3.09	3.06	-0.0282268		0
6	3.33	3.02	-0.31108885		0
7	3.50	2.87	-0.62722638		2.5425256
8	5.43	1.65	-3.78100599		

std dev = 1.0448547

N = 8

K = 4

b = 2.5425256

W = 0.8459035

Critical W = 0.818

Result = Lognormally transformed data meets assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST ON UNTRANSFORMED DATA

1. Order samples from smallest to largest in column x(i)
2. Order samples from largest to smallest in column x(n-i+1)
3. Compute K as the greatest integer less than or equal to N/2. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column a(n-i+1).
5. Sum the values in column b(i) and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W, the distribution is non-normal. Transform and re-test.

i	x(i)	x(n-i+1)	x(n-i+1)-x(i)	a(n-i+1)	b(i)
1	30.70	58.10	27.4070408	0.6052	16.586741
2	37.86	55.96	18.1020624	0.3164	5.7274925
3	40.47	51.54	11.0715316	0.1743	1.929768
4	46.07	50.75	4.67725354	0.0561	0.2623939
5	50.75	46.07	-4.67725354		0
6	51.54	40.47	-11.0715316		0
7	55.96	37.86	-18.1020624		24.506396
8	58.10	30.70	-27.4070408		

std dev = 9.4759327
 N = 8
 K = 4
 b = 24.506396
 W = 0.9554697
 Critical W = 0.818
 Result = Untransformed data meets assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST

1. Order samples from smallest to largest in column $x(i)$
2. Order samples from largest to smallest in column $x(n-i+1)$
3. Compute K as the greatest integer less than or equal to $N/2$. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column $a(n-i+1)$.
5. Sum the values in column $b(i)$ and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W , the distribution is non-normal. Transform and re-test.

i	$x(i)$	$x(n-i+1)$	$x(n-i+1)-x(i)$	$a(n-i+1)$	$b(i)$
1	2.26	3.21	0.9498696	0.6052	0.5748611
2	2.47	3.00	0.52753616	0.3164	0.1669124
3	2.52	2.89	0.37	0.1743	0.0645216
4	2.59	2.72	0.13	0.0561	0.0073964
5	2.72	2.59	-0.13		0
6	2.89	2.52	-0.37		0
7	3.00	2.47	-0.53		0.8136915
8	3.21	2.26	-0.95		

std dev = 0.3106604

N = 8

K = 4

b = 0.8136915

W = 0.980053

Critical W = 0.818

Result = Lognormally transformed data meets assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST

1. Order samples from smallest to largest in column $x(i)$
2. Order samples from largest to smallest in column $x(n-i+1)$
3. Compute K as the greatest integer less than or equal to $N/2$. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column $a(n-i+1)$.
5. Sum the values in column $b(i)$ and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W , the distribution is non-normal. Transform and re-test.

i	$x(i)$	$x(n-i+1)$	$x(n-i+1)-x(i)$	$a(n-i+1)$	$b(i)$
1	31.29	57.26	25.9728944	0.6052	15.718796
2	39.41	54.45	15.0326981	0.3164	4.7563457
3	41.47	52.82	11.35	0.1743	1.9787819
4	47.96	50.12	2.17	0.0561	0.1214677
5	50.12	47.96	-2.17		0
6	52.82	41.47	-11.35		0
7	54.45	39.41	-15.03		22.575391
8	57.26	31.29	-25.97		

std dev = 8.7839255
 N = 8
 K = 4
 b = 22.575391
 W = 0.9436159
 Critical W = 0.818
 Result = Untransformed data meets assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST

1. Order samples from smallest to largest in column x(i)
2. Order samples from largest to smallest in column x(n-i+1)
3. Compute K as the greatest integer less than or equal to N/2. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring.
Put into column a(n-i+1).
5. Sum the values in column b(i) and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W,
the distribution is non-normal. Transform and re-test.

i	x(i)	x(n-i+1)	x(n-i+1)-x(i)	a(n-i+1)	b(i)
1	1.64	3.41	1.77037341	0.6052	1.07143
2	2.59	3.41	0.81496067	0.3164	0.2578536
3	2.94	3.40	0.45687393	0.1743	0.0796331
4	3.13	3.23	0.1038072	0.0561	0.0058236
5	3.23	3.13	-0.1038072		0
6	3.40	2.94	-0.45687393		0
7	3.41	2.59	-0.81496067		1.4147403
8	3.41	1.64	-1.77037341		

std dev = 0.6065954

N = 8

K = 4

b = 1.4147403

W = 0.7770647

Critical W = 0.818

Result = Lognormally transformed data does not meet assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST ON UNTRANSFORMED DATA

1. Order samples from smallest to largest in column $x(i)$
2. Order samples from largest to smallest in column $x(n-i+1)$
3. Compute K as the greatest integer less than or equal to $N/2$. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column $a(n-i+1)$.
5. Sum the values in column $b(i)$ and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W , the distribution is non-normal. Transform and re-test.

i	$x(i)$	$x(n-i+1)$	$x(n-i+1)-x(i)$	$a(n-i+1)$	$b(i)$
1	5.15	30.23	25.0848787	0.6052	15.181369
2	13.36	30.17	16.8175901	0.3164	5.3210855
3	18.93	29.89	10.9626396	0.1743	1.9107881
4	22.81	25.30	2.49501123	0.0561	0.1399701
5	25.30	22.81	-2.49501123		0
6	29.89	18.93	-10.9626396		0
7	30.17	13.36	-16.8175901		22.553212
8	30.23	5.15	-25.0848787		

std dev = 9.0757451
 N = 8
 K = 4
 b = 22.553212
 W = 0.8821739
 Critical W = 0.818
 Result = Untransformed data meets assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST

1. Order samples from smallest to largest in column x(i)
2. Order samples from largest to smallest in column x(n-i+1)
3. Compute K as the greatest integer less than or equal to N/2. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring.
Put into column a(n-i+1).
5. Sum the values in column b(i) and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W,
the distribution is non-normal. Transform and re-test.

i	x(i)	x(n-i+1)	x(n-i+1)-x(i)	a(n-i+1)	b(i)
1	2.78	3.85	1.06650255	0.6052	0.6454473
2	2.80	3.75	0.95318633	0.3164	0.3015882
3	3.34	3.64	0.29	0.1743	0.0510591
4	3.59	3.63	0.04	0.0561	0.0023514
5	3.63	3.59	-0.04		0
6	3.64	3.34	-0.29		0
7	3.75	2.80	-0.95		1.000446
8	3.85	2.78	-1.07		

std dev = 0.4163123

N = 8

K = 4

b = 1.000446

W = 0.8249941

Critical W = 0.818

Result = Lognormally transformed data meets assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST

1. Order samples from smallest to largest in column x(i)
2. Order samples from largest to smallest in column x(n-i+1)
3. Compute K as the greatest integer less than or equal to N/2. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring.
Put into column a(n-i+1).
5. Sum the values in column b(i) and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W, the distribution is non-normal. Transform and re-test.

i	x(i)	x(n-i+1)	x(n-i+1)-x(i)	a(n-i+1)	b(i)
1	16.19	47.04	30.8500811	0.6052	18.670469
2	16.45	42.68	26.2271755	0.3164	8.2982783
3	28.36	38.01	9.65	0.1743	1.6823428
4	36.32	37.87	1.55	0.0561	0.0872152
5	37.87	36.32	-1.55		0
6	38.01	28.36	-9.65		0
7	42.68	16.45	-26.23		28.738305
8	47.04	16.19	-30.85		

std dev = 11.516846
 N = 8
 K = 4
 b = 28.738305
 W = 0.889523
 Critical W = 0.818
 Result = Untransformed data meets assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST
WHEELING SANDY LOAM SOIL TYPE
FOR SMWU 31, 54

SHAPIRO-WILK GOODNESS OF FIT TEST

1. Order samples from smallest to largest in column x(i)
2. Order samples from largest to smallest in column x(n-i+1)
3. Compute K as the greatest integer less than or equal to N/2. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring.
Put into column a(n-i+1).
5. Sum the values in column b(i) and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W,
the distribution is non-normal. Transform and re-test.

i	x(i)	x(n-i+1)	x(n-i+1)-x(i)	a(n-i+1)	b(i)
1	4.38	5.28	0.89674806	0.6431	0.5766987
2	4.71	5.23	0.52338181	0.2806	0.1468609
3	4.97	5.11	0.14447794	0.0875	0.0126418
4	5.11	4.97	-0.14447794		0
5	5.23	4.71	-0.52338181		0
6	5.28	4.38	-0.89674806		0
					0.7362014

std dev = 0.3456863

N = 6

K = 3

b = 0.7362014

W = 0.9071079

Critical W = 0.788

Result = Lognormally transformed data meets assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST ON UNTRANSFORMED DATA

1. Order samples from smallest to largest in column $x(i)$
2. Order samples from largest to smallest in column $x(n-i+1)$
3. Compute K as the greatest integer less than or equal to $N/2$. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column $a(n-i+1)$.
5. Sum the values in column $b(i)$ and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W , the distribution is non-normal. Transform and re-test.

i	$x(i)$	$x(n-i+1)$	$x(n-i+1)-x(i)$	$a(n-i+1)$	$b(i)$
1	79.72	195.44	115.723365	0.6431	74.421696
2	110.70	186.83	76.1292348	0.2806	21.361863
3	144.07	166.46	22.3933531	0.0875	1.9594184
4	166.46	144.07	-22.3933531		0
5	186.83	110.70	-76.1292348		0
6	195.44	79.72	-115.723365		0
					97.742977

std dev = 45.087632

 $N = 6$ $K = 3$ $b = 97.742977$ $W = 0.93991$ Critical $W = 0.788$

Result = Untransformed data meets assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST

1. Order samples from smallest to largest in column $x(i)$
2. Order samples from largest to smallest in column $x(n-i+1)$
3. Compute K as the greatest integer less than or equal to $N/2$. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring.
Put into column $a(n-i+1)$.
5. Sum the values in column $b(i)$ and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W , the distribution is non-normal. Transform and re-test.

i	$x(i)$	$x(n-i+1)$	$x(n-i+1)-x(i)$	$a(n-i+1)$	$b(i)$
1	4.02	5.16	1.15	0.6431	0.7369144
2	4.37	4.63	0.25	0.2806	0.0710852
3	4.39	4.61	0.22	0.0875	0.0188828
4	4.61	4.39	-0.22		0
5	4.63	4.37	-0.25		0
6	5.16	4.02	-1.15		0

std dev = 0.3803367
 N = 6
 K = 3
 b = 0.8268823
 W = 0.9453246
 Critical W = 0.788
 Result = Lognormally transformed data meets assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST ON UNTRANSFORMED DATA

1. Order samples from smallest to largest in column x(i)
2. Order samples from largest to smallest in column x(n-i+1)
3. Compute K as the greatest integer less than or equal to N/2. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column a(n-i+1).
5. Sum the values in column b(i) and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W, the distribution is non-normal. Transform and re-test.

i	x(i)	x(n-i+1)	x(n-i+1)-x(i)	a(n-i+1)	b(i)
1	55.63	174.97	119.34	0.6431	76.746906
2	79.22	102.06	22.84	0.2806	6.4086433
3	80.78	100.24	19.46	0.0875	1.7025159
4	100.24	80.78	-19.46		0
5	102.06	79.22	-22.84		0
6	174.97	55.63	-119.34		0

std dev = 40.954097
 N = 6
 K = 3
 b = 84.858065
 W = 0.8586606
 Critical W = 0.788
 Result = Untransformed data meets assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST

1. Order samples from smallest to largest in column $x(i)$
2. Order samples from largest to smallest in column $x(n-i+1)$
3. Compute K as the greatest integer less than or equal to $N/2$. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring.
Put into column $a(n-i+1)$.
5. Sum the values in column $b(i)$ and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W , the distribution is non-normal. Transform and re-test.

i	$x(i)$	$x(n-i+1)$	$x(n-i+1)-x(i)$	$a(n-i+1)$	$b(i)$
1	-0.377877	0.4563473	0.83422443	0.6431	0.5364897
2	-0.003612	0.4426878	0.44630008	0.2806	0.1252318
3	0.3966333	0.4222722	0.02563895	0.0875	0.0022434
4	0.4222722	0.3966333	-0.02563895		0
5	0.4426878	-0.003612	-0.44630008		0
6	0.4563473	-0.377877	-0.83422443		0
					0.6639649

std dev = 0.3420461

N = 6

K = 3

b = 0.6639649

W = 0.7536175

Critical W = 0.788

Result = Lognormally transformed data does not meet assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST ON UNTRANSFORMED DATA

1. Order samples from smallest to largest in column $x(i)$
2. Order samples from largest to smallest in column $x(n-i+1)$
3. Compute K as the greatest integer less than or equal to $N/2$. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column $a(n-i+1)$.
5. Sum the values in column $b(i)$ and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W , the distribution is non-normal. Transform and re-test.

i	$x(i)$	$x(n-i+1)$	$x(n-i+1)-x(i)$	$a(n-i+1)$	$b(i)$
1	0.69	1.58	0.89298367	0.6431	0.5742778
2	1.00	1.56	0.56049195	0.2806	0.157274
3	1.49	1.53	0.03861314	0.0875	0.0033786
4	1.53	1.49	-0.03861314		0
5	1.56	1.00	-0.56049195		0
6	1.58	0.69	-0.89298367		0
					0.6639649

std dev = 0.3739058

N = 6

K = 3

b = 0.6639649

W = 0.630661

Critical W = 0.788

Result = Untransformed data does not meet assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST

1. Order samples from smallest to largest in column x(i)
2. Order samples from largest to smallest in column x(n-i+1)
3. Compute K as the greatest integer less than or equal to N/2. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column a(n-i+1).
5. Sum the values in column b(i) and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W, the distribution is non-normal. Transform and re-test.

i	x(i)	x(n-i+1)	x(n-i+1)-x(i)	a(n-i+1)	b(i)
1	-0.40041	0.4099105	0.81032087	0.6431	0.5211173
2	-0.227506	-0.092412	0.13509329	0.2806	0.0379072
3	-0.17185	-0.117332	0.0545183	0.0875	0.0047704
4	-0.117332	-0.17185	-0.0545183		0
5	-0.092412	-0.227506	-0.13509329		0
6	0.4099105	-0.40041	-0.81032087		0

std dev = 0.2727758
 N = 6
 K = 3
 b = 0.5637949
 W = 0.8543987
 Critical W = 0.788
 Result = Lognormally transformed data meets assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST ON UNTRANSFORMED DATA

1. Order samples from smallest to largest in column $x(i)$
2. Order samples from largest to smallest in column $x(n-i+1)$
3. Compute K as the greatest integer less than or equal to $N/2$. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column $a(n-i+1)$.
5. Sum the values in column $b(i)$ and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W , the distribution is non-normal. Transform and re-test.

i	$x(i)$	$x(n-i+1)$	$x(n-i+1)-x(i)$	$a(n-i+1)$	$b(i)$
1	0.67	1.51	0.83663788	0.6431	0.5380418
2	0.80	0.91	0.11521119	0.2806	0.0323283
3	0.84	0.89	0.04718468	0.0875	0.0041287
4	0.89	0.84	-0.04718468		0
5	0.91	0.80	-0.11521119		0
6	1.51	0.67	-0.83663788		0

std dev = 0.2923879
 N = 6
 K = 3
 b = 0.5744987
 W = 0.7721282
 Critical W = 0.788
 Result = Untransformed data does not meet assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST

1. Order samples from smallest to largest in column x(i)
2. Order samples from largest to smallest in column x(n-i+1)
3. Compute K as the greatest integer less than or equal to N/2. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring.
Put into column a(n-i+1).
5. Sum the values in column b(i) and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W, the distribution is non-normal. Transform and re-test.

i	x(i)	x(n-i+1)	x(n-i+1)-x(i)	a(n-i+1)	b(i)
1	3.49	4.00	0.51925194	0.6431	0.3339309
2	3.53	3.90	0.36830934	0.2806	0.1033476
3	3.76	3.89	0.1248102	0.0875	0.0109209
4	3.89	3.76	-0.1248102		0
5	3.90	3.53	-0.36830934		0
6	4.00	3.49	-0.51925194		0
					0.4481994

std dev = 0.2118383

N = 6

K = 3

b = 0.4481994

W = 0.8952898

Critical W = 0.788

Result = Lognormally transformed data meets assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST ON UNTRANSFORMED DATA

1. Order samples from smallest to largest in column $x(i)$
2. Order samples from largest to smallest in column $x(n-i+1)$
3. Compute K as the greatest integer less than or equal to $N/2$. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring.
Put into column $a(n-i+1)$.
5. Sum the values in column $b(i)$ and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W , the distribution is non-normal. Transform and re-test.

i	$x(i)$	$x(n-i+1)$	$x(n-i+1)-x(i)$	$a(n-i+1)$	$b(i)$
1	32.63	54.85	22.2162659	0.6431	14.287281
2	34.01	49.16	15.1462498	0.2806	4.2500377
3	43.10	48.83	5.72933299	0.0875	0.5013166
4	48.83	43.10	-5.72933299		0
5	49.16	34.01	-15.1462498		0
6	54.85	32.63	-22.2162659		0
					19.038635

std dev = 8.9112582

 $N = 6$ $K = 3$ $b = 19.038635$ $W = 0.9129007$ Critical $W = 0.788$

Result = Untransformed data meets assumption of normality

Chromium horizon C

SHAPIRO-WILK GOODNESS OF FIT TEST

1. Order samples from smallest to largest in column x(i)
2. Order samples from largest to smallest in column x(n-i+1)
3. Compute K as the greatest integer less than or equal to N/2. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring.
Put into column a(n-i+1).
5. Sum the values in column b(i) and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W, the distribution is non-normal. Transform and re-test.

i	x(i)	x(n-i+1)	x(n-i+1)-x(i)	a(n-i+1)	b(i)
1	3.28	3.86	0.58344567	0.6431	0.3752139
2	3.34	3.67	0.32528638	0.2806	0.0912754
3	3.52	3.64	0.1123111	0.0875	0.0098272
4	3.64	3.52	-0.1123111		0
5	3.67	3.34	-0.32528638		0
6	3.86	3.28	-0.58344567		0
					0.4763165

std dev = 0.2173526

N = 6

K = 3

b = 0.4763165

W = 0.9604872

Critical W = 0.788

Result = Lognormally transformed data meets assumption of normality

Chromium horizon C

SHAPIRO-WILK GOODNESS OF FIT TEST ON UNTRANSFORMED DATA

1. Order samples from smallest to largest in column x(i)
2. Order samples from largest to smallest in column x(n-i+1)
3. Compute K as the greatest integer less than or equal to N/2. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring.
Put into column a(n-i+1).
5. Sum the values in column b(i) and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W, the distribution is non-normal. Transform and re-test.

i	x(i)	x(n-i+1)	x(n-i+1)-x(i)	a(n-i+1)	b(i)
1	26.58	47.63	21.0540463	0.6431	13.539857
2	28.29	39.17	10.8760648	0.2806	3.0518238
3	33.94	37.97	4.03354604	0.0875	0.3529353
4	37.97	33.94	-4.03354604		0
5	39.17	28.29	-10.8760648		0
6	47.63	26.58	-21.0540463		0
					16.944616

std dev = 7.7547526

N = 6

K = 3

b = 16.944616

W = 0.9548993

Critical W = 0.788

Result = Untransformed data meets assumption of normality

Lead horizon B

SHAPIRO-WILK GOODNESS OF FIT TEST

1. Order samples from smallest to largest in column $x(i)$
2. Order samples from largest to smallest in column $x(n-i+1)$
3. Compute K as the greatest integer less than or equal to $N/2$. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column $a(n-i+1)$.
5. Sum the values in column $b(i)$ and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W, the distribution is non-normal. Transform and re-test.

i	$x(i)$	$x(n-i+1)$	$x(n-i+1)-x(i)$	$a(n-i+1)$	$b(i)$
1	2.43	3.22	0.79100806	0.6431	0.5086973
2	2.50	3.16	0.66793915	0.2806	0.1874237
3	2.98	3.14	0.16018695	0.0875	0.0140164
4	3.14	2.98	-0.16018695		0
5	3.16	2.50	-0.66793915		0
6	3.22	2.43	-0.79100806		0

std dev = 0.3533872

N = 6

K = 3

b = 0.7101374

W = 0.8076313

Critical W = 0.788

Result = Lognormally transformed data meets assumption of normality

Lead horizon B

SHAPIRO-WILK GOODNESS OF FIT TEST ON UNTRANSFORMED DATA

1. Order samples from smallest to largest in column $x(i)$
2. Order samples from largest to smallest in column $x(n-i+1)$
3. Compute K as the greatest integer less than or equal to $N/2$. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column $a(n-i+1)$.
5. Sum the values in column $b(i)$ and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W, the distribution is non-normal. Transform and re-test.

i	$x(i)$	$x(n-i+1)$	$x(n-i+1)-x(i)$	$a(n-i+1)$	$b(i)$
1	11.31	24.94	13.632541	0.6431	8.7670871
2	12.14	23.67	11.535051	0.2806	3.2367353
3	19.76	23.19	3.43299366	0.0875	0.3003869
4	23.19	19.76	-3.43299366		0
5	23.67	12.14	-11.535051		0
6	24.94	11.31	-13.632541		0

std dev = 6.0227659

N = 6

K = 3

b = 12.304209

W = 0.8347289

Critical W = 0.788

Result = Untransformed data meets assumption of normality

Lead horizon C

SHAPIRO-WILK GOODNESS OF FIT TEST

1. Order samples from smallest to largest in column $x(i)$
2. Order samples from largest to smallest in column $x(n-i+1)$
3. Compute K as the greatest integer less than or equal to $N/2$. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column $a(n-i+1)$.
5. Sum the values in column $b(i)$ and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W , the distribution is non-normal. Transform and re-test.

i	$x(i)$	$x(n-i+1)$	$x(n-i+1)-x(i)$	$a(n-i+1)$	$b(i)$
1	2.38	3.13	0.7516109	0.6431	0.483361
2	2.63	2.92	0.30	0.2806	0.083078
3	2.72	2.82	0.10	0.0875	0.008927
4	2.82	2.72	-0.10		0
5	2.92	2.63	-0.30		0
6	3.13	2.38	-0.75		0
					0.575366

std dev = 0.257596
 N = 6
 K = 3
 b = 0.575366
 W = 0.997796
 Critical W = 0.788
 Result = Lognormally transformed data meets assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST ON UNTRANSFORMED DATA

1. Order samples from smallest to largest in column x(i)
2. Order samples from largest to smallest in column x(n-i+1)
3. Compute K as the greatest integer less than or equal to N/2. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column a(n-i+1).
5. Sum the values in column b(i) and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W, the distribution is non-normal. Transform and re-test.

i	x(i)	x(n-i+1)	x(n-i+1)-x(i)	a(n-i+1)	b(i)
1	10.83	22.96	12.134438	0.6431	7.803657
2	13.82	18.58	4.76	0.2806	1.336136
3	15.18	16.81	1.63	0.0875	0.142648
4	16.81	15.18	-1.63		0
5	18.58	13.82	-4.76		0
6	22.96	10.83	-12.13		0
					9.282441

std dev = 4.17581
N = 6
K = 3
b = 9.282441
W = 0.988264
Critical W = 0.788
Result = Untransformed data meets assumption of normality

Nickel horizon B

SHAPIRO-WILK GOODNESS OF FIT TEST

1. Order samples from smallest to largest in column x(i)
2. Order samples from largest to smallest in column x(n-i+1)
3. Compute K as the greatest integer less than or equal to N/2. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring.
Put into column a(n-i+1).
5. Sum the values in column b(i) and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W, the distribution is non-normal. Transform and re-test.

i	x(i)	x(n-i+1)	x(n-i+1)-x(i)	a(n-i+1)	b(i)
1	2.36	3.29	0.92977917	0.6431	0.597941
2	2.60	3.29	0.68627194	0.2806	0.1925679
3	3.05	3.28	0.23278519	0.0875	0.0203687
4	3.28	3.05	-0.23278519		0
5	3.29	2.60	-0.68627194		0
6	3.29	2.36	-0.92977917		0
					0.8108776

std dev = 0.4037816

N = 6

K = 3

b = 0.8108776

W = 0.8065803

Critical W = 0.788

Result = Lognormally transformed data meets assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST ON UNTRANSFORMED DATA

1. Order samples from smallest to largest in column $x(i)$
2. Order samples from largest to smallest in column $x(n-i+1)$
3. Compute K as the greatest integer less than or equal to $N/2$. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column $a(n-i+1)$.
5. Sum the values in column $b(i)$ and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W , the distribution is non-normal. Transform and re-test.

i	$x(i)$	$x(n-i+1)$	$x(n-i+1)-x(i)$	$a(n-i+1)$	$b(i)$
1	10.56	26.76	16.1976498	0.6431	10.416709
2	13.46	26.74	13.2770702	0.2806	3.7255459
3	21.07	26.59	5.52145252	0.0875	0.4831271
4	26.59	21.07	-5.52145252		0
5	26.74	13.46	-13.2770702		0
6	26.76	10.56	-16.1976498		0
					14.625382

std dev = 7.25274

 $N = 6$ $K = 3$ $b = 14.625382$ $W = 0.8132802$ Critical $W = 0.788$

Result = Untransformed data meets assumption of normality

SHAPIRO-WILK GOODNESS OF FIT TEST

1. Order samples from smallest to largest in column $x(i)$
2. Order samples from largest to smallest in column $x(n-i+1)$
3. Compute K as the greatest integer less than or equal to $N/2$. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring. Put into column $a(n-i+1)$.
5. Sum the values in column $b(i)$ and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W , the distribution is non-normal. Transform and re-test.

i	$x(i)$	$x(n-i+1)$	$x(n-i+1)-x(i)$	$a(n-i+1)$	$b(i)$
1	2.26	3.31	1.04951365	0.6431	0.6749422
2	2.58	2.73	0.1483551	0.2806	0.0416284
3	2.62	2.66	0.03351745	0.0875	0.0029328
4	2.66	2.62	-0.03351745		0
5	2.73	2.58	-0.1483551		0
6	3.31	2.26	-1.04951365		0
					0.7195034

std dev = 0.34279

N = 6

K = 3

b = 0.7195034

W = 0.8811289

Critical W = 0.788

Result = Lognormally transformed data meets assumption of normality

Nickel horizon C

SHAPIRO-WILK GOODNESS OF FIT TEST ON UNTRANSFORMED DATA

1. Order samples from smallest to largest in column x(i)
2. Order samples from largest to smallest in column x(n-i+1)
3. Compute K as the greatest integer less than or equal to N/2. Enter in cell
4. Look up coefficients from table A-1 in EPA Statistical Course for GW Monitoring.
Put into column a(n-i+1).
5. Sum the values in column b(i) and enter in cell
6. Enter N in cell
7. Compare W statistic to Critical W in Table A-2 in same guidance. If W is less than critical W, the distribution is non-normal. Transform and re-test.

i	x(i)	x(n-i+1)	x(n-i+1)-x(i)	a(n-i+1)	b(i)
1	9.57	27.34	17.7674004	0.6431	11.426215
2	13.18	15.28	2.10711608	0.2806	0.5912568
3	13.78	14.25	0.46986041	0.0875	0.0411128
4	14.25	13.78	-0.46986041		0
5	15.28	13.18	-2.10711608		0
6	27.34	9.57	-17.7674004		0
					12.058585

std dev = 6.0864235

N = 6

K = 3

b = 12.058585

W' = 0.7850519

Critical W' = 0.788

Result = Untransformed data does not meet assumption of normality

TOLERANCE LIMIT CALCULATIONS

**SUMMARY OF TOLERANCE LIMITS
RADFORD ARMY AMMUNITION PLANT**

Soil Horizon	Soil Series	Constituent	Upper	Tolerance Limit Type	Exceedance?
			Tolerance Limit		
SWMU 17A	B	Antimony	21.0	Poisson	Yes
SWMU 17A	B	Arsenic	5.5	Poisson	Yes
SWMU 17A	B	Barium	9.7	Normal	No
SWMU 17A	B	Beryllium	4.5	Poisson	No
SWMU 17A	B	Cadmium	3.5	Poisson	Yes
SWMU 17A	B	Chromium	5.1	Normal	Yes
SWMU 17A	B	Lead	8.7	Normal	No
SWMU 17A	B	Mercury	1.5	Poisson	No
SWMU 17A	B	Nickel	6.0	Normal	Yes
SWMU 17A	B	Selenium	2.5	Poisson	No
SWMU 17A	B	Silver	1.5	Poisson	Yes
SWMU 17A	B	Thallium	33.5	Poisson	No
SWMU 17A	C	Antimony	21.5	Poisson	No
SWMU 17A	C	Arsenic	11.5	Poisson	Yes
SWMU 17A	C	Barium	6.9	Normal	No
SWMU 17A	C	Beryllium	2.7	Normal	No
SWMU 17A	C	Cadmium	3.5	Poisson	No
SWMU 17A	C	Chromium	5.0	Normal	No
SWMU 17A	C	Lead	4.2	Normal	Yes
SWMU 17A	C	Mercury	1.5	Poisson	No
SWMU 17A	C	Nickel	5.4	Normal	No
SWMU 17A	C	Selenium	2.5	Poisson	No
SWMU 17A	C	Silver	1.5	Poisson	Yes
SWMU 17A	C	Thallium	33.5	Poisson	No
SWMU 17BCD	B	Antimony	21.0	Poisson	No
SWMU 17BCD	B	Arsenic	5.5	Poisson	Yes
SWMU 17BCD	B	Barium	9.7	Normal	No
SWMU 17BCD	B	Beryllium	4.5	Poisson	No
SWMU 17BCD	B	Cadmium	3.5	Poisson	No
SWMU 17BCD	B	Chromium	5.1	Normal	No
SWMU 17BCD	B	Lead	8.7	Normal	No
SWMU 17BCD	B	Mercury	1.5	Poisson	No
SWMU 17BCD	B	Nickel	6.0	Normal	No
SWMU 17BCD	B	Selenium	2.5	Poisson	No
SWMU 17BCD	B	Silver	1.5	Poisson	No
SWMU 17BCD	B	Thallium	33.5	Poisson	No
SWMU 17BCD	C	Antimony	21.5	Poisson	No
SWMU 17BCD	C	Arsenic	11.5	Poisson	No
SWMU 17BCD	C	Barium	6.9	Normal	No
SWMU 17BCD	C	Beryllium	2.3	Normal	Yes
SWMU 17BCD	C	Cadmium	3.5	Poisson	Yes
SWMU 17BCD	C	Chromium	5.0	Normal	No
SWMU 17BCD	C	Lead	4.2	Normal	Yes
SWMU 17BCD	C	Mercury	1.5	Poisson	No
SWMU 17BCD	C	Nickel	5.4	Normal	No
SWMU 17BCD	C	Selenium	2.5	Poisson	No
SWMU 17BCD	C	Silver	1.5	Poisson	No
SWMU 17BCD	C	Thallium	33.5	Poisson	No

**SUMMARY OF TOLERANCE LIMITS
RADFORD ARMY AMMUNITION PLANT**

Soil Horizon	Soil Series	Constituent	Upper	Tolerance	Tolerance	Exceedance?
			Limit		Limit Type	
SWMU 31	C	Antimony	20.5	Poisson	No	No
SWMU 31	C	Arsenic	7.0	Poisson	No	No
SWMU 31	C	Barium	7.1	Normal	No	No
SWMU 31	C	Beryllium	.5	Normal	No	No
SWMU 31	C	Cadmium	3.5	Poisson	No	No
SWMU 31	C	Chromium	4.8	Normal	No	No
SWMU 31	C	Lead	4.1	Normal	No	No
SWMU 31	C	Mercury	2.0	Poisson	No	No
SWMU 31	C	Nickel	4.3	Normal	No	No
SWMU 31	C	Selenium	2.5	Poisson	No	No
SWMU 31	C	Silver	1.5	Poisson	No	No
SWMU 31	C	Thallium	31.5	Poisson	No	No
SWMU 54	B	Antimony	20.5	Poisson	No	No
SWMU 54	B	Arsenic	6.5	Poisson	No	No
SWMU 54	B	Barium	7.4	Normal	No	No
SWMU 54	B	Beryllium	5.0	Poisson	No	No
SWMU 54	B	Cadmium	3.5	Poisson	Yes	Yes
SWMU 54	B	Chromium	5.0	Normal	No	No
SWMU 54	B	Lead	4.7	Normal	Yes	Yes
SWMU 54	B	Mercury	1.5	Poisson	Yes	Yes
SWMU 54	B	Nickel	5.0	Normal	No	No
SWMU 54	B	Selenium	2.5	Poisson	No	No
SWMU 54	B	Silver	2.0	Poisson	No	No
SWMU 54	B	Thallium	32.0	Poisson	No	No
SWMU 54	C	Antimony	20.5	Poisson	No	No
SWMU 54	C	Arsenic	7.0	Poisson	No	No
SWMU 54	C	Barium	7.1	Normal	No	No
SWMU 54	C	Beryllium	.5	Normal	Yes	Yes
SWMU 54	C	Cadmium	3.5	Poisson	No	No
SWMU 54	C	Chromium	4.8	Normal	No	No
SWMU 54	C	Lead	4.1	Normal	Yes	Yes
SWMU 54	C	Mercury	2.0	Poisson	No	No
SWMU 54	C	Nickel	4.3	Normal	No	No
SWMU 54	C	Selenium	2.5	Poisson	No	No
SWMU 54	C	Silver	1.5	Poisson	No	No
SWMU 54	C	Thallium	31.5	Poisson	No	No

Antimony soil B

Poisson-based Tolerance Limit (K) Calculation for Antimony soil horizon B, SWMU 17A

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of Tn})$

Where

Lambda of Tn = $(1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2Tn+2))$

Where

Tn = Poisson count of background

n = Background sample size

alpha = Probability level test is conducted at (here, 0.05)

Tn 100.94

2Tn+2 203.88

Chi Square (2Tn+2) 238.191

n 8

Lambda Tn 14.886938

2(Lambda Tn) 29.773875

Chi Square $0.05[2K+2] \geq$ 29.773875 $[2K+2] = 44$

K = 21

FSampNo	Value	Limit	Limit Exceeded?
17ASB105	77.95	21	Yes
17ASB205	12.21	21	No
17ASB305	14.83	21	No

Antimony soil C

Poisson-based Tolerance Limit (K) Calculation for Antimony soil horizon C, SWMU 17A

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of Tn})$

Where

Lambda of Tn = $(1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2Tn+2))$

Where

Tn = Poisson count of background

n = Background sample size

alpha = Probability level test is conducted at (here, 0.05)

Tn	101.34
2Tn+2	204.68
Chi Square (2Tn+2)	239.056
n	8
Lambda Tn	14.941
2(Lambda Tn)	29.882
Chi Square 0.05 $[2K+2] \geq$	29.882
$[2K+2] = 45$	
K = 21.5	

FSampNo	Value	Limit	Limit Exceeded?
17ASB110	12.42	21.5	No
17ASB210	11.74	21.5	No
17ASB310	14.37	21.5	No
17ASB115	12.03	21.5	No
17ASB215	14.10	21.5	No
17ASB315	13.37	21.5	No
17ASB120	12.21	21.5	No
17ASB220	15.06	21.5	No
17ASB320	10.77	21.5	No
17ASB122	12.81	21.5	No
17ASB225	14.04	21.5	No
17ASB325	10.75	21.5	No
17ASB340	10.76	21.5	No

Arsenic horizon B

Poisson-based Tolerance Limit (K) Calculation for Arsenic soil horizon B, SWMU 17A

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of Tn})$

Where

Lambda of Tn = $(1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2Tn+2))$

Where

Tn = Poisson count of background

n = Background sample size

alpha = Probability level test is conducted at (here, 0.05)

Tn	55.13
2Tn+2	112.26
Chi Square (2Tn+2)	137.988
n	8
Lambda Tn	8.62425
2(Lambda Tn)	17.2485
Chi Square0.05[2K+2]>=	17.2485
[2K+2] = 13	
K = 5.5	

FSampNo	Value	Limit	Limit Exceeded?
17ASB105	94.87	5.5	Yes
17ASB205	7.33	5.5	Yes
17ASB305	6.70	5.5	Yes

Arsenic horizon C

Poisson-based Tolerance Limit (K) Calculation for Arsenic soil horizon C, SWMU 17A

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

 $T_n =$ Poisson count of background $n =$ Background sample size $\alpha =$ Probability level test is conducted at (here, 0.05)

T_n	43.70
$2T_n+2$	89.40
Chi Square ($2T_n+2$)	112.471
n	8
Lambda T_n	7.0294375
$2(\text{Lambda } T_n)$	14.058875
Chi Square $0.05[2K+2] \geq$	14.058875
$[2K+2] = 25$	
$K = 11.5$	

FSampNo	Value	Limit	Limit Exceeded?
17ASB110	9.30	11.5	No
17ASB210	1.50	11.5	No
17ASB310	7.51	11.5	No
17ASB115	13.50	11.5	Yes
17ASB215	8.98	11.5	No
17ASB315	4.64	11.5	No
17ASB120	16.69	11.5	Yes
17ASB220	1.92	11.5	No
17ASB320	3.75	11.5	No
17ASB122	1.64	11.5	No
17ASB225	1.79	11.5	No
17ASB325	1.37	11.5	No
17ASB340	3.30	11.5	No

Barium horizon B

Normal Tolerance Limit (K) Calculation for Barium soil horizon B, SWMU 17A

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	4.39
Where		std. dev.	0.83
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	6.399951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17ASB105	8.54	9.7019594	5128.21	16349.61	No
17ASB205	4.16	9.7019594	64.38	16349.61	No
17ASB305	4.27	9.7019594	71.26	16349.61	No

Barium horizon C

Normal Tolerance Limit (K) Calculation for Barium soil horizon C

$K = \text{average} + t(N-1, \alpha) * \text{SQRT}(1 + (1/N))$		average	4.51
Where		std. dev.	0.37
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	6.519951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17ASB110	4.15	6.9223819	63.12	1014.7341	No
17ASB210	4.33	6.9223819	75.69	1014.7341	No
17ASB310	4.84	6.9223819	126.39	1014.7341	No
17ASB115	4.24	6.9223819	69.20	1014.7341	No
17ASB215	4.46	6.9223819	86.91	1014.7341	No
17ASB315	3.81	6.9223819	45.16	1014.7341	No
17ASB120	4.24	6.9223819	69.36	1014.7341	No
17ASB220	4.90	6.9223819	134.25	1014.7341	No
17ASB320	3.97	6.9223819	52.97	1014.7341	No
17ASB122	4.27	6.9223819	71.50	1014.7341	No
17ASB225	2.26	6.9223819	9.56	1014.7341	No
17ASB325	4.00	6.9223819	54.71	1014.7341	No
17ASB340	3.54	6.9223819	34.58	1014.7341	No

Beryllium horizon B

Poisson-based Tolerance Limit (K) Calculation for Beryllium soil horizon B, SWMU 17A

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

 $T_n =$ Poisson count of background $n =$ Background sample size $\alpha =$ Probability level test is conducted at (here, 0.05)

T_n	10.67
$2T_n+2$	23.34
Chi Square ($2T_n+2$)	35.5955
n	8
Lambda T_n	2.2247188
$2(\text{Lambda } T_n)$	4.4494375
Chi Square $0.05[2K+2] \geq$	4.4494375
$[2K+2] = 11$	
$K = 4.5$	

FSampNo	Value	Limit	Limit Exceeded?
17ASB105	1.65	4.5	No
17ASB205	2.23	4.5	No
17ASB305	3.40	4.5	No

Beryllium horizon C

Normal Tolerance Limit (K) Calculation for Beryllium soil horizon C, SWMU 17A

$$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$$

Where

t = Critical value of Student's t distribution

N = Sample size

alpha = Probability level test is conducted at (here, 0.05)

average 0.7

std. dev. 0.59

t 1.895

N 8

K 2.709951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17ASB110	0.80	2.2988711	2.22	9.962929	No
17ASB210	0.72	2.2988711	2.06	9.962929	No
17ASB310	2.00	2.2988711	7.39	9.962929	No
17ASB115	0.75	2.2988711	2.11	9.962929	No
17ASB215	1.51	2.2988711	4.52	9.962929	No
17ASB315	0.79	2.2988711	2.20	9.962929	No
17ASB120	0.57	2.2988711	1.77	9.962929	No
17ASB220	1.92	2.2988711	6.82	9.962929	No
17ASB320	-0.56	2.2988711	0.57	9.962929	No
17ASB122	0.76	2.2988711	2.13	9.962929	No
17ASB225	-1.17	2.2988711	0.31	9.962929	No
17ASB325	-0.26	2.2988711	0.77	9.962929	No
17ASB340	0.44	2.2988711	1.55	9.962929	No

Cadmium soil B

Poisson-based Tolerance Limit (K) Calculation for Cadmium soil horizon B, SWMU 17A

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

 $T_n =$ Poisson count of background $n =$ Background sample size $\alpha =$ Probability level test is conducted at (here, 0.05)

T_n	6.2
$2T_n+2$	14.40
Chi Square ($2T_n+2$)	24.2105
n	8
Lambda T_n	1.5131563
$2(\text{Lambda } T_n)$	3.0263125
Chi Square $0.05[2K+2] \geq$	3.0263125
$[2K+2] = 9$	
$K = 3.5$	

FSampNo	Value	Limit	Limit Exceeded?
17ASB105	13.72	3.5	Yes
17ASB205	0.75	3.5	No
17ASB305	0.91	3.5	No

Cadmium soil C

Poisson-based Tolerance Limit (K) Calculation for Cadmium soil horizon C, SWMU 17A

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of Tn})$

Where

Lambda of Tn = $(1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2Tn+2))$

Where

Tn = Poisson count of background

n = Background sample size

alpha = Probability level test is conducted at (here, 0.05)

Tn	6.23
2Tn+2	14.46
Chi Square (2Tn+2)	24.2892
n	8
Lambda Tn	1.518075
2(Lambda Tn)	3.03615
Chi Square 0.05 [2K+2] $\geq$	3.03615
[2K+2] = 9	
K = 3.5	

FSampNo	Value	Limit	Limit Exceeded?
17ASB110	0.76	3.5	No
17ASB210	0.72	3.5	No
17ASB310	0.88	3.5	No
17ASB115	0.74	3.5	No
17ASB215	0.87	3.5	No
17ASB315	0.82	3.5	No
17ASB120	0.75	3.5	No
17ASB220	0.92	3.5	No
17ASB320	0.66	3.5	No
17ASB122	0.79	3.5	No
17ASB225	0.86	3.5	No
17ASB325	0.66	3.5	No
17ASB340	0.66	3.5	No

Chromium soil B

Normal Tolerance Limit (K) Calculation for Chromium soil horizon B, SWMU 17A

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	3.82
Where		std. dev.	0.22
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	5.829951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17ASB105	7.63	5.1025892	2051.28	164.44715	Yes
17ASB205	3.85	5.1025892	46.82	164.44715	No
17ASB305	3.98	5.1025892	53.71	164.44715	No

Chromium soil C

Normal Tolerance Limit (K) Calculation for Chromium soil horizon C, SWMU 17A

K = average + $t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	3.83
Where		std. dev.	0.2
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	5.839951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17ASB110	4.02	4.9979902	55.51	148.11518	No
17ASB210	3.91	4.9979902	49.70	148.11518	No
17ASB310	4.37	4.9979902	79.33	148.11518	No
17ASB115	4.00	4.9979902	54.72	148.11518	No
17ASB215	4.45	4.9979902	86.04	148.11518	No
17ASB315	4.33	4.9979902	75.99	148.11518	No
17ASB120	4.01	4.9979902	54.92	148.11518	No
17ASB220	4.81	4.9979902	122.27	148.11518	No
17ASB320	2.85	4.9979902	17.25	148.11518	No
17ASB122	4.23	4.9979902	68.50	148.11518	No
17ASB225	2.02	4.9979902	7.56	148.11518	No
17ASB325	3.12	4.9979902	22.59	148.11518	No
17ASB340	3.82	4.9979902	45.44	148.11518	No

Lead horizon B

Normal Tolerance Limit (K) Calculation for Lead soil horizon B, SWMU 17A

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	3.24
Where		std. dev.	1.04
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	5.249951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17ASB105	8.57	8.6999491	5256.41	6002.6065	No
17ASB205	3.27	8.6999491	26.28	6002.6065	No
17ASB305	3.30	8.6999491	27.08	6002.6065	No

Lead horizon C

Normal Tolerance Limit (K) Calculation for Lead soil horizon C, SWMU 17A

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	2.71
Where		std. dev.	0.31
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	4.719951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17ASB110	4.62	4.1731848	101.39	64.921888	Yes
17ASB210	2.65	4.1731848	14.13	64.921888	No
17ASB310	3.14	4.1731848	23.02	64.921888	No
17ASB115	4.03	4.1731848	56.44	64.921888	No
17ASB215	4.24	4.1731848	69.06	64.921888	Yes
17ASB315	3.08	4.1731848	21.83	64.921888	No
17ASB120	5.61	4.1731848	273.97	64.921888	Yes
17ASB220	3.73	4.1731848	41.78	64.921888	No
17ASB320	3.43	4.1731848	30.77	64.921888	No
17ASB122	2.47	4.1731848	11.79	64.921888	No
17ASB225	4.35	4.1731848	77.36	64.921888	Yes
17ASB325	2.22	4.1731848	9.23	64.921888	No
17ASB340	2.75	4.1731848	15.70	64.921888	No

Mercury, horizon B

Poisson-based Tolerance Limit (K) Calculation for Mercury soil horizon B, SWMU 17A

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

$T_n =$ Poisson count of background

$n =$ Background sample size

$\alpha =$ Probability level test is conducted at (here, 0.05)

T_n	0.76
$2T_n+2$	3.52
Chi Square $(2T_n+2)$	8.69852
n	8
Lambda T_n	0.5436575
$2(\text{Lambda } T_n)$	1.087315
Chi Square $0.05[2K+2] \geq$	1.087315
$[2K+2] = 5$	
$K = 1.5$	

FSampNo	Value	Limit	Limit Exceeded?
17ASB105	0.29	1.5	No
17ASB205	0.18	1.5	No
17ASB305	0.18	1.5	No

Mercury, horizon C

Poisson-based Tolerance Limit (K) Calculation for Mercury soil horizon C, SWMU 17A

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

$T_n =$ Poisson count of background

$n =$ Background sample size

alpha = Probability level test is conducted at (here, 0.05)

T_n	0.63
$2T_n+2$	3.26
Chi Square ($2T_n+2$)	8.26084
n	8
Lambda T_n	0.5163025
$2(\text{Lambda } T_n)$	1.032605
Chi Square $0.05[2K+2] \geq$	1.032605
$[2K+2] = 5$	
$K = 1.5$	

FSampNo	Value	Limit	Limit Exceeded?
17ASB110	0.14	1.5	No
17ASB210	0.03	1.5	No
17ASB310	0.13	1.5	No
17ASB115	0.16	1.5	No
17ASB215	0.12	1.5	No
17ASB315	0.04	1.5	No
17ASB120	0.11	1.5	No
17ASB220	0.04	1.5	No
17ASB320	0.03	1.5	No
17ASB122	0.09	1.5	No
17ASB225	0.04	1.5	No
17ASB325	0.03	1.5	No
17ASB340	0.03	1.5	No

Nickel horizon B

Normal Tolerance Limit (K) Calculation for Nickel soil horizon B, SWMU 17A

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	2.97
Where		std. dev.	0.61
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	4.979951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17ASB105	6.81	6.0077701	902.56	406.5757	Yes
17ASB205	3.26	6.0077701	26.15	406.5757	No
17ASB305	3.55	6.0077701	34.64	406.5757	No

Nickel horizon C

Normal Tolerance Limit (K) Calculation for Nickel soil horizon C, SWMU 17A

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	3.24
Where		std. dev.	0.42
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	5.249951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17ASB110	3.21	5.4449794	24.84	231.59252	No
17ASB210	3.32	5.4449794	27.78	231.59252	No
17ASB310	4.27	5.4449794	71.26	231.59252	No
17ASB115	3.37	5.4449794	29.20	231.59252	No
17ASB215	4.04	5.4449794	56.83	231.59252	No
17ASB315	3.60	5.4449794	36.43	231.59252	No
17ASB120	3.19	5.4449794	24.28	231.59252	No
17ASB220	4.37	5.4449794	78.96	231.59252	No
17ASB320	1.84	5.4449794	6.30	231.59252	No
17ASB122	3.35	5.4449794	28.37	231.59252	No
17ASB225	1.81	5.4449794	6.12	231.59252	No
17ASB325	2.39	5.4449794	10.90	231.59252	No
17ASB340	3.17	5.4449794	23.71	231.59252	No

Selenium horizon B

Poisson-based Tolerance Limit (K) Calculation for Selenium soil horizon B, SWMU 17A

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

$T_n =$ Poisson count of background

$n =$ Background sample size

alpha = Probability level test is conducted at (here, 0.05)

T_n	2.34
$2T_n+2$	6.68
Chi Square $(2T_n+2)$	13.5992
n	8
Lambda T_n	0.84995
$2(\text{Lambda } T_n)$	1.6999
Chi Square $0.05[2K+2] \geq$	1.6999
$[2K+2] = 7$	
$K = 2.5$	

FSampNo	Value	Limit	Limit Exceeded?
17ASB105	0.29	2.5	No
17ASB205	0.28	2.5	No
17ASB305	0.34	2.5	No

Selenium horizon C

Poisson-based Tolerance Limit (K) Calculation for Silver soil horizon C, SWMU 17A

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

 $T_n =$ Poisson count of background $n =$ Background sample size $\alpha =$ Probability level test is conducted at (here, 0.05)

T_n	2.34
$2T_n+2$	6.68
Chi Square ($2T_n+2$)	13.5992
n	8
Lambda T_n	0.84995
$2(\text{Lambda } T_n)$	1.6999
Chi Square $0.05[2K+2] \geq$	1.6999
$[2K+2] = 7$	
$K = 2.5$	

FSampNo	Value	Limit	Limit Exceeded?
17ASB110	0.29	2.5	No
17ASB210	0.27	2.5	No
17ASB310	0.33	2.5	No
17ASB115	0.28	2.5	No
17ASB215	0.33	2.5	No
17ASB315	0.31	2.5	No
17ASB120	0.28	2.5	No
17ASB220	0.35	2.5	No
17ASB320	0.25	2.5	No
17ASB122	0.3	2.5	No
17ASB225	0.32	2.5	No
17ASB325	0.25	2.5	No
17ASB340	0.25	2.5	No

Silver horizon B

Poisson-based Tolerance Limit (K) Calculation for Silver soil horizon B, SWMU 17A

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

 $T_n =$ Poisson count of background $n =$ Background sample size $\alpha =$ Probability level test is conducted at (here, 0.05) T_n 0.18 $2T_n+2$ 2.36Chi Square $(2T_n+2)$ 6.67165 n 8Lambda T_n 0.4169781 $2(\text{Lambda } T_n)$ 0.8339563Chi Square $0.05[2K+2] \geq$ 0.8339563 $[2K+2] = 5$ $K = 1.5$

FSampNo	Value	Limit	Limit Exceeded?
17ASB105	42.31	1.5	Yes
17ASB205	0.01	1.5	No
17ASB305	0.01	1.5	No

Silver horizon C

Poisson-based Tolerance Limit (K) Calculation for Silver soil horizon C, SWMU 17A

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

$T_n =$ Poisson count of background

$n =$ Background sample size

alpha = Probability level test is conducted at (here, 0.05)

T_n	0.215
$2T_n+2$	2.43
Chi Square ($2T_n+2$)	6.80037
n	8
Lambda T_n	0.4250231
$2(\text{Lambda } T_n)$	0.8500463
Chi Square $0.05[2K+2] \geq$	0.8500463
$[2K+2] = 5$	
$K = 1.5$	

FSampNo	Value	Limit	Limit Exceeded?
17ASB110	0.39	1.5	No
17ASB210	0.005	1.5	No
17ASB310	0.01	1.5	No
17ASB115	0.01	1.5	No
17ASB215	0.01	1.5	No
17ASB315	0.01	1.5	No
17ASB120	2.12	1.5	Yes
17ASB220	0.01	1.5	No
17ASB320	0.005	1.5	No
17ASB122	0.01	1.5	No
17ASB225	0.01	1.5	No
17ASB325	0.005	1.5	No
17ASB340	0.005	1.5	No

Thallium Horizon B

Poisson-based Tolerance Limit (K) Calculation for Thallium soil horizon B, SWMU 17A

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

 $T_n =$ Poisson count of background $n =$ Background sample size $\alpha =$ Probability level test is conducted at (here, 0.05)

T_n	176.62
$2T_n+2$	355.24
Chi Square ($2T_n+2$)	400.19
n	8
Lambda T_n	25.011875
$2(\text{Lambda } T_n)$	50.02375
Chi Square 0.05 $[2K+2] \geq$	50.02375
$[2K+2] =$	69
$K =$	33.5

FSampNo	Value	Limit	Limit Exceeded?
17ASB105	21.99	33.5	No
17ASB205	21.36	33.5	No
17ASB305	25.95	33.5	No

Thallium horizon C

Poisson-based Tolerance Limit (K) Calculation for Thallium soil horizon C

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

$T_n =$ Poisson count of background

$n =$ Background sample size

alpha = Probability level test is conducted at (here, 0.05)

T_n	177.36
$2T_n+2$	356.72
Chi Square ($2T_n+2$)	401.762
n	8
Lambda T_n	25.110125
$2(\text{Lambda } T_n)$	50.22025
Chi Square 0.05 $[2K+2] \geq$	50.22025
$[2K+2] = 69$	
$K = 33.5$	

FSampNo	Value	Limit	Limit Exceeded?
17ASB110	21.74	33.5	No
17ASB210	20.59	33.5	No
17ASB310	25.15	33.5	No
17ASB115	21.05	33.5	No
17ASB215	24.68	33.5	No
17ASB315	23.40	33.5	No
17ASB120	21.36	33.5	No
17ASB220	26.35	33.5	No
17ASB320	18.85	33.5	No
17ASB122	22.42	33.5	No
17ASB225	24.57	33.5	No
17ASB325	18.81	33.5	No
17ASB340	18.83	33.5	No

Antimony soil B

Poisson-based Tolerance Limit (K) Calculation for Antimony soil horizon B, SWMU 17BCD

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of Tn})$

Where

Lambda of Tn = $(1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2Tn+2))$

Where

Tn = Poisson count of background

n = Background sample size

alpha = Probability level test is conducted at (here, 0.05)

Tn	100.94
2Tn+2	203.88
Chi Square (2Tn+2)	238.191
n	8
Lambda Tn	14.886938
2(Lambda Tn)	29.773875
Chi Square 0.05[2K+2] ≥	29.773875
[2K+2] =	44
K =	21

FSampNo	Value	Limit	Limit Exceeded?
17CSB105	12.06	21	No
17CSB205	12.22	21	No
17DSB105	12.53	21	No
17DSB205	12.07	21	No

Antimony soil C

Poisson-based Tolerance Limit (K) Calculation for Antimony soil horizon C, SWMU 17BCD

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

 $T_n =$ Poisson count of background $n =$ Background sample size $\alpha =$ Probability level test is conducted at (here, 0.05)

T_n	101.34
$2T_n+2$	204.68
Chi Square ($2T_n+2$)	239.056
n	8
Lambda T_n	14.941
$2(\text{Lambda } T_n)$	29.882
Chi Square $0.05[2K+2] \geq$	29.882
$[2K+2] = 45$	
$K = 21.5$	

FSampNo	Value	Limit	Limit Exceeded?
17CSB110	13.39	21.5	No
17CSB210	14.50	21.5	No
17DSB110	12.13	21.5	No
17DSB210	12.60	21.5	No
17CSB114	13.02	21.5	No
17CSB215	12.45	21.5	No
17DSB115	12.57	21.5	No
17DSB215	15.83	21.5	No
17DSB120	13.09	21.5	No
17DSB220	15.99	21.5	No
17DSB125	15.63	21.5	No
17DSB225	13.88	21.5	No
17DSB127	16.31	21.5	No
17CSB240	15.22	21.5	No
17DSB240	12.36	21.5	No

Arsenic horizon B

Poisson-based Tolerance Limit (K) Calculation for Arsenic soil horizon B, SWMU 17BCD

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of Tn})$

Where

Lambda of Tn = $(1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2Tn+2))$

Where

Tn = Poisson count of background

n = Background sample size

alpha = Probability level test is conducted at (here, 0.05)

Tn 55.13

2Tn+2 112.26

Chi Square (2Tn+2) 137.988

n 8

Lambda Tn 8.62425

2(Lambda Tn) 17.2485

Chi Square 0.05 $[2K+2] \geq$ 17.2485 $[2K+2] = 13$

K = 5.5

FSampNo	Value	Limit	Limit Exceeded?
17CSB105	11.98	5.5	Yes
17CSB205	1.56	5.5	No
17DSB105	1.60	5.5	No
17DSB205	1.54	5.5	No

Arsenic horizon C

Poisson-based Tolerance Limit (K) Calculation for Arsenic soil horizon C, SWMU 17BCD

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

 $T_n =$ Poisson count of background $n =$ Background sample size

alpha = Probability level test is conducted at (here, 0.05)

 T_n 43.70 $2T_n+2$ 89.40Chi Square $(2T_n+2)$ 112.471 n 8Lambda T_n 7.0294375 $2(\text{Lambda } T_n)$ 14.058875Chi Square $0.05[2K+2] \geq$ 14.058875 $[2K+2] = 25$

K = 11.5

FSampNo	Value	Limit	Limit Exceeded?
17CSB110	1.71	11.5	No
17CSB210	1.85	11.5	No
17DSB110	1.55	11.5	No
17DSB210	6.32	11.5	No
17CSB114	1.66	11.5	No
17CSB215	4.59	11.5	No
17DSB115	1.61	11.5	No
17DSB215	11.32	11.5	No
17DSB120	1.67	11.5	No
17DSB220	2.04	11.5	No
17DSB125	1.50	11.5	No
17DSB225	1.77	11.5	No
17DSB127	2.08	11.5	No
17CSB240	1.94	11.5	No
17DSB240	8.03	11.5	No

Barium horizon B

Normal Tolerance Limit (K) Calculation for Barium soil horizon B, SWMU 17BCD

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	4.39
Where		std. dev.	0.83
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	6.399951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17CSB105	3.38	9.7019594	29.40	16349.61	No
17CSB205	3.60	9.7019594	36.74	16349.61	No
17DSB105	4.23	9.7019594	68.93	16349.61	No
17DSB205	4.19	9.7019594	65.89	16349.61	No

Barium horizon C

Normal Tolerance Limit (K) Calculation for Barium soil horizon C, SWMU 17BCD

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	4.51
Where		std. dev.	0.37
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	6.519951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17CSB110	4.36	6.9223819	78.55	1014.7341	No
17CSB210	4.25	6.9223819	70.12	1014.7341	No
17DSB110	4.10	6.9223819	60.40	1014.7341	No
17DSB210	4.39	6.9223819	80.98	1014.7341	No
17CSB114	4.43	6.9223819	84.33	1014.7341	No
17CSB215	4.65	6.9223819	104.70	1014.7341	No
17DSB115	4.21	6.9223819	67.05	1014.7341	No
17DSB215	4.96	6.9223819	142.65	1014.7341	No
17DSB120	4.24	6.9223819	69.69	1014.7341	No
17DSB220	4.72	6.9223819	111.91	1014.7341	No
17DSB125	4.29	6.9223819	72.73	1014.7341	No
17DSB225	4.02	6.9223819	55.95	1014.7341	No
17DSB127	4.71	6.9223819	111.48	1014.7341	No
17CSB240	4.46	6.9223819	86.49	1014.7341	No
17DSB240	4.23	6.9223819	68.85	1014.7341	No

Beryllium horizon B

Poisson-based Tolerance Limit (K) Calculation for Beryllium soil horizon B, SWMU 17BCD

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

$T_n =$ Poisson count of background

$n =$ Background sample size

$\alpha =$ Probability level test is conducted at (here, 0.05)

T_n 10.67

$2T_n+2$ 23.34

Chi Square ($2T_n+2$) 35.5955

n 8

Lambda T_n 2.2247188

$2(\text{Lambda } T_n)$ 4.4494375

Chi Square $0.05[2K+2] \geq$ 4.4494375

$[2K+2] = 11$

$K = 4.5$

FSampNo	Value	Limit	Limit Exceeded?
17CSB105	3.23	4.5	No
17CSB205	1.56	4.5	No
17DSB105	1.83	4.5	No
17DSB205	1.42	4.5	No

Beryllium horizon C

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Normal Tolerance Limit (K) Calculation for Beryllium soil horizon C, SWMU 17BCD

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	0.70
Where		std. dev.	0.59
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	2.709951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17CSB110	1.65	2.2988711	5.19	9.962929	No
17CSB210	1.75	2.2988711	5.77	9.962929	No
17DSB110	0.70	2.2988711	2.02	9.962929	No
17DSB210	0.91	2.2988711	2.48	9.962929	No
17CSB114	1.28	2.2988711	3.61	9.962929	No
17CSB215	0.92	2.2988711	2.52	9.962929	No
17DSB115	1.16	2.2988711	3.21	9.962929	No
17DSB215	2.06	2.2988711	7.88	9.962929	No
17DSB120	1.11	2.2988711	3.04	9.962929	No
17DSB220	1.70	2.2988711	5.48	9.962929	No
17DSB125	1.56	2.2988711	4.77	9.962929	No
17DSB225	2.47	2.2988711	11.84	9.962929	Yes
17DSB127	1.77	2.2988711	5.89	9.962929	No
17CSB240	1.83	2.2988711	6.21	9.962929	No
17DSB240	0.80	2.2988711	2.23	9.962929	No

Cadmium horizon B

Poisson-based Tolerance Limit (K) Calculation for Cadmium soil horizon B, SWMU 17BCD

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

$T_n =$ Poisson count of background

$n =$ Background sample size

$\alpha =$ Probability level test is conducted at (here, 0.05)

T_n 6.2

$2T_n+2$ 14.40

Chi Square $(2T_n+2)$ 24.2105

n 8

Lambda T_n 1.5131563

$2(\text{Lambda } T_n)$ 3.0263125

Chi Square $0.05[2K+2] \geq$ 3.0263125

$[2K+2] = 9$

$K = 3.5$

FSampNo	Value	Limit	Limit Exceeded?
17CSB105	0.74	3.5	No
17CSB205	0.75	3.5	No
17DSB105	0.77	3.5	No
17DSB205	0.74	3.5	No

Poisson-based Tolerance Limit (K) Calculation for Cadmium soil horizon C, SWMU 17BCD

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

 $T_n =$ Poisson count of background $n =$ Background sample size $\alpha =$ Probability level test is conducted at (here, 0.05)

T_n	6.23
$2T_n+2$	14.46
Chi Square ($2T_n+2$)	24.2892
n	8
Lambda T_n	1.518075
$2(\text{Lambda } T_n)$	3.03615
Chi Square $0.05[2K+2] \geq$	3.03615
$[2K+2] = 9$	
$K = 3.5$	

FSampNo	Value	Limit	Limit Exceeded?
17CSB110	0.82	3.5	No
17CSB210	0.89	3.5	No
17DSB110	0.75	3.5	No
17DSB210	0.77	3.5	No
17CSB114	0.80	3.5	No
17CSB215	4.73	3.5	Yes
17DSB115	0.77	3.5	No
17DSB215	0.97	3.5	No
17DSB120	0.80	3.5	No
17DSB220	0.98	3.5	No
17DSB125	0.96	3.5	No
17DSB225	0.85	3.5	No
17DSB127	1.00	3.5	No
17CSB240	0.93	3.5	No
17DSB240	0.76	3.5	No

Chromium horizon B

358

Normal Tolerance Limit (K) Calculation for Chromium soil horizon B, SWMU 17BCD

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	3.82
Where		std. dev.	0.22
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	5.829951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17CSB105	4.13	5.1025892	61.87	164.44715	No
17CSB205	3.52	5.1025892	33.62	164.44715	No
17DSB105	3.40	5.1025892	29.92	164.44715	No
17DSB205	3.44	5.1025892	31.28	164.44715	No

Chromium horizon C

359

Normal Tolerance Limit (K) Calculation for Chromium soil horizon C, SWMU 17A

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	3.83
Where		std. dev.	0.2
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	5.839951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17CSB110	4.29	4.9979902	72.81	148.11518	No
17CSB210	3.99	4.9979902	54.29	148.11518	No
17DSB110	3.78	4.9979902	43.94	148.11518	No
17DSB210	4.03	4.9979902	56.30	148.11518	No
17CSB114	4.09	4.9979902	59.89	148.11518	No
17CSB215	4.28	4.9979902	71.92	148.11518	No
17DSB115	4.22	4.9979902	67.82	148.11518	No
17DSB215	4.58	4.9979902	97.09	148.11518	No
17DSB120	4.03	4.9979902	56.07	148.11518	No
17DSB220	4.15	4.9979902	63.30	148.11518	No
17DSB125	4.47	4.9979902	86.92	148.11518	No
17DSB225	4.35	4.9979902	77.76	148.11518	No
17DSB127	4.36	4.9979902	77.87	148.11518	No
17CSB240	4.31	4.9979902	74.38	148.11518	No
17DSB240	3.90	4.9979902	49.18	148.11518	No

Lead horizon B

Normal Tolerance Limit (K) Calculation for Lead soil horizon B, SWMU 17BCD

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	3.24
Where		std. dev.	1.04
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	5.249951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17CSB105	3.73	8.6999491	41.82	6002.6065	No
17CSB205	2.50	8.6999491	12.20	6002.6065	No
17DSB105	3.00	8.6999491	20.08	6002.6065	No
17DSB205	3.04	8.6999491	20.81	6002.6065	No

Normal Tolerance Limit (K) Calculation for Lead soil horizon C, SWMU 17BCD

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	2.71
Where		std. dev.	0.31
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	4.719951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17CSB110	2.91	4.1731848	18.44	64.921888	No
17CSB210	2.62	4.1731848	13.68	64.921888	No
17DSB110	2.89	4.1731848	17.95	64.921888	No
17DSB210	2.88	4.1731848	17.87	64.921888	No
17CSB114	2.93	4.1731848	18.73	64.921888	No
17CSB215	5.25	4.1731848	190.60	64.921888	Yes
17DSB115	3.28	4.1731848	26.54	64.921888	No
17DSB215	3.14	4.1731848	23.10	64.921888	No
17DSB120	2.51	4.1731848	12.36	64.921888	No
17DSB220	2.43	4.1731848	11.31	64.921888	No
17DSB125	3.34	4.1731848	28.23	64.921888	No
17DSB225	2.13	4.1731848	8.43	64.921888	No
17DSB127	3.16	4.1731848	23.46	64.921888	No
17CSB240	2.85	4.1731848	17.24	64.921888	No
17DSB240	2.68	4.1731848	14.63	64.921888	No

Mercury horizon B

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Poisson-based Tolerance Limit (K) Calculation for Mercury soil horizon B, SWMU 17BCD

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

$T_n =$ Poisson count of background

$n =$ Background sample size

alpha = Probability level test is conducted at (here, 0.05)

T_n 0.76

$2T_n+2$ 3.52

Chi Square ($2T_n+2$) 8.69852

n 8

Lambda T_n 0.5436575

$2(\text{Lambda } T_n)$ 1.087315

Chi Square $0.05[2K+2] \geq$ 1.087315

$[2K+2] = 5$

$K = 1.5$

FSampNo	Value	Limit	Limit Exceeded?
17CSB105	0.03	1.5	No
17CSB205	0.03	1.5	No
17DSB105	0.03	1.5	No
17DSB205	0.03	1.5	No

Poisson-based Tolerance Limit (K) Calculation for Mercury soil horizon C, SWMU 17BCD

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

 $T_n =$ Poisson count of background $n =$ Background sample size $\alpha =$ Probability level test is conducted at (here, 0.05) T_n 0.63 $2T_n+2$ 3.26Chi Square $(2T_n+2)$ 8.26084 n 8Lambda T_n 0.5163025 $2(\text{Lambda } T_n)$ 1.032605Chi Square $0.05[2K+2] \geq$ 1.032605 $[2K+2] = 5$ $K = 1.5$

FSampNo	Value	Limit	Limit Exceeded?
17CSB110	0.10	1.5	No
17CSB210	0.04	1.5	No
17DSB110	0.03	1.5	No
17DSB210	0.03	1.5	No
17CSB114	0.04	1.5	No
17CSB215	0.03	1.5	No
17DSB115	0.03	1.5	No
17DSB215	0.24	1.5	No
17DSB120	0.04	1.5	No
17DSB220	0.04	1.5	No
17DSB125	0.04	1.5	No
17DSB225	0.04	1.5	No
17DSB127	0.15	1.5	No
17CSB240	0.04	1.5	No
17DSB240	0.03	1.5	No

Nickel horizon B

Normal Tolerance Limit (K) Calculation for Nickel soil horizon B, SWMU 17BCD

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	2.97
Where		std. dev.	0.61
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	4.979951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17CSB105	3.26	6.0077701	25.95	406.5757	No
17CSB205	2.93	6.0077701	18.68	406.5757	No
17DSB105	2.68	6.0077701	14.58	406.5757	No
17DSB205	2.41	6.0077701	11.18	406.5757	No

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Nickel horizon C

Normal Tolerance Limit (K) Calculation for Nickel soil horizon C, SWMU 17BCD

K =average+ t((N-1),alpha)*SQRT(1+(1/N))		average	3.24
Where		std. dev.	0.42
t =	Critical value of Student's t distribution	t	1.895
N =	Sample size	N	8
alpha =	Probability level test is conducted at (here, 0.05)	K	5.249951

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
17CSB110	3.83	5.4449794	46.17	231.59252	No
17CSB210	3.84	5.4449794	46.60	231.59252	No
17DSB110	2.79	5.4449794	16.21	231.59252	No
17DSB210	3.36	5.4449794	28.79	231.59252	No
17CSB114	3.56	5.4449794	35.33	231.59252	No
17CSB215	3.82	5.4449794	45.62	231.59252	No
17DSB115	3.37	5.4449794	28.97	231.59252	No
17DSB215	4.28	5.4449794	72.05	231.59252	No
17DSB120	3.82	5.4449794	45.53	231.59252	No
17DSB220	4.05	5.4449794	57.42	231.59252	No
17DSB125	3.92	5.4449794	50.40	231.59252	No
17DSB225	4.48	5.4449794	87.82	231.59252	No
17DSB127	4.20	5.4449794	66.39	231.59252	No
17CSB240	4.04	5.4449794	56.83	231.59252	No
17DSB240	3.15	5.4449794	23.33	231.59252	No

Selenium horizon B

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Poisson-based Tolerance Limit (K) Calculation for Selenium soil horizon B, SWMU 17BCD

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of Tn})$

Where

Lambda of Tn = $(1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2Tn+2))$

Where

Tn = Poisson count of background

n = Background sample size

alpha = Probability level test is conducted at (here, 0.05)

Tn	2.34
2Tn+2	6.68
Chi Square (2Tn+2)	13.5992
n	8
Lambda Tn	0.84995
2(Lambda Tn)	1.6999
Chi Square 0.05[2K+2] $\geq$	1.6999
[2K+2] =	7
K =	2.5

FSampNo	Value	Limit	Limit Exceeded?
17CSB105	0.28	2.5	No
17CSB205	0.28	2.5	No
17DSB105	0.29	2.5	No
17DSB205	0.28	2.5	No

Poisson-based Tolerance Limit (K) Calculation for Silver soil horizon C, SWMU 17BCD

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of Tn})$

Where

Lambda of Tn = $(1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2Tn+2))$

Where

Tn = Poisson count of background

n = Background sample size

alpha = Probability level test is conducted at (here, 0.05)

Tn 2.34

2Tn+2 6.68

Chi Square (2Tn+2) 13.5992

n 8

Lambda Tn 0.84995

2(Lambda Tn) 1.6999

Chi Square 0.05 $[2K+2] \geq$ 1.6999 $[2K+2] = 7$

K = 2.5

FSampNo	Value	Limit	Limit Exceeded?
17CSB110	0.30	2.5	No
17CSB210	0.33	2.5	No
17DSB110	0.28	2.5	No
17DSB210	0.29	2.5	No
17CSB114	0.30	2.5	No
17CSB215	0.29	2.5	No
17DSB115	0.29	2.5	No
17DSB215	0.37	2.5	No
17DSB120	0.30	2.5	No
17DSB220	0.37	2.5	No
17DSB125	0.36	2.5	No
17DSB225	0.32	2.5	No
17DSB127	0.38	2.5	No
17CSB240	0.35	2.5	No
17DSB240	0.29	2.5	No

Silver horizon B

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Poisson-based Tolerance Limit (K) Calculation for Silver soil horizon B, SWMU 17BCD

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

$T_n =$ Poisson count of background

$n =$ Background sample size

alpha = Probability level test is conducted at (here, 0.05)

T_n	0.18
$2T_n+2$	2.36
Chi Square ($2T_n+2$)	6.67165
n	8
Lambda T_n	0.4169781
$2(\text{Lambda } T_n)$	0.8339563
Chi Square $0.05[2K+2] \geq$	0.8339563
$[2K+2] = 5$	
$K = 1.5$	

FSampNo	Value	Limit	Limit Exceeded?
17CSB105	0.01	1.5	No
17CSB205	0.01	1.5	No
17DSB105	0.03	1.5	No
17DSB205	0.01	1.5	No

Silver horizon C

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Poisson-based Tolerance Limit (K) Calculation for Silver soil horizon C, SWMU 17BCD

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of Tn})$

Where

Lambda of Tn = $(1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2Tn+2))$

Where

Tn = Poisson count of background

n = Background sample size

alpha = Probability level test is conducted at (here, 0.05)

Tn	0.215
2Tn+2	2.43
Chi Square (2Tn+2)	6.80037
n	8
Lambda Tn	0.4250231
2(Lambda Tn)	0.8500463
Chi Square 0.05[2K+2] $\geq$	0.8500463
[2K+2] = 5	
K = 1.5	

FSampNo	Value	Limit	Limit Exceeded?
17CSB110	0.01	1.5	No
17CSB210	0.01	1.5	No
17DSB110	0.01	1.5	No
17DSB210	0.01	1.5	No
17CSB114	0.01	1.5	No
17CSB215	0.04	1.5	No
17DSB115	0.01	1.5	No
17DSB215	0.01	1.5	No
17DSB120	0.01	1.5	No
17DSB220	0.01	1.5	No
17DSB125	0.01	1.5	No
17DSB225	0.01	1.5	No
17DSB127	0.07	1.5	No
17CSB240	0.01	1.5	No
17DSB240	0.01	1.5	No

Thallium Horizon B

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Poisson-based Tolerance Limit (K) Calculation for Thallium soil horizon B, SWMU 17BCD

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of Tn})$

Where

Lambda of Tn = $(1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2Tn+2))$

Where

Tn = Poisson count of background

n = Background sample size

alpha = Probability level test is conducted at (here, 0.05)

Tn	176.62
2Tn+2	355.24
Chi Square (2Tn+2)	400.19
n	8
Lambda Tn	25.011875
2(Lambda Tn)	50.02375
Chi Square 0.05 $[2K+2] \geq$	50.02375
$[2K+2] = 69$	
K = 33.5	

FSampNo	Value	Limit	Limit Exceeded?
17CSB105	21.10	33.5	No
17CSB205	21.36	33.5	No
17DSB105	21.93	33.5	No
17DSB205	21.12	33.5	No

Thallium horizon C

Poisson-based Tolerance Limit (K) Calculation for Thallium soil horizon C, SWMU 17BCD

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

 $T_n =$ Poisson count of background $n =$ Background sample size $\alpha =$ Probability level test is conducted at (here, 0.05) T_n 177.36 $2T_n+2$ 356.72Chi Square ($2T_n+2$) 401.761 n 8Lambda T_n 25.110063 $2(\text{Lambda } T_n)$ 50.220125Chi Square $0.05[2K+2] \geq$ 50.220125 $[2K+2] = 69$

K = 33.5

FSampNo	Value	Limit	Limit Exceeded?
17CSB110	23.43	33.5	No
17CSB210	25.37	33.5	No
17DSB110	21.23	33.5	No
17DSB210	22.10	33.5	No
17CSB114	22.78	33.5	No
17CSB215	21.79	33.5	No
17DSB115	21.99	33.5	No
17DSB215	27.71	33.5	No
17DSB120	22.90	33.5	No
17DSB220	27.98	33.5	No
17DSB125	27.35	33.5	No
17DSB225	24.29	33.5	No
17DSB127	28.54	33.5	No
17CSB240	26.63	33.5	No
17DSB240	21.63	33.5	No

Antimony horizon C

Poisson-based Tolerance Limit (K) Calculation for Antimony soil horizon C, SWMU 31

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

 $T_n =$ Poisson count of background $n =$ Background sample size $\alpha =$ Probability level test is conducted at (here, 0.05)

T_n	69.27
$2T_n+2$	140.54
Chi Square ($2T_n+2$)	169.204
n	6
Lambda T_n	14.100333
$2(\text{Lambda } T_n)$	28.200667
Chi Square $0.05[2K+2] \geq$	28.200667
$[2K+2] = 43$	
$K = 20.5$	

FSampNo	Value	Limit	Limit Exceeded?
31MW3A1	9.80	20.5	No
31MW2A	12.13	20.5	No
31MW4A1	11.27	20.5	No
31MW3B2	9.80	20.5	No
31MW2B	10.89	20.5	No
31MW4B2	10.61	20.5	No
31MW1A2	10.24	20.5	No
31MW1B3	10.41	20.5	No
31MW4C4	11.38	20.5	No

Arsenic horizon C

Poisson-based Tolerance Limit (K) Calculation for Arsenic soil horizon C, SWMU 31

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

 $T_n =$ Poisson count of background $n =$ Background sample size $\alpha =$ Probability level test is conducted at (here, 0.05) T_n 14.26 $2T_n+2$ 30.52Chi Square ($2T_n+2$) 44.4038 n 6Lambda T_n 3.7003167 $2(\text{Lambda } T_n)$ 7.4006333Chi Square $0.05[2K+2] \geq$ 7.4006333 $[2K+2] = 16$ $K = 7$

FSampNo	Value	Limit	Limit Exceeded?
31MW3A1	1.46	7	No
31MW2A	1.55	7	No
31MW4A1	1.44	7	No
31MW3B2	1.39	7	No
31MW2B	4.40	7	No
31MW4B2	1.36	7	No
31MW1A2	1.31	7	No
31MW1B3	1.33	7	No
31MW4C4	1.45	7	No

Barium horizon C

Normal Tolerance Limit (K) Calculation for Barium soil horizon C, SWMU 31

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	4.53
Where		std. dev.	0.38
t =	Critical value of Student's t distribution	t	2.015
N =	Sample size	N	6
alpha =	Probability level test is conducted at (here, 0.05)	K	6.7064488

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
31MW3A1	4.90	7.0784505	134.00	1186.1292	No
31MW2A	4.90	7.0784505	134.90	1186.1292	No
31MW4A1	4.92	7.0784505	136.78	1186.1292	No
31MW3B2	4.32	7.0784505	75.10	1186.1292	No
31MW2B	4.58	7.0784505	97.33	1186.1292	No
31MW4B2	4.42	7.0784505	82.68	1186.1292	No
31MW1A2	3.34	7.0784505	28.11	1186.1292	No
31MW1B3	4.07	7.0784505	58.39	1186.1292	No
31MW4C4	4.95	7.0784505	140.53	1186.1292	No

Beryllium C

Normal Tolerance Limit (K) Calculation for Beryllium soil horizon C, SWMU 31

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	-0.09993
Where		std. dev.	0.27
t =	Critical value of Student's t distribution	t	2.015
N =	Sample size	N	6
alpha =	Probability level test is conducted at (here, 0.05)	K	2.0765188

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
31MW3A1	-0.05	0.4607301	0.95	1	No
31MW2A	0.00	0.4607301	1.00	1	Yes
31MW4A1	0.17	0.4607301	1.18	1	Yes
31MW3B2	-0.29	0.4607301	0.75	1	No
31MW2B	0.06	0.4607301	1.06	1	Yes
31MW4B2	-0.19	0.4607301	0.83	1	No
31MW1A2	-0.06	0.4607301	0.94	1	No
31MW1B3	0.16	0.4607301	1.18	1	Yes
31MW4C4	0.20	0.4607301	1.22	1	Yes

Cadmium horizon C

Poisson-based Tolerance Limit (K) Calculation for Cadmium soil horizon C, SWMU 31

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

 $T_n =$ Poisson count of background $n =$ Background sample size $\alpha =$ Probability level test is conducted at (here, 0.05) T_n 4.21 $2T_n+2$ 10.42Chi Square $(2T_n+2)$ 18.8839 n 6Lambda T_n 1.5736583 $2(\text{Lambda } T_n)$ 3.1473167Chi Square $0.05[2K+2] \geq$ 3.1473167 $[2K+2] = 9$ $K = 3.5$

FSampNo	Value	Limit	Limit Exceeded?
31MW3A1	0.60	3.5	No
31MW2A	0.75	3.5	No
31MW4A1	0.69	3.5	No
31MW3B2	0.60	3.5	No
31MW2B	0.67	3.5	No
31MW4B2	0.65	3.5	No
31MW1A2	0.63	3.5	No
31MW1B3	0.64	3.5	No
31MW4C4	0.70	3.5	No

Chromium horizon C

Normal Tolerance Limit (K) Calculation for Chromium soil horizon C, SWMU 31

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	3.55
Where		std. dev.	0.22
t =	Critical value of Student's t distribution	t	2.015
N =	Sample size	N	6
alpha =	Probability level test is conducted at (here, 0.05)	K	5.7264488

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
31MW3A1	3.29	4.8098187	26.80	122.70937	No
31MW2A	3.78	4.8098187	43.94	122.70937	No
31MW4A1	3.78	4.8098187	43.91	122.70937	No
31MW3B2	2.97	4.8098187	19.50	122.70937	No
31MW2B	3.53	4.8098187	34.00	122.70937	No
31MW4B2	3.47	4.8098187	32.03	122.70937	No
31MW1A2	2.92	4.8098187	18.50	122.70937	No
31MW1B3	3.18	4.8098187	24.10	122.70937	No
31MW4C4	3.79	4.8098187	44.13	122.70937	No

Lead horizon C

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Normal Tolerance Limit (K) Calculation for Lead soil horizon C, SWMU 31

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	2.77
Where		std. dev.	0.26
t =	Critical value of Student's t distribution	t	2.015
N =	Sample size	N	6
alpha =	Probability level test is conducted at (here, 0.05)	K	4.9464488

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
31MW3A1	3.45	4.0560767	31.54	57.747305	No
31MW2A	3.05	4.0560767	21.16	57.747305	No
31MW4A1	2.87	4.0560767	17.70	57.747305	No
31MW3B2	3.69	4.0560767	40.00	57.747305	No
31MW2B	3.04	4.0560767	20.86	57.747305	No
31MW4B2	2.64	4.0560767	13.96	57.747305	No
31MW1A2	-0.46	4.0560767	0.63	57.747305	No
31MW1B3	1.99	4.0560767	7.32	57.747305	No
31MW4C4	2.99	4.0560767	19.98	57.747305	No

Mercury horizon C

379

Poisson-based Tolerance Limit (K) Calculation for Mercury soil horizon C, SWMU 31

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

$T_n =$ Poisson count of background

$n =$ Background sample size

$\alpha =$ Probability level test is conducted at (here, 0.05)

T_n 0.31

$2T_n+2$ 2.62

Chi Square $(2T_n+2)$ 7.14479

n 6

Lambda T_n 0.5953992

$2(\text{Lambda } T_n)$ 1.1907983

Chi Square $0.05[2K+2] \geq$ 1.1907983

$[2K+2] = 6$

$K = 2$

FSampNo	Value	Limit	Limit Exceeded?
31MW3A1	0.18	2	No
31MW2A	0.03	2	No
31MW4A1	0.03	2	No
31MW3B2	0.03	2	No
31MW2B	0.07	2	No
31MW4B2	0.03	2	No
31MW1A2	0.03	2	No
31MW1B3	0.03	2	No
31MW4C4	0.03	2	No

Nickel horizon C

380

Normal Tolerance Limit (K) Calculation for Nickel soil horizon C, SWMU 31

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	2.69
Where		std. dev.	0.34
t =	Critical value of Student's t distribution	t	2.015
N =	Sample size	N	6
alpha =	Probability level test is conducted at (here, 0.05)	K	4.8664488

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
31MW3A10	2.53	4.3445926	12.60	77.060635	No
31MW2A	2.59	4.3445926	13.37	77.060635	No
31MW4A12	3.01	4.3445926	20.23	77.060635	No
31MW3B20	2.59	4.3445926	13.30	77.060635	No
31MW2B	3.13	4.3445926	22.78	77.060635	No
31MW4B22	2.90	4.3445926	18.18	77.060635	No
31MW1A25	3.16	4.3445926	23.62	77.060635	No
31MW1B35	3.43	4.3445926	30.89	77.060635	No
31MW4C40	3.07	4.3445926	21.49	77.060635	No

Poisson-based Tolerance Limit (K) Calculation for Selenium soil horizon C, SWMU 31

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

$T_n =$ Poisson count of background

$n =$ Background sample size

$\alpha =$ Probability level test is conducted at (here, 0.05)

T_n 1.61

$2T_n+2$ 5.22

Chi Square (2 11.4097

n 6

Lambda T_n 0.950808333

$2(\text{Lambda } T_n)$ 1.901616667

Chi Square 0.0 1.901616667

$[2K+2] = 7$

$K = 2.5$

FSampNo	Value	Limit	Limit Exceeded?
31MW3A10	0.26	2.5	No
31MW2A	0.28	2.5	No
31MW4A12	0.26	2.5	No
31MW3B20	0.25	2.5	No
31MW2B	0.27	2.5	No
31MW4B22	0.25	2.5	No
31MW1A25	0.24	2.5	No
31MW1B35	0.24	2.5	No
31MW4C40	0.26	2.5	No

Poisson-based Tolerance Limit (K) Calculation for Silver soil horizon C, SWMU 31

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

$T_n =$ Poisson count of background

$n =$ Background sample size

alpha = Probability level test is conducted at (here, 0.05)

T_n 0.04

$2T_n+2$ 2.08

Chi Square $(2T_n+2)$ 6.1455

n 6

Lambda T_n 0.512125

$2(\text{Lambda } T_n)$ 1.02425

Chi Square $0.05[2K+2] \geq$ 1.02425

$[2K+2] = 5$

$K = 1.5$

FSampNo	Value	Limit	Limit Exceeded?
31MW3A1	0.005	1.5	No
31MW2A	0.01	1.5	No
31MW4A1	0.005	1.5	No
31MW3B2	0.11	1.5	No
31MW2B	0.005	1.5	No
31MW4B2	0.005	1.5	No
31MW1A2	0.005	1.5	No
31MW1B3	0.01	1.5	No
31MW4C4	0.005	1.5	No

Poisson-based Tolerance Limit (K) Calculation for Thallium soil horizon C, SWMU 31

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

$T_n =$ Poisson count of background

$n =$ Background sample size

$\alpha =$ Probability level test is conducted at (here, 0.05)

T_n	121.19
$2T_n+2$	244.38
Chi Square ($2T_n+2$)	281.844
n	6
Lambda T_n	23.487
$2(\text{Lambda } T_n)$	46.974
Chi Square $0.05[2K+2] \geq$	46.974
$[2K+2] = 65$	
$K = 31.5$	

FSampNo	Value	Limit	Limit Exceeded?
31MW3A1	17.15	31.5	No
31MW2A	21.23	31.5	No
31MW4A1	19.72	31.5	No
31MW3B2	17.15	31.5	No
31MW2B	19.06	31.5	No
31MW4B2	18.56	31.5	No
31MW1A2	17.92	31.5	No
31MW1B3	18.22	31.5	No
31MW4C4	19.92	31.5	No

Antimony horizon B

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Poisson-based Tolerance Limit (K) Calculation for Antimony soil horizon B, SWMU 54

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

$T_n =$ Poisson count of background

$n =$ Background sample size

$\alpha =$ Probability level test is conducted at (here, 0.05)

T_n	70.65
$2T_n+2$	143.30
Chi Square ($2T_n+2$)	172.234
n	6
Lambda T_n	14.352833
$2(\text{Lambda } T_n)$	28.705667
Chi Square $0.05[2K+2] \geq$	28.705667
$[2K+2] = 43$	
$K = 20.5$	

FSampNo	Value	Limit	Limit Exceeded?
54SB10A	11.85	20.5	No
54SB11A	11.91	20.5	No
54SB12A	12.24	20.5	No
54SB13A	12.03	20.5	No
54SB14A	11.56	20.5	No
54SB16A	12	20.5	No
54SB1A	11.52	20.5	No
54SB2A	10.99	20.5	No
54SB3A	11.27	20.5	No
54SB4A	12.15	20.5	No
54SB5A	12.22	20.5	No
54SB6A	11.93	20.5	No
54SB7A	11.2	20.5	No
54SB8A	11.85	20.5	No

Antimony horizon C

385

Poisson-based Tolerance Limit (K) Calculation for Antimony soil horizon C, SWMU 54

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

$T_n =$ Poisson count of background

$n =$ Background sample size

alpha = Probability level test is conducted at (here, 0.05)

T_n	69.27
$2T_n+2$	140.54
Chi Square ($2T_n+2$)	169.204
n	6
Lambda T_n	14.100333
$2(\text{Lambda } T_n)$	28.200667
Chi Square 0.05 $[2K+2] \geq$	28.200667
$[2K+2] = 43$	
$K = 20.5$	

FSampNo	Value	Limit	Limit Exceeded?
54SB15A	12.2	20.5	No
54SB9A	11.95	20.5	No
54SB16B	12.1	20.5	No
54SB14B	11.81	20.5	No
54SB6B	13.61	20.5	No
54SB10B	12.01	20.5	No
54SB11B	11.87	20.5	No
54SB12B	13.02	20.5	No
54SB2B	12.03	20.5	No
54SB3B	12.9	20.5	No
54SB4B	11.8	20.5	No
54SB5B	12.49	20.5	No
54SB7B	13.14	20.5	No
54SB8B	12.22	20.5	No
54SB9B	12.31	20.5	No
54SB10D	11.22	20.5	No
54SB13B	11.87	20.5	No
54SB1B	10.72	20.5	No
54SB16D	12.19	20.5	No

Arsenic horizon B

386

Poisson-based Tolerance Limit (K) Calculation for Arsenic soil horizon B, SWMU 54

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of Tn})$

Where

Lambda of Tn = $(1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2Tn+2))$

Where

Tn = Poisson count of background

n = Background sample size

alpha = Probability level test is conducted at (here, 0.05)

Tn	13.85
2Tn+2	29.70
Chi Square (2Tn+2)	43.4086
n	6
Lambda Tn	3.6173833
2(Lambda Tn)	7.2347667
Chi Square $_{0.05}[2K+2] \geq$	7.2347667
$[2K+2] = 15$	
K = 6.5	

FSampNo	Value	Limit	Limit Exceeded?
54SB10A	4.28	6.5	No
54SB11A	1.57	6.5	No
54SB12A	1.56	6.5	No
54SB13A	1.54	6.5	No
54SB14A	1.48	6.5	No
54SB16A	1.53	6.5	No
54SB1A	1.47	6.5	No
54SB2A	3.27	6.5	No
54SB3A	1.44	6.5	No
54SB4A	1.55	6.5	No
54SB5A	1.56	6.5	No
54SB6A	4.08	6.5	No
54SB7A	1.43	6.5	No
54SB8A	1.51	6.5	No

Poisson-based Tolerance Limit (K) Calculation for Arsenic soil horizon C, SWMU 54

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

$T_n =$ Poisson count of background

$n =$ Background sample size

alpha = Probability level test is conducted at (here, 0.05)

T_n	14.26
$2T_n+2$	30.52
Chi Square ($2T_n+2$)	44.4038
n	6
Lambda T_n	3.7003167
$2(\text{Lambda } T_n)$	7.4006333
Chi Square $0.05[2K+2] \geq$	7.4006333
$[2K+2] = 16$	
$K = 7$	

FSampNo	Value	Limit	Limit Exceeded?
54SB15A	1.55	7	No
54SB9A	1.53	7	No
54SB16B	1.55	7	No
54SB14B	1.51	7	No
54SB6B	1.74	7	No
54SB10B	1.53	7	No
54SB11B	1.52	7	No
54SB12B	1.66	7	No
54SB2B	1.54	7	No
54SB3B	1.65	7	No
54SB4B	1.51	7	No
54SB5B	1.59	7	No
54SB7B	1.68	7	No
54SB8B	1.56	7	No
54SB9B	1.57	7	No
54SB10D	1.43	7	No
54SB13B	1.52	7	No
54SB1B	1.37	7	No
54SB16D	1.56	7	No

Barium horizon B

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Normal Tolerance Limit (K) Calculation for Barium soil horizon B, SWMU 54

K = average + t((N-1), alpha) * SQRT(1 + (1/N))		average	4.95
Where		std. dev.	0.35
t =	Critical value of Student's t distribution	t	2.015
N =	Sample size	N	6
alpha =	Probability level test is conducted at (here, 0.05)	K	7.1264488

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
54SB10A	5.77	7.4442571	319.23	1710.0144	No
54SB11A	5.41	7.4442571	223.57	1710.0144	No
54SB12A	5.46	7.4442571	235.96	1710.0144	No
54SB13A	5.42	7.4442571	226.99	1710.0144	No
54SB14A	5.03	7.4442571	153.30	1710.0144	No
54SB16A	5.44	7.4442571	231.33	1710.0144	No
54SB1A	5.10	7.4442571	164.51	1710.0144	No
54SB2A	5.41	7.4442571	224.22	1710.0144	No
54SB3A	5.18	7.4442571	178.16	1710.0144	No
54SB4A	5.75	7.4442571	313.51	1710.0144	No
54SB5A	5.64	7.4442571	281.80	1710.0144	No
54SB6A	6.98	7.4442571	1077.02	1710.0144	No
54SB7A	4.93	7.4442571	138.29	1710.0144	No
54SB8A	5.24	7.4442571	188.63	1710.0144	No

Barium horizon C

389

Normal Tolerance Limit (K) Calculation for Barium soil horizon C, SWMU 54

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	4.53
Where		std. dev.	0.38
t =	Critical value of Student's t distribution	t	2.015
N =	Sample size	N	6
alpha =	Probability level test is conducted at (here, 0.05)	K	6.7064488
Limit =	Avg. + K(std. dev.)		

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
54SB15A	5.82	7.0784505	338.27	1186.1292	No
54SB9A	5.27	7.0784505	193.90	1186.1292	No
54SB16B	5.32	7.0784505	203.70	1186.1292	No
54SB14B	5.11	7.0784505	166.27	1186.1292	No
54SB6B	5.89	7.0784505	362.50	1186.1292	No
54SB10B	5.06	7.0784505	158.09	1186.1292	No
54SB11B	5.17	7.0784505	175.54	1186.1292	No
54SB12B	5.51	7.0784505	248.34	1186.1292	No
54SB2B	5.17	7.0784505	175.46	1186.1292	No
54SB3B	4.47	7.0784505	87.63	1186.1292	No
54SB4B	4.68	7.0784505	108.30	1186.1292	No
54SB5B	5.50	7.0784505	244.59	1186.1292	No
54SB7B	6.04	7.0784505	420.91	1186.1292	No
54SB8B	5.49	7.0784505	243.14	1186.1292	No
54SB9B	5.30	7.0784505	201.01	1186.1292	No
54SB10D	4.95	7.0784505	141.88	1186.1292	No
54SB13B	4.78	7.0784505	118.64	1186.1292	No
54SB1B	5.73	7.0784505	307.44	1186.1292	No
54SB16D	5.47	7.0784505	237.56	1186.1292	No

Beryllium horizon B

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Poisson-based Tolerance Limit (K) Calculation for Beryllium soil horizon B, SWMU 54

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

$T_n =$ Poisson count of background

$n =$ Background sample size

alpha = Probability level test is conducted at (here, 0.05)

T_n	7.83
$2T_n+2$	17.66
Chi Square ($2T_n+2$)	28.4343
n	6
Lambda T_n	2.369525
$2(\text{Lambda } T_n)$	4.73905
Chi Square $0.05[2K+2] \geq$	4.73905
$[2K+2] =$	12
$K =$	5

FSampNo	Value	Limit	Limit Exceeded?
54SB10A	1.81	5	No
54SB11A	1.49	5	No
54SB12A	1.54	5	No
54SB13A	1.42	5	No
54SB14A	0.89	5	No
54SB16A	1.47	5	No
54SB1A	0.93	5	No
54SB2A	1.76	5	No
54SB3A	1.11	5	No
54SB4A	1.78	5	No
54SB5A	1.55	5	No
54SB6A	1.11	5	No
54SB7A	0.82	5	No
54SB8A	1.15	5	No

Normal Tolerance Limit (K) Calculation for Beryllium soil horizon C, SWMU 54

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	-0.09993
Where		std. dev.	0.27
t =	Critical value of Student's t distribution	t	2.015
N =	Sample size	N	6
alpha =	Probability level test is conducted at (here, 0.05)	K	2.0765188

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
54SB15A	0.66	0.4607301	1.93	1.5852309	Yes
54SB9A	0.33	0.4607301	1.39	1.5852309	No
54SB16B	0.39	0.4607301	1.48	1.5852309	No
54SB14B	0.08	0.4607301	1.08	1.5852309	No
54SB6B	0.89	0.4607301	2.43	1.5852309	Yes
54SB10B	0.18	0.4607301	1.20	1.5852309	No
54SB11B	0.30	0.4607301	1.34	1.5852309	No
54SB12B	0.60	0.4607301	1.82	1.5852309	Yes
54SB2B	0.28	0.4607301	1.33	1.5852309	No
54SB3B	-1.27	0.4607301	0.28	1.5852309	No
54SB4B	-1.35	0.4607301	0.26	1.5852309	No
54SB5B	0.47	0.4607301	1.61	1.5852309	Yes
54SB7B	0.90	0.4607301	2.47	1.5852309	Yes
54SB8B	0.54	0.4607301	1.72	1.5852309	Yes
54SB9B	0.43	0.4607301	1.53	1.5852309	No
54SB10D	0.03	0.4607301	1.03	1.5852309	No
54SB13B	-1.35	0.4607301	0.26	1.5852309	No
54SB1B	-1.43	0.4607301	0.24	1.5852309	No
54SB16D	0.57	0.4607301	1.77	1.5852309	Yes

Poisson-based Tolerance Limit (K) Calculation for Cadmium soil horizon B, SWMU 54

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

 $T_n =$ Poisson count of background $n =$ Background sample size $\alpha =$ Probability level test is conducted at (here, 0.05)

T_n	4.33
$2T_n+2$	10.66
Chi Square ($2T_n+2$)	19.212
n	6
Lambda T_n	1.601
$2(\text{Lambda } T_n)$	3.202
Chi Square $0.05[2K+2] \geq$	3.202
$[2K+2] = 9$	
$K = 3.5$	

FSampNo	Value	Limit	Limit Exceeded?
54SB10A	0.73	3.5	No
54SB11A	0.73	3.5	No
54SB12A	0.75	3.5	No
54SB13A	0.74	3.5	No
54SB14A	0.71	3.5	No
54SB16A	0.74	3.5	No
54SB1A	2.4	3.5	No
54SB2A	0.68	3.5	No
54SB3A	0.69	3.5	No
54SB4A	0.75	3.5	No
54SB5A	0.75	3.5	No
54SB6A	11.75	3.5	Yes
54SB7A	0.69	3.5	No
54SB8A	0.73	3.5	No

Cadmium horizon C

Poisson-based Tolerance Limit (K) Calculation for Cadmium soil horizon C, SWMU 54

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

 $T_n =$ Poisson count of background $n =$ Background sample size $\alpha =$ Probability level test is conducted at (here, 0.05) T_n 4.21 $2T_n+2$ 10.42Chi Square $(2T_n+2)$ 18.8839 n 6Lambda T_n 1.5736583 $2(\text{Lambda } T_n)$ 3.1473167Chi Square $0.05[2K+2] \geq$ 3.1473167 $[2K+2] = 9$ $K = 3.5$

FSampNo	Value	Limit	Limit Exceeded?
54SB15A	0.74	3.5	No
54SB9A	0.73	3.5	No
54SB16B	0.74	3.5	No
54SB14B	0.73	3.5	No
54SB6B	0.84	3.5	No
54SB10B	0.74	3.5	No
54SB11B	0.73	3.5	No
54SB12B	0.8	3.5	No
54SB2B	0.74	3.5	No
54SB3B	0.79	3.5	No
54SB4B	0.72	3.5	No
54SB5B	0.77	3.5	No
54SB7B	0.81	3.5	No
54SB8B	0.75	3.5	No
54SB9B	0.76	3.5	No
54SB10D	0.69	3.5	No
54SB13B	0.73	3.5	No
54SB1B	0.66	3.5	No
54SB16D	0.75	3.5	No

Chromium horizon B

Normal Tolerance Limit (K) Calculation for Chromium soil horizon B, SWMU 54

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	3.76
Where		std. dev.	0.21
t =	Critical value of Student's t distribution	t	2.015
N =	Sample size	N	6
alpha =	Probability level test is conducted at (here, 0.05)	K	5.9364488

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
54SB10A	3.52	5.0066542	33.86	149.40403	No
54SB11A	3.50	5.0066542	33.17	149.40403	No
54SB12A	3.59	5.0066542	36.08	149.40403	No
54SB13A	3.44	5.0066542	31.29	149.40403	No
54SB14A	3.02	5.0066542	20.52	149.40403	No
54SB16A	3.53	5.0066542	34.27	149.40403	No
54SB1A	3.23	5.0066542	25.38	149.40403	No
54SB2A	3.33	5.0066542	27.91	149.40403	No
54SB3A	3.34	5.0066542	28.16	149.40403	No
54SB4A	3.57	5.0066542	35.56	149.40403	No
54SB5A	3.54	5.0066542	34.54	149.40403	No
54SB6A	4.92	5.0066542	136.92	149.40403	No
54SB7A	3.18	5.0066542	24.00	149.40403	No
54SB8A	3.32	5.0066542	27.69	149.40403	No

Chromium horizon C

Normal Tolerance Limit (K) Calculation for Chromium soil horizon C, SWMU 54

$K = \text{average} + t(N-1, \alpha) * \text{SQRT}(1 + (1/N))$		average	3.55
Where		std. dev.	0.22
t =	Critical value of Student's t distribution	t	2.015
N =	Sample size	N	6
alpha =	Probability level test is conducted at (here, 0.05)	K	5.7264488

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
54SB15A	3.83	4.8098187	45.93	122.70937	No
54SB9A	3.33	4.8098187	27.93	122.70937	No
54SB16B	3.53	4.8098187	34.20	122.70937	No
54SB14B	3.53	4.8098187	34.10	122.70937	No
54SB6B	4.25	4.8098187	70.14	122.70937	No
54SB10B	3.39	4.8098187	29.78	122.70937	No
54SB11B	3.49	4.8098187	32.93	122.70937	No
54SB12B	3.84	4.8098187	46.48	122.70937	No
54SB2B	3.38	4.8098187	29.45	122.70937	No
54SB3B	3.63	4.8098187	37.76	122.70937	No
54SB4B	3.06	4.8098187	21.30	122.70937	No
54SB5B	3.70	4.8098187	40.64	122.70937	No
54SB7B	4.04	4.8098187	57.10	122.70937	No
54SB8B	3.69	4.8098187	40.15	122.70937	No
54SB9B	3.63	4.8098187	37.56	122.70937	No
54SB10D	3.30	4.8098187	27.23	122.70937	No
54SB13B	3.48	4.8098187	32.32	122.70937	No
54SB1B	2.28	4.8098187	9.80	122.70937	No
54SB16D	3.77	4.8098187	43.53	122.70937	No

Lead horizon B

Normal Tolerance Limit (K) Calculation for Lead soil horizon B, SWMU 54

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	2.91
Where		std. dev.	0.35
t =	Critical value of Student's t distribution	t	2.015
N =	Sample size	N	6
alpha =	Probability level test is conducted at (here, 0.05)	K	5.0864488

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
54SB10A	5.33	4.6902571	205.56	108.88117	Yes
54SB11A	4.51	4.6902571	91.13	108.88117	No
54SB12A	3.06	4.6902571	21.22	108.88117	No
54SB13A	4.91	4.6902571	134.97	108.88117	Yes
54SB14A	3.60	4.6902571	36.56	108.88117	No
54SB16A	3.46	4.6902571	31.82	108.88117	No
54SB1A	6.57	4.6902571	716.80	108.88117	Yes
54SB2A	7.76	4.6902571	2354.26	108.88117	Yes
54SB3A	5.77	4.6902571	321.84	108.88117	Yes
54SB4A	4.43	4.6902571	84.26	108.88117	No
54SB5A	3.69	4.6902571	39.90	108.88117	No
54SB6A	8.24	4.6902571	3789.73	108.88117	Yes
54SB7A	3.92	4.6902571	50.29	108.88117	No
54SB8A	5.44	4.6902571	229.75	108.88117	Yes

Lead horizon C

Normal Tolerance Limit (K) Calculation for Lead soil horizon C

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	2.77
Where		std. dev.	0.26
t =	Critical value of Student's t distribution	t	2.015
N =	Sample size	N	6
alpha =	Probability level test is conducted at (here, 0.05)	K	4.9464488

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
54SB15A	3.35	4.0560767	28.40	57.747305	No
54SB9A	3.04	4.0560767	20.85	57.747305	No
54SB16B	2.70	4.0560767	14.81	57.747305	No
54SB14B	2.58	4.0560767	13.25	57.747305	No
54SB6B	6.07	4.0560767	430.56	57.747305	Yes
54SB10B	2.46	4.0560767	11.69	57.747305	No
54SB11B	2.49	4.0560767	12.11	57.747305	No
54SB12B	2.59	4.0560767	13.28	57.747305	No
54SB2B	2.66	4.0560767	14.23	57.747305	No
54SB3B	2.69	4.0560767	14.74	57.747305	No
54SB4B	2.12	4.0560767	8.36	57.747305	No
54SB5B	2.82	4.0560767	16.82	57.747305	No
54SB7B	3.13	4.0560767	22.79	57.747305	No
54SB8B	3.05	4.0560767	21.20	57.747305	No
54SB9B	2.76	4.0560767	15.83	57.747305	No
54SB10D	2.58	4.0560767	13.16	57.747305	No
54SB13B	2.11	4.0560767	8.23	57.747305	No
54SB1B	1.75	4.0560767	5.77	57.747305	No
54SB16D	2.62	4.0560767	13.68	57.747305	No

Mercury horizon B

Poisson-based Tolerance Limit (K) Calculation for Mercury soil horizon B, SWMU 54

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of Tn})$

Where

Lambda of Tn = $(1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2Tn+2))$

Where

Tn = Poisson count of background

n = Background sample size

alpha = Probability level test is conducted at (here, 0.05)

Tn	0.22
2Tn+2	2.44
Chi Square (2Tn+2)	6.81867
n	6
Lambda Tn	0.5682225
2(Lambda Tn)	1.136445
Chi Square 0.05[2K+2] >=	1.136445
[2K+2] = 5	
K = 1.5	

FSampNo	Value	Limit	Limit Exceeded?
54SB10A	0.03	1.5	No
54SB11A	0.03	1.5	No
54SB12A	0.03	1.5	No
54SB13A	0.03	1.5	No
54SB14A	0.03	1.5	No
54SB16A	0.03	1.5	No
54SB1A	0.09	1.5	No
54SB2A	0.13	1.5	No
54SB3A	5.06	1.5	Yes
54SB4A	0.03	1.5	No
54SB5A	0.03	1.5	No
54SB6A	72.13	1.5	Yes
54SB7A	0.03	1.5	No
54SB8A	0.03	1.5	No

Mercury Horizon C

399

Poisson-based Tolerance Limit (K) Calculation for Mercury soil horizon C, SWMU 54

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of Tn})$

Where

Lambda of Tn = $(1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2Tn+2))$

Where

Tn = Poisson count of background

n = Background sample size

alpha = Probability level test is conducted at (here, 0.05)

Tn	0.31
2Tn+2	2.62
Chi Square (2Tn+2)	7.14479
n	6
Lambda Tn	0.5953992
2(Lambda Tn)	1.1907983
Chi Square 0.05[2K+2] >=	1.1907983
[2K+2] = 6	
K = 2	

FSampNo	Value	Limit	Limit Exceeded?
54SB15A	0.03	2	No
54SB9A	0.03	2	No
54SB16B	0.03	2	No
54SB14B	0.03	2	No
54SB6B	0.04	2	No
54SB10B	0.12	2	No
54SB11B	0.03	2	No
54SB12B	0.04	2	No
54SB2B	0.03	2	No
54SB3B	0.21	2	No
54SB4B	0.03	2	No
54SB5B	0.03	2	No
54SB7B	0.04	2	No
54SB8B	0.03	2	No
54SB9B	0.03	2	No
54SB10D	0.03	2	No
54SB13B	0.03	2	No
54SB1B	0.03	2	No
54SB16D	0.03	2	No

Nickel horizon B

200

Normal Tolerance Limit (K) Calculation for Nickel soil horizon B, SWMU 54

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	2.98
Where		std. dev.	0.4
t =	Critical value of Student's t distribution	t	2.015
N =	Sample size	N	6
alpha =	Probability level test is conducted at (here, 0.05)	K	5.1564488

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
54SB10A	2.98	5.0425795	19.71	154.86898	No
54SB11A	3.00	5.0425795	20.05	154.86898	No
54SB12A	3.00	5.0425795	20.10	154.86898	No
54SB13A	2.94	5.0425795	18.90	154.86898	No
54SB14A	2.52	5.0425795	12.38	154.86898	No
54SB16A	3.02	5.0425795	20.56	154.86898	No
54SB1A	2.46	5.0425795	11.66	154.86898	No
54SB2A	2.33	5.0425795	10.25	154.86898	No
54SB3A	2.60	5.0425795	13.45	154.86898	No
54SB4A	3.07	5.0425795	21.44	154.86898	No
54SB5A	3.05	5.0425795	21.20	154.86898	No
54SB6A	2.83	5.0425795	16.99	154.86898	No
54SB7A	2.51	5.0425795	12.34	154.86898	No
54SB8A	2.75	5.0425795	15.60	154.86898	No

Normal Tolerance Limit (K) Calculation for Nickel soil horizon C, SWMU 54

$K = \text{average} + t((N-1), \alpha) * \text{SQRT}(1 + (1/N))$		average	2.69
Where		std. dev.	0.34
t =	Critical value of Student's t distribution	t	2.015
N =	Sample size	N	6
alpha =	Probability level test is conducted at (here, 0.05)	K	4.8664488

FSampNo	LN Value	LN Limit	Value	Limit	Limit Exceeded?
54SB15A	3.26	4.3445926	26.05	77.060635	No
54SB9A	2.87	4.3445926	17.68	77.060635	No
54SB16B	3.00	4.3445926	20.12	77.060635	No
54SB14B	3.00	4.3445926	20.12	77.060635	No
54SB6B	3.41	4.3445926	30.14	77.060635	No
54SB10B	2.89	4.3445926	18.01	77.060635	No
54SB11B	2.94	4.3445926	18.89	77.060635	No
54SB12B	3.27	4.3445926	26.43	77.060635	No
54SB2B	2.81	4.3445926	16.69	77.060635	No
54SB3B	2.33	4.3445926	10.26	77.060635	No
54SB4B	2.22	4.3445926	9.19	77.060635	No
54SB5B	3.20	4.3445926	24.46	77.060635	No
54SB7B	3.55	4.3445926	34.72	77.060635	No
54SB8B	3.24	4.3445926	25.56	77.060635	No
54SB9B	3.12	4.3445926	22.61	77.060635	No
54SB10D	2.74	4.3445926	15.45	77.060635	No
54SB13B	2.58	4.3445926	13.20	77.060635	No
54SB1B	1.83	4.3445926	6.23	77.060635	No
54SB16D	3.19	4.3445926	24.25	77.060635	No

Selenium horizon B

402

Poisson-based Tolerance Limit (K) Calculation for Selenium soil horizon B, SWMU 54

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

$T_n =$ Poisson count of background

$n =$ Background sample size

$\alpha =$ Probability level test is conducted at (here, 0.05)

T_n	1.62
$2T_n+2$	5.24
Chi Square ($2T_n+2$)	11.4404
n	6
Lambda T_n	0.9533667
$2(\text{Lambda } T_n)$	1.9067333
Chi Square $0.05[2K+2] \geq$	1.9067333
$[2K+2] = 7$	
$K = 2.5$	

FSampNo	Value	Limit	Limit Exceeded?
54SB10A	0.27	2.5	No
54SB11A	0.28	2.5	No
54SB12A	0.28	2.5	No
54SB13A	0.28	2.5	No
54SB14A	0.27	2.5	No
54SB16A	0.28	2.5	No
54SB1A	0.27	2.5	No
54SB2A	0.25	2.5	No
54SB3A	0.26	2.5	No
54SB4A	0.28	2.5	No
54SB5A	0.28	2.5	No
54SB6A	0.28	2.5	No
54SB7A	0.26	2.5	No
54SB8A	0.27	2.5	No

Selenium horizon C

403

Poisson-based Tolerance Limit (K) Calculation for Selenium soil horizon C, SWMU 54

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of Tn})$

Where

Lambda of Tn = $(1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2Tn+2))$

Where

Tn = Poisson count of background

n = Background sample size

alpha = Probability level test is conducted at (here, 0.05)

Tn	1.61
2Tn+2	5.22
Chi Square (2Tn+2)	11.4097
n	6
Lambda Tn	0.9508083
2(Lambda Tn)	1.9016167
Chi Square $0.05[2K+2] \geq$	1.9016167
$[2K+2] = 7$	
K = 2.5	

FSampNo	Value	Limit	Limit Exceeded?
54SB15A	0.28	2.5	No
54SB9A	0.28	2.5	No
54SB16B	0.28	2.5	No
54SB14B	0.27	2.5	No
54SB6B	0.31	2.5	No
54SB10B	0.28	2.5	No
54SB11B	0.27	2.5	No
54SB12B	0.3	2.5	No
54SB2B	0.28	2.5	No
54SB3B	0.3	2.5	No
54SB4B	0.27	2.5	No
54SB5B	0.29	2.5	No
54SB7B	0.3	2.5	No
54SB8B	0.28	2.5	No
54SB9B	0.28	2.5	No
54SB10D	0.26	2.5	No
54SB13B	0.27	2.5	No
54SB1B	0.25	2.5	No
54SB16D	0.28	2.5	No

Silver horizon B

404

Poisson-based Tolerance Limit (K) Calculation for Silver soil horizon B, SWMU 54

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

$T_n =$ Poisson count of background

$n =$ Background sample size

alpha = Probability level test is conducted at (here, 0.05)

T_n	0.585
$2T_n+2$	3.17
Chi Square ($2T_n+2$)	8.10743
n	6
Lambda T_n	0.6756192
$2(\text{Lambda } T_n)$	1.3512383
Chi Square $0.05[2K+2] \geq$	1.3512383
$[2K+2] = 6$	
$K = 2$	

FSampNo	Value	Limit	Limit Exceeded?
54SB10A	0.07	2	No
54SB11A	0.01	2	No
54SB12A	0.01	2	No
54SB13A	0.07	2	No
54SB14A	0.005	2	No
54SB16A	0.01	2	No
54SB1A	0.07	2	No
54SB2A	0.03	2	No
54SB3A	0.03	2	No
54SB4A	0.04	2	No
54SB5A	0.04	2	No
54SB6A	0.3	2	No
54SB7A	0.005	2	No
54SB8A	0.02	2	No

Silver horizon C

405

Poisson-based Tolerance Limit (K) Calculation for Silver soil horizon C, SWMU 54

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

$T_n =$ Poisson count of background

$n =$ Background sample size

alpha = Probability level test is conducted at (here, 0.05)

T_n	0.04
$2T_n+2$	2.08
Chi Square ($2T_n+2$)	6.1455
n	6
Lambda T_n	0.512125
$2(\text{Lambda } T_n)$	1.02425
Chi Square $0.05[2K+2] \geq$	1.02425
$[2K+2] = 5$	
$K = 1.5$	

FSampNo	Value	Limit	Limit Exceeded?
54SB15A	0.01	1.5	No
54SB9A	0.02	1.5	No
54SB16B	0.01	1.5	No
54SB14B	0.005	1.5	No
54SB6B	0.01	1.5	No
54SB10B	0.03	1.5	No
54SB11B	0.01	1.5	No
54SB12B	0.01	1.5	No
54SB2B	0.03	1.5	No
54SB3B	0.04	1.5	No
54SB4B	0.03	1.5	No
54SB5B	0.05	1.5	No
54SB7B	0.01	1.5	No
54SB8B	0.01	1.5	No
54SB9B	0.04	1.5	No
54SB10D	0.03	1.5	No
54SB13B	0.01	1.5	No
54SB1B	0.005	1.5	No
54SB16D	0.01	1.5	No

Thallium Horizon B

Poisson-based Tolerance Limit (K) Calculation for Thallium soil horizon B, SWMU 54

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of } T_n)$

Where

Lambda of $T_n = (1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2T_n+2))$

Where

$T_n =$ Poisson count of background

$n =$ Background sample size

$\alpha =$ Probability level test is conducted at (here, 0.05)

T_n	123.64
$2T_n+2$	249.28
Chi Square ($2T_n+2$)	287.107
n	6
Lambda T_n	23.925583
$2(\text{Lambda } T_n)$	47.851167
Chi Square $0.05[2K+2] \geq$	47.851167
$[2K+2] = 66$	
$K = 32$	

FSampNo	Value	Limit	Limit Exceeded?
54SB10A	20.74	32	No
54SB11A	20.84	32	No
54SB12A	21.41	32	No
54SB13A	21.05	32	No
54SB14A	20.23	32	No
54SB16A	20.99	32	No
54SB1A	20.16	32	No
54SB2A	19.23	32	No
54SB3A	19.72	32	No
54SB4A	21.25	32	No
54SB5A	21.39	32	No
54SB6A	20.97	32	No
54SB7A	19.6	32	No
54SB8A	20.74	32	No

Thallium horizon C

407

Poisson-based Tolerance Limit (K) Calculation for Thallium soil horizon C

K = Poisson based tolerance limit

Where

Chi square at alpha $[2K+2] \geq 2(\text{Lambda of Tn})$

Where

Lambda of Tn = $(1/2n) * ((\text{Chi Square at alpha}) \text{ of } (2Tn+2))$

Where

Tn = Poisson count of background

n = Background sample size

alpha = Probability level test is conducted at (here, 0.05)

Tn	121.19
2Tn+2	244.38
Chi Square (2Tn+2)	281.844
n	6
Lambda Tn	23.487
2(Lambda Tn)	46.974
Chi Square 0.05[2K+2] $\geq$	46.974
[2K+2] = 65	
K = 31.5	

FSampNo	Value	Limit	Limit Exceeded?
54SB15A	21.18	31.5	No
54SB9A	20.92	31.5	No
54SB16B	21.18	31.5	No
54SB14B	20.67	31.5	No
54SB6B	23.82	31.5	No
54SB10B	21.02	31.5	No
54SB11B	20.77	31.5	No
54SB12B	22.78	31.5	No
54SB2B	21.05	31.5	No
54SB3B	22.57	31.5	No
54SB4B	20.64	31.5	No
54SB5B	21.85	31.5	No
54SB7B	22.99	31.5	No
54SB8B	21.39	31.5	No
54SB9B	21.55	31.5	No
54SB10D	19.62	31.5	No
54SB13B	20.77	31.5	No
54SB1B	18.77	31.5	No
54SB16D	21.33	31.5	No

TAIL AREA PROBABILITY CALCULATIONS

New River Surface Water, Barium

Tail Area Probabilities

Distributions available:

(1) Bernoulli	(7) Beta	(13) Lognormal
(2) Binomial	(8) Chi-square	(14) Normal
(3) Discrete uniform	(9) Erlang	(15) Student's t
(4) Geometric	(10) Exponential	(16) Triangular
(5) Negative binomial	(11) F	(17) Uniform
(6) Poisson	(12) Gamma	(18) Weibull

Distribution number: 13

Mean: 3.22

Standard deviation: 0.004619

Area at or below 3.27	= 1.	Sample: NRSW4
Area at or below 3.05	= 0.	Sample: NRSW5
Area at or below 3.21	= 0.015094	Sample: NRSW6
Area at or below 3.28	= 1.	Sample: SPG3SW1

New River Sediment, Barium

Tail Area Probabilities

Distributions available:

- | | | |
|-----------------------|------------------|------------------|
| (1) Bernoulli | (7) Beta | (13) Lognormal |
| (2) Binomial | (8) Chi-square | (14) Normal |
| (3) Discrete uniform | (9) Erlang | (15) Student's t |
| (4) Geometric | (10) Exponential | (16) Triangular |
| (5) Negative binomial | (11) F | (17) Uniform |
| (6) Poisson | (12) Gamma | (18) Weibull |

Distribution number: 13

Mean: 5.49

Standard deviation: 0.506317

Area at or below 4.58	= 0.027226	Sample: NRSE4
Area at or below 5.19	= 0.286173	Sample: NRSE5
Area at or below 4.70	= 0.050275	Sample: NRSE6
Area at or below 6.55	= 0.97525	Sample: SPGSE1

95th Percentile of Background = 6.36

New River Sediment, Benz(a) anthracene

Tail Area Probabilities

Distributions available:

(1) Bernoulli	(7) Beta	(13) Lognormal
(2) Binomial	(8) Chi-square	(14) Normal
(3) Discrete uniform	(9) Erlang	(15) Student's t
(4) Geometric	(10) Exponential	(16) Triangular
(5) Negative binomial	(11) F	(17) Uniform
(6) Poisson	(12) Gamma	(18) Weibull

Distribution number: 14

Mean: 0.54

Standard deviation: 0.202672

Area at or below 0.03	= 0.005928	Sample: NRSE4
Area at or below 0.09	= 0.013198	Sample: NRSE5
Area at or below 0.40	= 0.244853	Sample: NRSE6

95th Percentile of Background = 0.87

New River Sediment, Beryllium

Tail Area Probabilities

Distributions available:

(1) Bernoulli	(7) Beta	(13) Lognormal
(2) Binomial	(8) Chi-square	(14) Normal
(3) Discrete uniform	(9) Erlang	(15) Student's t
(4) Geometric	(10) Exponential	(16) Triangular
(5) Negative binomial	(11) F	(17) Uniform
(6) Poisson	(12) Gamma	(18) Weibull

Distribution number: 14

Mean: 1.26

Standard deviation: 1.536045

Area at or below 0.99	= 0.430233	Sample: NRSE4
Area at or below 1.31	= 0.512987	Sample: NRSE5
Area at or below 0.33	= 0.272438	Sample: NRSE6
Area at or below 4.23	= 0.973415	Sample: SPG3SE1

95th Percentile of Background = 3.79

New River Sediment, Chromium

Tail Area Probabilities

Distributions available:

- | | | |
|-----------------------|------------------|------------------|
| (1) Bernoulli | (7) Beta | (13) Lognormal |
| (2) Binomial | (8) Chi-square | (14) Normal |
| (3) Discrete uniform | (9) Erlang | (15) Student's t |
| (4) Geometric | (10) Exponential | (16) Triangular |
| (5) Negative binomial | (11) F | (17) Uniform |
| (6) Poisson | (12) Gamma | (18) Weibull |

Distribution number: 13

Mean: 3.88

Standard deviation: 0.443074

Area at or below 3.63	= 0.298672	Sample: NRSE4
Area at or below 3.45	= 0.164771	Sample: NRSE5
Area at or below 3.21	= 0.053863	Sample: NRSE6
Area at or below 4.14	= 0.734587	Sample: SPG3SE1

95th Percentile of Background = 4.65

New River Sediment, Chrysene

Tail Area Probabilities

Distributions available:

- | | | |
|-----------------------|------------------|------------------|
| (1) Bernoulli | (7) Beta | (13) Lognormal |
| (2) Binomial | (8) Chi-square | (14) Normal |
| (3) Discrete uniform | (9) Erlang | (15) Student's t |
| (4) Geometric | (10) Exponential | (16) Triangular |
| (5) Negative binomial | (11) F | (17) Uniform |
| (6) Poisson | (12) Gamma | (18) Weibull |

Distribution number: 14

Mean: 0.90

Standard deviation: 0.686824

Area at or below 0.02	= 0.100051	Sample: NRSE4
Area at or below 0.10	= 0.122053	Sample: NRSE5
Area at or below 0.53	= 0.295041	Sample: NRSE6

95th Percentile of Background = 2.04

New River Sediment, Fluoranthene

Tail Area Probabilities

Distributions available:

- | | | |
|-----------------------|------------------|------------------|
| (1) Bernoulli | (7) Beta | (13) Lognormal |
| (2) Binomial | (8) Chi-square | (14) Normal |
| (3) Discrete uniform | (9) Erlang | (15) Student's t |
| (4) Geometric | (10) Exponential | (16) Triangular |
| (5) Negative binomial | (11) F | (17) Uniform |
| (6) Poisson | (12) Gamma | (18) Weibull |

Distribution number: 14

Mean: 0.41

Standard deviation: 0.345881

Area at or below 0.08	= 0.170019	Sample: NRSE4
Area at or below 0.11	= 0.192874	Sample: NRSE5
Area at or below 0.50	= 0.602649	Sample: NRSE6

95th Percentile of Background = 0.98

New River Sediment, Lead

Tail Area Probabilities

Distributions available:

(1) Bernoulli	(7) Beta	(13) Lognormal
(2) Binomial	(8) Chi-square	(14) Normal
(3) Discrete uniform	(9) Erlang	(15) Student's t
(4) Geometric	(10) Exponential	(16) Triangular
(5) Negative binomial	(11) F	(17) Uniform
(6) Poisson	(12) Gamma	(18) Weibull

Distribution number: 13

Mean: 5.07

Standard deviation: 0.20

Area at or below 8.39	= 1.	Sample: NRSE4
Area at or below 5.39	= 0.942008	Sample: NRSE5
Area at or below 4.96	= 0.295786	Sample: NRSE6
Area at or below 6.31	= 1.	Sample: SPG3SE1

95th Percentile of Background = 5.41

New River Sediment, Nickel

Tail Area Probabilities

Distributions available:

(1) Bernoulli	(7) Beta	(13) Lognormal
(2) Binomial	(8) Chi-square	(14) Normal
(3) Discrete uniform	(9) Erlang	(15) Student's t
(4) Geometric	(10) Exponential	(16) Triangular
(5) Negative binomial	(11) F	(17) Uniform
(6) Poisson	(12) Gamma	(18) Weibull

Distribution number: 13

Mean: 3.24

Standard deviation: 0.61909

Area at or below 2.58	= 0.13389	Sample: NRSE4
Area at or below 2.76	= 0.22601	Sample: NRSE5
Area at or below 2.52	= 0.108891	Sample: NRSE6
Area at or below 3.97	= 0.878536	Sample: SPG3SE1

95th Percentile of Background = 4.35

New River Sediment, Phenanthrene

Tail Area Probabilities

Distributions available:

- | | | |
|-----------------------|------------------|------------------|
| (1) Bernoulli | (7) Beta | (13) Lognormal |
| (2) Binomial | (8) Chi-square | (14) Normal |
| (3) Discrete uniform | (9) Erlang | (15) Student's t |
| (4) Geometric | (10) Exponential | (16) Triangular |
| (5) Negative binomial | (11) F | (17) Uniform |
| (6) Poisson | (12) Gamma | (18) Weibull |

Distribution number: 14

Mean: 0.69

Standard deviation: 0.164939

Area at or below 0.02	= 0.000024	Sample: NRSE4
Area at or below 0.11	= 0.000219	Sample: NRSE4
Area at or below 0.35	= 0.019634	Sample: NRSE4

95th Percentile of Background = 0.96

New River Sediment, Pyrene

Tail Area Probabilities

Distributions available:

(1) Bernoulli	(7) Beta	(13) Lognormal
(2) Binomial	(8) Chi-square	(14) Normal
(3) Discrete uniform	(9) Erlang	(15) Student's t
(4) Geometric	(10) Exponential	(16) Triangular
(5) Negative binomial	(11) F	(17) Uniform
(6) Poisson	(12) Gamma	(18) Weibull

Distribution number: 14

Mean: 0.73

Standard deviation: 0.307338

Area at or below 0.06	= 0.014628	Sample: NRSE4
Area at or below 0.15	= 0.029568	Sample: NRSE5
Area at or below 0.76	= 0.538883	Sample: NRSE6

95th Percentile of Background = 1.24

420

New River Sediment, Silver

Tail Area Probabilities

Distributions available:

- | | | |
|-----------------------|------------------|------------------|
| (1) Bernoulli | (7) Beta | (13) Lognormal |
| (2) Binomial | (8) Chi-square | (14) Normal |
| (3) Discrete uniform | (9) Erlang | (15) Student's t |
| (4) Geometric | (10) Exponential | (16) Triangular |
| (5) Negative binomial | (11) F | (17) Uniform |
| (6) Poisson | (12) Gamma | (18) Weibull |

Distribution number: 14

Mean: 0.13

Standard deviation: 0.036502

Area at or below 0.10	= 0.205574	Sample: NRSE4
Area at or below 0.10	= 0.205574	Sample: NRSE5
Area at or below 0.11	= 0.291874	Sample: NRSE6
Area at or below 0.22	= 0.993161.	Sample: SPG3SE1

95th Percentile of Background = 0.19

APPENDIX I
RISK CALCULATION TABLES

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 17
Exposure Scenario: Commercial Worker Exposure to GROUNDWATER--Ingestion

CHEMICAL	EP CONCENTRATIONS	HAZARD INDEX-CT	HAZARD INDEX-RME	CANCER RISK-CT	CANCER RISK-RME
Antimony	4.13E-02	0.25	1.01	0.00E+00	0.00E+00
Barium	7.71E-02	0.00	0.01	0.00E+00	0.00E+00
Beryllium	1.55E-03	0.00	0.00	1.16E-06	2.32E-05

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.26
Total Hazard Index-RME: 1.02
Total Cancer Risk-CT: 1.16E-06
Total Cancer Risk-RME: 2.32E-05

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 17
Exposure Scenario: Commercial Worker Exposure to GROUNDWATER--Dermal (Showering)

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Antimony	4.13E-02	0.11	0.46	0.00E+00	0.00E+00
Barium	7.71E-02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	1.55E-03	0.00	0.00	5.27E-07	1.06E-05

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.12
Total Hazard Index-RME: 0.46
Total Cancer Risk-CT: 5.27E-07
Total Cancer Risk-RME: 1.06E-05

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 17A
Exposure Scenario: Commercial Worker Exposure to Surface Soil--Ingestion

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Arsenic	1.02E+02	0.08	0.33	2.67E-06	5.33E-05
Barium	5.77E+02	0.00	0.01	0.00E+00	0.00E+00
Beryllium	9.84E-01	0.00	0.00	7.40E-08	1.48E-06
Cadmium	4.29E+00	0.00	0.01	0.00E+00	0.00E+00
Chromium III	2.23E+02	0.00	0.00	0.00E+00	0.00E+00
Lead	4.72E+03	0.00	0.00	0.00E+00	0.00E+00
Mercury	3.29E-01	0.00	0.00	0.00E+00	0.00E+00
Nickel	6.91E+01	0.00	0.00	0.00E+00	0.00E+00
Silver	2.18E+00	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.09
 Total Hazard Index-RME: 0.35
 Total Cancer Risk-CT: 2.74E-06
 Total Cancer Risk-RME: 5.48E-05

425

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 17A
Exposure Scenario: Commercial Worker Exposure to Surface Soil--Dermal

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Arsenic	1.02E+02	0.07	0.17	2.46E-06	3.19E-05
Barium	5.77E+02	0.03	0.07	0.00E+00	0.00E+00
Beryllium	9.84E-01	0.00	0.01	4.67E-06	6.06E-05
Cadmium	4.29E+00	0.07	0.17	0.00E+00	0.00E+00
Chromium III	2.23E+02	0.00	0.00	0.00E+00	0.00E+00
Lead	4.72E+03	0.00	0.00	0.00E+00	0.00E+00
Mercury	3.29E-01	0.02	0.04	0.00E+00	0.00E+00
Nickel	6.91E+01	0.01	0.03	0.00E+00	0.00E+00
Silver	2.18E+00	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.19
Total Hazard Index-RME: 0.50
Total Cancer Risk-CT: 7.13E-06
Total Cancer Risk-RME: 9.25E-05

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 17A
Exposure Scenario: Commercial Worker Exposure to Surface Soil--Inhalation of Particulates

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Arsenic	1.02E+02	0.00	0.00	6.46E-14	9.73E-13
Barium	5.77E+02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	9.84E-01	0.00	0.00	3.49E-16	5.26E-15
Cadmium	4.29E+00	0.00	0.00	1.14E-15	1.72E-14
Chromium III	2.23E+02	0.00	0.00	0.00E+00	0.00E+00
Lead	4.72E+03	0.00	0.00	0.00E+00	0.00E+00
Mercury	3.29E-01	0.00	0.00	0.00E+00	0.00E+00
Nickel	6.91E+01	0.00	0.00	0.00E+00	0.00E+00
Silver	2.18E+00	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.00
 Total Hazard Index-RME: 0.00
 Total Cancer Risk-CT: 6.61E-14
 Total Cancer Risk-RME: 9.96E-13

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 17A
Exposure Scenario: Hunter Exposure to Surface Soil--Ingestion

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Arsenic	1.02E+02	0.02	0.05	9.60E-07	1.66E-05
Barium	5.77E+02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	9.84E-01	0.00	0.00	2.66E-08	4.61E-07
Cadmium	4.29E+00	0.00	0.00	0.00E+00	0.00E+00
Chromium III	2.23E+02	0.00	0.00	0.00E+00	0.00E+00
Lead	4.72E+03	0.00	0.00	0.00E+00	0.00E+00
Mercury	3.29E-01	0.00	0.00	0.00E+00	0.00E+00
Nickel	6.91E+01	0.00	0.00	0.00E+00	0.00E+00
Silver	2.18E+00	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.02
 Total Hazard Index-RME: 0.06
 Total Cancer Risk-CT: 9.86E-07
 Total Cancer Risk-RME: 1.71E-05

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 17A
Exposure Scenario: Hunter Exposure to Surface Soil--Dermal

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Arsenic	1.02E+02	0.01	0.02	5.54E-07	6.04E-06
Barium	5.77E+02	0.00	0.01	0.00E+00	0.00E+00
Beryllium	9.84E-01	0.00	0.00	1.05E-06	1.15E-05
Cadmium	4.29E+00	0.01	0.02	0.00E+00	0.00E+00
Chromium III	2.23E+02	0.00	0.00	0.00E+00	0.00E+00
Lead	4.72E+03	0.00	0.00	0.00E+00	0.00E+00
Mercury	3.29E-01	0.00	0.00	0.00E+00	0.00E+00
Nickel	6.91E+01	0.00	0.00	0.00E+00	0.00E+00
Silver	2.18E+00	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.02
 Total Hazard Index-RME: 0.05
 Total Cancer Risk-CT: 1.61E-06
 Total Cancer Risk-RME: 1.75E-05

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 17A
Exposure Scenario: Construction Worker Exposure to Surface Soil--Ingestion

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Arsenic	1.02E+02	0.33	1.59	1.07E-06	2.05E-05
Barium	5.77E+02	0.01	0.04	0.00E+00	0.00E+00
Beryllium	9.84E-01	0.00	0.00	2.96E-08	5.68E-07
Cadmium	4.29E+00	0.01	0.04	0.00E+00	0.00E+00
Chromium III	2.23E+02	0.00	0.00	0.00E+00	0.00E+00
Lead	4.72E+03	0.00	0.00	0.00E+00	0.00E+00
Mercury	3.29E-01	0.00	0.01	0.00E+00	0.00E+00
Nickel	6.91E+01	0.00	0.02	0.00E+00	0.00E+00
Silver	2.18E+00	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.35
 Total Hazard Index-RME: 1.70
 Total Cancer Risk-CT: 1.10E-06
 Total Cancer Risk-RME: 2.10E-05

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 17A
Exposure Scenario: Construction Worker Exposure to Surface Soil--Dermal

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Arsenic	1.02E+02	0.13	0.17	4.91E-07	2.55E-06
Barium	5.77E+02	0.05	0.07	0.00E+00	0.00E+00
Beryllium	9.84E-01	0.01	0.01	9.35E-07	4.85E-06
Cadmium	4.29E+00	0.13	0.17	0.00E+00	0.00E+00
Chromium III	2.23E+02	0.00	0.00	0.00E+00	0.00E+00
Lead	4.72E+03	0.00	0.00	0.00E+00	0.00E+00
Mercury	3.29E-01	0.03	0.04	0.00E+00	0.00E+00
Nickel	6.91E+01	0.03	0.03	0.00E+00	0.00E+00
Silver	2.18E+00	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.39
Total Hazard Index-RME: 0.50
Total Cancer Risk-CT: 1.43E-06
Total Cancer Risk-RME: 7.40E-06

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 17A
Exposure Scenario: Construction Worker Exposure to Surface Soil--Inhalation of Particulates

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Arsenic	1.02E+02	0.00	0.00	3.12E-14	2.18E-13
Barium	5.77E+02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	9.84E-01	0.00	0.00	1.68E-16	1.18E-15
Cadmium	4.29E+00	0.00	0.00	5.50E-16	3.85E-15
Chromium III	2.23E+02	0.00	0.00	0.00E+00	0.00E+00
Lead	4.72E+03	0.00	0.00	0.00E+00	0.00E+00
Mercury	3.29E-01	0.00	0.00	0.00E+00	0.00E+00
Nickel	6.91E+01	0.00	0.00	0.00E+00	0.00E+00
Silver	2.18E+00	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.00
 Total Hazard Index-RME: 0.00
 Total Cancer Risk-CT: 3.19E-14
 Total Cancer Risk-RME: 2.23E-13

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 17A
Exposure Scenario: Construction Worker Exposure to Subsurface Soil--Ingestion

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Antimony	7.16E+01	0.09	0.84	0.00E+00	0.00E+00
Arsenic	9.49E+01	0.15	1.49	4.97E-07	1.91E-05
Barium	5.13E+03	0.04	0.34	0.00E+00	0.00E+00
Benzo (a) anthracene	9.21E-02	0.00	0.00	2.35E-10	9.02E-09
Benzo (b) fluoranthene	4.43E-01	0.00	0.00	1.13E-09	4.34E-08
Benzo (g,h,i) perylene	4.22E-01	0.00	0.00	0.00E+00	0.00E+00
Benzo (k) fluoranthene	1.65E-01	0.00	0.00	4.21E-11	1.62E-09
bis (2-Ethyl hexyl) Phthalate	5.91E+00	0.00	0.00	2.89E-10	1.11E-08
Cadmium	1.37E+01	0.01	0.13	0.00E+00	0.00E+00
Chromium III	2.05E+03	0.00	0.01	0.00E+00	0.00E+00
Chrysene	7.94E-02	0.00	0.00	2.03E-12	7.78E-11
Fluoranthene	7.30E-02	0.00	0.00	0.00E+00	0.00E+00
Lead	5.26E+03	0.00	0.00	0.00E+00	0.00E+00
Nickel	9.03E+02	0.02	0.21	0.00E+00	0.00E+00
Phenanthrene	9.30E-02	0.00	0.00	0.00E+00	0.00E+00
Pyrene	1.71E-01	0.00	0.00	0.00E+00	0.00E+00
Silver	4.23E+01	0.00	0.04	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.32
 Total Hazard Index-RME: 3.06
 Total Cancer Risk-CT: 4.99E-07
 Total Cancer Risk-RME: 1.92E-05

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 17A
Exposure Scenario: Construction Worker Exposure to Subsurface Soil--Dermal

CHEMICAL	EP CONCENTRATIONS	HAZARD INDEX-CT	HAZARD INDEX-RME	CANCER RISK-CT	CANCER RISK-RME
Antimony	7.16E+01	2.77	7.18	0.00E+00	0.00E+00
Arsenic	9.49E+01	0.06	0.16	2.29E-07	2.38E-06
Barium	5.13E+03	0.23	0.59	0.00E+00	0.00E+00
Benzo (a) anthracene	9.21E-02	0.00	0.00	9.28E-09	9.63E-08
Benzo (b) fluoranthene	4.43E-01	0.00	0.00	4.47E-08	4.64E-07
Benzo (g,h,i) perylene	4.22E-01	0.00	0.00	0.00E+00	0.00E+00
Benzo (k) fluoranthene	1.65E-01	0.00	0.00	1.66E-09	1.73E-08
bis (2-Ethyl hexyl) Phthalate	5.91E+00	0.00	0.01	4.57E-09	4.74E-08
Cadmium	1.37E+01	0.21	0.55	0.00E+00	0.00E+00
Chromium III	2.05E+03	0.02	0.04	0.00E+00	0.00E+00
Chrysene	7.94E-02	0.00	0.00	1.07E-11	1.11E-10
Fluoranthene	7.30E-02	0.00	0.00	0.00E+00	0.00E+00
Lead	5.26E+03	0.00	0.00	0.00E+00	0.00E+00
Nickel	9.03E+02	0.17	0.45	0.00E+00	0.00E+00
Phenanthrene	9.30E-02	0.00	0.00	0.00E+00	0.00E+00
Pyrene	1.71E-01	0.00	0.00	0.00E+00	0.00E+00
Silver	4.23E+01	0.01	0.02	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 3.47
 Total Hazard Index-RME: 8.99
 Total Cancer Risk-CT: 2.89E-07
 Total Cancer Risk-RME: 3.00E-06

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 17A
Exposure Scenario: Construction Worker Exposure to Subsurface Soil--Inhalation of Particulates

CHEMICAL	EP CONCENTRATIONS	HAZARD INDEX-CT	HAZARD INDEX-RME	CANCER RISK-CT	CANCER RISK-RME
Antimony	7.16E+01	0.00	0.00	0.00E+00	0.00E+00
Arsenic	9.49E+01	0.00	0.00	6.03E-15	7.27E-14
Barium	5.13E+03	0.00	0.00	0.00E+00	0.00E+00
Cadmium	1.37E+01	0.00	0.00	3.65E-16	4.40E-15
Chromium III	2.05E+03	0.00	0.00	0.00E+00	0.00E+00
Lead	5.26E+03	0.00	0.00	0.00E+00	0.00E+00
Nickel	9.03E+02	0.00	0.00	0.00E+00	0.00E+00
Silver	4.23E+01	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.00
 Total Hazard Index-RME: 0.00
 Total Cancer Risk-CT: 6.40E-15
 Total Cancer Risk-RME: 7.70E-14

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 17A
Exposure Scenario: Construction Worker Exposure to Subsurface Soil--Inhalation of Volatiles

CHEMICAL	EP CONCENTRATIONS	HAZARD INDEX-CT	HAZARD INDEX-RME	CANCER RISK-CT	CANCER RISK-RME
Benzo (a) anthracene	9.21E-02	0.00	0.00	5.64E-10	6.79E-09
Benzo (b) fluoranthene	4.43E-01	0.00	0.00	3.23E-09	3.89E-08
Benzo (g,h,i) perylene	4.22E-01	0.00	0.00	0.00E+00	0.00E+00
Benzo (k) fluoranthene	1.65E-01	0.00	0.00	5.05E-09	6.09E-08
bis (2-Ethyl hexyl) Phthalate	5.91E+00	0.00	0.00	0.00E+00	0.00E+00
Chrysene	7.94E-02	0.00	0.00	1.50E-18	1.80E-17
Fluoranthene	7.30E-02	0.00	0.00	0.00E+00	0.00E+00
Phenanthrene	9.30E-02	0.00	0.00	0.00E+00	0.00E+00
Pyrene	1.71E-01	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.00
 Total Hazard Index-RME: 0.00
 Total Cancer Risk-CT: 8.85E-09
 Total Cancer Risk-RME: 1.07E-07

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 17BCD
Exposure Scenario: Commercial Worker Exposure to Surface Soil--Ingestion

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Arsenic	4.82E+01	0.04	0.16	1.26E-06	2.53E-05
Barium	1.61E+02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	2.82E+00	0.00	0.00	2.12E-07	4.23E-06
Cadmium	1.64E+00	0.00	0.00	0.00E+00	0.00E+00
Chromium III	1.05E+02	0.00	0.00	0.00E+00	0.00E+00
Lead	2.90E+02	0.00	0.00	0.00E+00	0.00E+00
Mercury	9.41E-02	0.00	0.00	0.00E+00	0.00E+00
Nickel	4.58E+01	0.00	0.00	0.00E+00	0.00E+00
Silver	4.88E-01	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.04
 Total Hazard Index-RME: 0.17
 Total Cancer Risk-CT: 1.47E-06
 Total Cancer Risk-RME: 2.95E-05

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 17BCD
Exposure Scenario: Commercial Worker Exposure to Surface Soil--Dermal

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Arsenic	4.82E+01	0.03	0.08	1.16E-06	1.51E-05
Barium	1.61E+02	0.01	0.02	0.00E+00	0.00E+00
Beryllium	2.82E+00	0.01	0.02	1.34E-05	1.74E-04
Cadmium	1.64E+00	0.03	0.07	0.00E+00	0.00E+00
Chromium III	1.05E+02	0.00	0.00	0.00E+00	0.00E+00
Lead	2.90E+02	0.00	0.00	0.00E+00	0.00E+00
Mercury	9.41E-02	0.00	0.01	0.00E+00	0.00E+00
Nickel	4.58E+01	0.01	0.02	0.00E+00	0.00E+00
Silver	4.88E-01	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.09
Total Hazard Index-RME: 0.23
Total Cancer Risk-CT: 1.45E-05
Total Cancer Risk-RME: 1.89E-04

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 17BCD
Exposure Scenario: Commercial Worker Exposure to Surface Soil--Inhalation of Particulates

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Arsenic	4.82E+01	0.00	0.00	3.06E-14	4.61E-13
Barium	1.61E+02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	2.82E+00	0.00	0.00	9.99E-16	1.50E-14
Cadmium	1.64E+00	0.00	0.00	4.37E-16	6.59E-15
Chromium III	1.05E+02	0.00	0.00	0.00E+00	0.00E+00
Lead	2.90E+02	0.00	0.00	0.00E+00	0.00E+00
Mercury	9.41E-02	0.00	0.00	0.00E+00	0.00E+00
Nickel	4.58E+01	0.00	0.00	0.00E+00	0.00E+00
Silver	4.88E-01	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.00
 Total Hazard Index-RME: 0.00
 Total Cancer Risk-CT: 3.21E-14
 Total Cancer Risk-RME: 4.83E-13

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 17BCD
Exposure Scenario: Hunter Exposure to Surface Soil—Ingestion

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Arsenic	4.82E+01	0.01	0.02	4.55E-07	7.88E-06
Barium	1.61E+02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	2.82E+00	0.00	0.00	7.62E-08	1.32E-06
Cadmium	1.64E+00	0.00	0.00	0.00E+00	0.00E+00
Chromium III	1.05E+02	0.00	0.00	0.00E+00	0.00E+00
Lead	2.90E+02	0.00	0.00	0.00E+00	0.00E+00
Mercury	9.41E-02	0.00	0.00	0.00E+00	0.00E+00
Nickel	4.58E+01	0.00	0.00	0.00E+00	0.00E+00
Silver	4.88E-01	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.01
Total Hazard Index-RME: 0.03
Total Cancer Risk-CT: 5.31E-07
Total Cancer Risk-RME: 9.20E-06

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 17BCD
Exposure Scenario: Hunter Exposure to Surface Soil--Dermal

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Arsenic	4.82E+01	0.00	0.01	2.63E-07	2.86E-06
Barium	1.61E+02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	2.82E+00	0.00	0.00	3.02E-06	3.29E-05
Cadmium	1.64E+00	0.00	0.01	0.00E+00	0.00E+00
Chromium III	1.05E+02	0.00	0.00	0.00E+00	0.00E+00
Lead	2.90E+02	0.00	0.00	0.00E+00	0.00E+00
Mercury	9.41E-02	0.00	0.00	0.00E+00	0.00E+00
Nickel	4.58E+01	0.00	0.00	0.00E+00	0.00E+00
Silver	4.88E-01	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.01
 Total Hazard Index-RME: 0.02
 Total Cancer Risk-CT: 3.28E-06
 Total Cancer Risk-RME: 3.57E-05

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 17BCD
Exposure Scenario: Construction Worker Exposure to Surface Soil--Ingestion

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Arsenic	4.82E+01	0.16	0.75	5.05E-07	9.70E-06
Barium	1.61E+02	0.00	0.01	0.00E+00	0.00E+00
Beryllium	2.82E+00	0.00	0.00	8.47E-08	1.63E-06
Cadmium	1.64E+00	0.00	0.02	0.00E+00	0.00E+00
Chromium III	1.05E+02	0.00	0.00	0.00E+00	0.00E+00
Lead	2.90E+02	0.00	0.00	0.00E+00	0.00E+00
Mercury	9.41E-02	0.00	0.00	0.00E+00	0.00E+00
Nickel	4.58E+01	0.00	0.01	0.00E+00	0.00E+00
Silver	4.88E-01	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.17
 Total Hazard Index-RME: 0.80
 Total Cancer Risk-CT: 5.90E-07
 Total Cancer Risk-RME: 1.13E-05

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 17BCD
Exposure Scenario: Construction Worker Exposure to Surface Soil--Dermal

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Arsenic	4.82E+01	0.06	0.08	2.33E-07	1.21E-06
Barium	1.61E+02	0.01	0.02	0.00E+00	0.00E+00
Beryllium	2.82E+00	0.02	0.02	2.68E-06	1.39E-05
Cadmium	1.64E+00	0.05	0.07	0.00E+00	0.00E+00
Chromium III	1.05E+02	0.00	0.00	0.00E+00	0.00E+00
Lead	2.90E+02	0.00	0.00	0.00E+00	0.00E+00
Mercury	9.41E-02	0.01	0.01	0.00E+00	0.00E+00
Nickel	4.58E+01	0.02	0.02	0.00E+00	0.00E+00
Silver	4.88E-01	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.17
 Total Hazard Index-RME: 0.23
 Total Cancer Risk-CT: 2.91E-06
 Total Cancer Risk-RME: 1.51E-05

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 17BCD
Exposure Scenario: Construction Worker Exposure to Surface Soil--Inhalation of Particulates

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Arsenic	4.82E+01	0.00	0.00	1.48E-14	1.03E-13
Barium	1.61E+02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	2.82E+00	0.00	0.00	4.82E-16	3.37E-15
Cadmium	1.64E+00	0.00	0.00	2.11E-16	1.48E-15
Chromium III	1.05E+02	0.00	0.00	0.00E+00	0.00E+00
Lead	2.90E+02	0.00	0.00	0.00E+00	0.00E+00
Mercury	9.41E-02	0.00	0.00	0.00E+00	0.00E+00
Nickel	4.58E+01	0.00	0.00	0.00E+00	0.00E+00
Silver	4.88E-01	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.00
 Total Hazard Index-RME: 0.00
 Total Cancer Risk-CT: 1.55E-14
 Total Cancer Risk-RME: 1.08E-13

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 17BCD
Exposure Scenario: Construction Worker Exposure to Subsurface Soil--Ingestion

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Arsenic	8.13E+00	0.03	0.13	8.52E-08	1.64E-06
Lead	2.74E+01	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks
 Total Hazard Index-CT: 0.03
 Total Hazard Index-RME: 0.13
 Total Cancer Risk-CT: 8.52E-08
 Total Cancer Risk-RME: 1.64E-06

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 17BCD
Exposure Scenario: Construction Worker Exposure to Subsurface Soil--Dermal

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Arsenic	8.13E+00	0.01	0.01	3.93E-08	2.04E-07
Lead	2.74E+01	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.01
 Total Hazard Index-RME: 0.01
 Total Cancer Risk-CT: 3.93E-08
 Total Cancer Risk-RME: 2.04E-07

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 17BCD
Exposure Scenario: Construction Worker Exposure to Subsurface Soil--Inhalation of Particulates

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Arsenic	8.13E+00	0.00	0.00	2.49E-15	1.74E-14
Lead	2.74E+01	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.00
 Total Hazard Index-RME: 0.00
 Total Cancer Risk-CT: 2.49E-15
 Total Cancer Risk-RME: 1.74E-14

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 31
Exposure Scenario: Commercial Worker Exposure to GROUNDWATER--Ingestion

CHEMICAL	EP CONCENTRATIONS	HAZARD INDEX-CT	HAZARD INDEX-RME	CANCER RISK-CT	CANCER RISK-RME
Antimony	4.23E-02	0.26	1.03	0.00E+00	0.00E+00
Barium	4.32E-02	0.00	0.01	0.00E+00	0.00E+00
Beryllium	1.61E-03	0.00	0.00	1.21E-06	2.42E-05
Selenium	1.82E-03	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.26
Total Hazard Index-RME: 1.05
Total Cancer Risk-CT: 1.21E-06
Total Cancer Risk-RME: 2.42E-05

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 31
Exposure Scenario: Commercial Worker Exposure to GROUNDWATER--Dermal (Showering)

CHEMICAL	EP CONCENTRATIONS	HAZARD INDEX-CT	HAZARD INDEX-RME	CANCER RISK-CT	CANCER RISK-RME
Antimony	4.23E-02	0.12	0.47	0.00E+00	0.00E+00
Barium	4.32E-02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	1.61E-03	0.00	0.00	5.50E-07	1.10E-05
Selenium	1.82E-03	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.12
 Total Hazard Index-RME: 0.47
 Total Cancer Risk-CT: 5.50E-07
 Total Cancer Risk-RME: 1.10E-05

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 48
Exposure Scenario: Commercial Worker Exposure to GROUNDWATER--Ingestion

EXPOSURE ASSUMPTIONS

	chem-specific	chem-specific
Chemical concentration (mg/L)	0.5	1
Ingestion Rate (L/day)	125	250
Exposure Frequency (days/yr)	5	25
Exposure Duration (yrs.)	1	1
Conversion Factor	70	70
Body Weight (Kg)	1825	9125
Averaging Time Non-carcinogenic (days)	25550	25550
Averaging Time Carcinogenic (days)		

CHEMICAL	EP CONCENTRATIONS	HAZARD INDEX-CT	HAZARD INDEX-RME	CANCER RISK-CT	CANCER RISK-RME
1,1,1-Trichloroethane	1.00E-03	0.00	0.00	0.00E+00	0.00E+00
1,1-Dichloroethane	7.32E-04	0.00	0.00	0.00E+00	0.00E+00
1,1-Dichloroethene	6.09E-04	0.00	0.00	6.38E-08	1.28E-06
Barium	1.85E-01	0.01	0.03	0.00E+00	0.00E+00
Beryllium	1.36E-03	0.00	0.00	1.02E-06	2.04E-05
bis (2-Ethyl hexyl) phthalate	1.02E-02	0.00	0.00	2.50E-08	4.99E-07
Carbon tetrachloride	6.93E-03	0.02	0.10	1.57E-07	3.15E-06
Chloroform	2.66E-03	0.00	0.00	2.85E-09	5.70E-08
Methylene chloride	6.09E-04	0.00	0.00	7.98E-10	1.60E-08
Tetrachloroethene	6.22E-04	0.00	0.00	0.00E+00	0.00E+00
Trichloroethene	7.67E-03	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.03
 Total Hazard Index-RME: 0.13
 Total Cancer Risk-CT: 1.27E-06
 Total Cancer Risk-RME: 2.54E-05

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 48
Exposure Scenario: Commercial Worker Exposure to GROUNDWATER--Dermal (Showering)

EXPOSURE ASSUMPTIONS

Chemical concentration (mg/L)	chem-specific	chem-specific
Exposure Time (hrs/day)	0.117	0.2
Exposure Frequency (days/yr)	125	250
Skin Surface Area (cm ²)	19400	22800
Exposure Duration (yrs.)	5	25
Conversion Factor	0.001	0.001
Body Weight (Kg)	70	70
Averaging Time Non-carcinogenic (days)	1825	9125
Averaging Time Carcinogenic (days)	25550	25550

CHEMICAL	EP CONCENTRATIONS	HAZARD INDEX-CT	HAZARD INDEX-RME	CANCER RISK-CT	CANCER RISK-RME
1,1,1-Trichloroethane	1.00E-03	0.00	0.00	0.00E+00	0.00E+00
1,1-Dichloroethane	7.32E-04	0.00	0.00	0.00E+00	0.00E+00
1,1-Dichloroethene	6.09E-04	0.00	0.00	5.15E-09	1.04E-07
Barium	1.85E-01	0.00	0.00	0.00E+00	0.00E+00
Beryllium	1.36E-03	0.00	0.00	4.64E-07	9.32E-06
bis (2-Ethyl hexyl) Phthalate	1.02E-02	0.00	0.00	0.00E+00	0.00E+00
Carbon tetrachloride	6.93E-03	0.00	0.00	8.40E-10	1.69E-08
Chloroform	2.66E-03	0.00	0.00	1.15E-10	2.31E-09
Methylene chloride	6.09E-04	0.00	0.00	1.66E-11	3.34E-10
Tetrachloroethene	6.22E-04	0.00	0.00	0.00E+00	0.00E+00
Trichloroethene	7.67E-03	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.00
 Total Hazard Index-RME: 0.00
 Total Cancer Risk-CT: 4.70E-07
 Total Cancer Risk-RME: 9.44E-06

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 48
Exposure Scenario: Commercial Worker Exposure to GROUNDWATER--Inhalation of Volatiles (Showerin

EXPOSURE ASSUMPTIONS

Chemical concentration (mg/L)	chem-specific	chem-specific
Exposure Time (hrs/day)	0.117	0.2
Exposure Frequency (days/yr)	125	250
Inhalation Rate (m ³ /hour)	1.4	2
Exposure Duration (yrs.)	5	25
Conversion Factor	1	1
Body Weight (Kg)	70	70
Averaging Time Non-carcinogenic (days)	1825	9125
Averaging Time Carcinogenic (days)	25550	25550

CHEMICAL	EP CONCENTRATIONS	HAZARD INDEX-CT	HAZARD INDEX-RME	CANCER RISK-CT	CANCER RISK-RME
1,1,1-Trichloroethane	1.00E-03	0.00	0.00	0.00E+00	0.00E+00
1,1-Dichloroethane	7.32E-04	0.00	0.00	0.00E+00	0.00E+00
1,1-Dichloroethene	6.09E-04	0.00	0.00	1.78E-08	4.35E-07
Barium	1.85E-01	0.00	0.00	0.00E+00	0.00E+00
Beryllium	1.36E-03	0.00	0.00	0.00E+00	0.00E+00
bis (2-Ethyl hexyl) Phthalate	1.02E-02	0.00	0.00	0.00E+00	0.00E+00
Carbon tetrachloride	6.93E-03	0.00	0.00	6.07E-08	1.48E-06
Chloroform	2.66E-03	0.00	0.00	7.56E-09	1.85E-07
Methylene chloride	6.09E-04	0.00	0.00	2.97E-11	7.25E-10
Tetrachloroethene	6.22E-04	0.00	0.00	0.00E+00	0.00E+00
Trichloroethene	7.67E-03	0.69	3.38	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.69
 Total Hazard Index-RME: 3.38
 Total Cancer Risk-CT: 8.61E-08
 Total Cancer Risk-RME: 2.10E-06

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 48
Exposure Scenario: Commercial Worker Exposure to Surface Soil--Ingestion

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Arsenic	9.78E+00	0.01	0.03	2.56E-07	5.13E-06
Barium	7.58E+02	0.00	0.01	0.00E+00	0.00E+00
Beryllium	2.15E+00	0.00	0.00	1.61E-07	3.22E-06
bis (2-Ethyl hexyl) phthalate	1.99E+00	0.00	0.00	4.86E-10	9.72E-09
Chromium III	5.87E+01	0.00	0.00	0.00E+00	0.00E+00
Chrysene	2.82E-01	0.00	0.00	3.60E-11	7.20E-10
Di-n-butyl phthalate	1.23E+01	0.00	0.00	0.00E+00	0.00E+00
Lead	1.96E+02	0.00	0.00	0.00E+00	0.00E+00
Mercury	1.47E+00	0.00	0.00	0.00E+00	0.00E+00
Nickel	3.12E+01	0.00	0.00	0.00E+00	0.00E+00
Phenanthrene	1.00E+00	0.00	0.00	0.00E+00	0.00E+00
Selenium	1.00E+00	0.00	0.00	0.00E+00	0.00E+00
Silver	6.45E-02	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.01
 Total Hazard Index-RME: 0.05
 Total Cancer Risk-CT: 4.18E-07
 Total Cancer Risk-RME: 8.36E-06

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 48
Exposure Scenario: Commercial Worker Exposure to Surface Soil—Dermal

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Arsenic	9.78E+00	0.01	0.02	2.36E-07	3.06E-06
Barium	7.58E+02	0.03	0.09	0.00E+00	0.00E+00
Beryllium	2.15E+00	0.01	0.02	1.02E-05	1.32E-04
bis (2-Ethyl hexyl) phthalate	1.99E+00	0.00	0.00	0.00E+00	0.00E+00
Chromium III	5.87E+01	0.00	0.00	0.00E+00	0.00E+00
Chrysene	2.82E-01	0.00	0.00	3.79E-10	4.92E-09
Di-n-butyl phthalate	1.23E+01	0.00	0.00	0.00E+00	0.00E+00
Lead	1.96E+02	0.00	0.00	0.00E+00	0.00E+00
Mercury	1.47E+00	0.08	0.20	0.00E+00	0.00E+00
Nickel	3.12E+01	0.01	0.02	0.00E+00	0.00E+00
Phenanthrene	1.00E+00	0.00	0.00	0.00E+00	0.00E+00
Selenium	1.00E+00	0.00	0.00	0.00E+00	0.00E+00
Silver	6.45E-02	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.13
 Total Hazard Index-RME: 0.33
 Total Cancer Risk-CT: 1.04E-05
 Total Cancer Risk-RME: 1.35E-04

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 48
Exposure Scenario: Commercial Worker Exposure to Surface Soil--Inhalation of Volatiles

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
bis (2-Ethyl hexyl) phthalate	1.99E+00	0.00	0.00	0.00E+00	0.00E+00
Chrysene	2.82E-01	0.00	0.00	5.32E-17	8.01E-16
Di-n-butyl phthalate	1.23E+01	0.00	0.00	0.00E+00	0.00E+00
Phenanthrene	1.00E+00	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.00
 Total Hazard Index-RME: 0.00
 Total Cancer Risk-CT: 5.32E-17
 Total Cancer Risk-RME: 8.01E-16

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 48
Exposure Scenario: Commercial Worker Exposure to Surface Soil--Inhalation of Particulates

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Arsenic	9.78E+00	0.00	0.00	6.22E-15	9.36E-14
Barium	7.58E+02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	2.15E+00	0.00	0.00	7.61E-16	1.15E-14
Chromium III	5.87E+01	0.00	0.00	0.00E+00	0.00E+00
Lead	1.96E+02	0.00	0.00	0.00E+00	0.00E+00
Mercury	1.47E+00	0.00	0.00	0.00E+00	0.00E+00
Nickel	3.12E+01	0.00	0.00	0.00E+00	0.00E+00
Selenium	1.00E+00	0.00	0.00	0.00E+00	0.00E+00
Silver	6.45E-02	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.00
Total Hazard Index-RME: 0.00
Total Cancer Risk-CT: 6.98E-15
Total Cancer Risk-RME: 1.05E-13

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 48
Exposure Scenario: Hunter Exposure to Surface Soil--Ingestion

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Arsenic	9.78E+00	0.00	0.00	9.23E-08	1.60E-06
Barium	7.58E+02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	2.15E+00	0.00	0.00	5.80E-08	1.01E-06
bis (2-Ethyl hexyl) phthalate	1.99E+00	0.00	0.00	1.75E-10	3.03E-09
Chromium III	5.87E+01	0.00	0.00	0.00E+00	0.00E+00
Chrysene	2.82E-01	0.00	0.00	1.30E-11	2.25E-10
Di-n-butyl phthalate	1.23E+01	0.00	0.00	0.00E+00	0.00E+00
Lead	1.96E+02	0.00	0.00	0.00E+00	0.00E+00
Mercury	1.47E+00	0.00	0.00	0.00E+00	0.00E+00
Nickel	3.12E+01	0.00	0.00	0.00E+00	0.00E+00
Phenanthrene	1.00E+00	0.00	0.00	0.00E+00	0.00E+00
Selenium	1.00E+00	0.00	0.00	0.00E+00	0.00E+00
Silver	6.45E-02	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.00
Total Hazard Index-RME: 0.01
Total Cancer Risk-CT: 1.50E-07
Total Cancer Risk-RME: 2.61E-06

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 48
Exposure Scenario: Hunter Exposure to Surface Soil--Dermal

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Arsenic	9.78E+00	0.00	0.00	5.33E-08	5.81E-07
Barium	7.58E+02	0.00	0.01	0.00E+00	0.00E+00
Beryllium	2.15E+00	0.00	0.00	2.30E-06	2.50E-05
bis (2-Ethyl hexyl) phthalate	1.99E+00	0.00	0.00	0.00E+00	0.00E+00
Chromium III	5.87E+01	0.00	0.00	0.00E+00	0.00E+00
Chrysene	2.82E-01	0.00	0.00	8.55E-11	9.32E-10
Di-n-butyl phthalate	1.23E+01	0.00	0.00	0.00E+00	0.00E+00
Lead	1.96E+02	0.00	0.00	0.00E+00	0.00E+00
Mercury	1.47E+00	0.01	0.02	0.00E+00	0.00E+00
Nickel	3.12E+01	0.00	0.00	0.00E+00	0.00E+00
Phenanthrene	1.00E+00	0.00	0.00	0.00E+00	0.00E+00
Selenium	1.00E+00	0.00	0.00	0.00E+00	0.00E+00
Silver	6.45E-02	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks
 Total Hazard Index-CT: 0.02
 Total Hazard Index-RME: 0.03
 Total Cancer Risk-CT: 2.35E-06
 Total Cancer Risk-RME: 2.56E-05

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 48
Exposure Scenario: Construction Worker Exposure to Surface Soil--Ingestion

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Arsenic	9.78E+00	0.03	0.15	1.03E-07	1.97E-06
Barium	7.58E+02	0.01	0.05	0.00E+00	0.00E+00
Beryllium	2.15E+00	0.00	0.00	6.45E-08	1.24E-06
bis (2-Ethyl hexyl) phthalate	1.99E+00	0.00	0.00	1.94E-10	3.73E-09
Chromium III	5.87E+01	0.00	0.00	0.00E+00	0.00E+00
Chrysene	2.82E-01	0.00	0.00	1.44E-11	2.76E-10
Di-n-butyl phthalate	1.23E+01	0.00	0.00	0.00E+00	0.00E+00
Lead	1.96E+02	0.00	0.00	0.00E+00	0.00E+00
Mercury	1.47E+00	0.00	0.02	0.00E+00	0.00E+00
Nickel	3.12E+01	0.00	0.01	0.00E+00	0.00E+00
Phenanthrene	1.00E+00	0.00	0.00	0.00E+00	0.00E+00
Selenium	1.00E+00	0.00	0.00	0.00E+00	0.00E+00
Silver	6.45E-02	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.05
 Total Hazard Index-RME: 0.24
 Total Cancer Risk-CT: 1.67E-07
 Total Cancer Risk-RME: 3.21E-06

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 48
Exposure Scenario: Construction Worker Exposure to Surface Soil--Dermal

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Arsenic	9.78E+00	0.01	0.02	4.72E-08	2.45E-07
Barium	7.58E+02	0.07	0.09	0.00E+00	0.00E+00
Beryllium	2.15E+00	0.01	0.02	2.04E-06	1.06E-05
bis (2-Ethyl hexyl) phthalate	1.99E+00	0.00	0.00	0.00E+00	0.00E+00
Chromium III	5.87E+01	0.00	0.00	0.00E+00	0.00E+00
Chrysene	2.82E-01	0.00	0.00	7.58E-11	3.93E-10
Di-n-butyl phthalate	1.23E+01	0.00	0.00	0.00E+00	0.00E+00
Lead	1.96E+02	0.00	0.00	0.00E+00	0.00E+00
Mercury	1.47E+00	0.15	0.20	0.00E+00	0.00E+00
Nickel	3.12E+01	0.01	0.02	0.00E+00	0.00E+00
Phenanthrene	1.00E+00	0.00	0.00	0.00E+00	0.00E+00
Selenium	1.00E+00	0.00	0.00	0.00E+00	0.00E+00
Silver	6.45E-02	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.26
 Total Hazard Index-RME: 0.33
 Total Cancer Risk-CT: 2.09E-06
 Total Cancer Risk-RME: 1.08E-05

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 48
Exposure Scenario: Construction Worker Exposure to Surface Soil--Inhalation of Volatiles

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
bis (2-Ethyl hexyl) phthalate	1.99E+00	0.00	0.00	0.00E+00	0.00E+00
Chrysene	2.82E-01	0.00	0.00	2.56E-17	1.79E-16
Di-n-butyl phthalate	1.23E+01	0.00	0.00	0.00E+00	0.00E+00
Phenanthrene	1.00E+00	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.00
Total Hazard Index-RME: 0.00
Total Cancer Risk-CT: 2.56E-17
Total Cancer Risk-RME: 1.79E-16

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 48
Exposure Scenario: Construction Worker Exposure to Surface Soil--Inhalation of Particulates

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Arsenic	9.78E+00	0.00	0.00	3.00E-15	2.10E-14
Barium	7.58E+02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	2.15E+00	0.00	0.00	3.67E-16	2.57E-15
Chromium III	5.87E+01	0.00	0.00	0.00E+00	0.00E+00
Lead	1.96E+02	0.00	0.00	0.00E+00	0.00E+00
Mercury	1.47E+00	0.00	0.00	0.00E+00	0.00E+00
Nickel	3.12E+01	0.00	0.00	0.00E+00	0.00E+00
Selenium	1.00E+00	0.00	0.00	0.00E+00	0.00E+00
Silver	6.45E-02	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks
Total Hazard Index-CT: 0.00
Total Hazard Index-RME: 0.00
Total Cancer Risk-CT: 3.36E-15
Total Cancer Risk-RME: 2.35E-14

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 54
Exposure Scenario: Commercial Worker Exposure to GROUNDWATER--Ingestion

CHEMICAL	EP CONCENTRATIONS	HAZARD INDEX-CT	HAZARD INDEX-RME	CANCER RISK-CT	CANCER RISK-RME
Antimony	4.44E-02	0.27	1.09	0.00E+00	0.00E+00
Arsenic	2.75E-03	0.02	0.09	7.21E-07	1.44E-05
Barium	1.70E-01	0.01	0.02	0.00E+00	0.00E+00
Beryllium	4.79E-03	0.00	0.01	3.60E-06	7.20E-05
Chromium III	1.23E-02	0.00	0.00	0.00E+00	0.00E+00
HMX	1.58E-03	0.00	0.00	0.00E+00	0.00E+00
Lead	3.16E-03	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.30
 Total Hazard Index-RME: 1.21
 Total Cancer Risk-CT: 4.32E-06
 Total Cancer Risk-RME: 8.65E-05

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 54
Exposure Scenario: Commercial Worker Exposure to GROUNDWATER--Dermal (Showering)

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Antimony	4.44E-02	0.12	0.50	0.00E+00	0.00E+00
Arsenic	2.75E-03	0.00	0.00	4.78E-09	9.59E-08
Barium	1.70E-01	0.00	0.00	0.00E+00	0.00E+00
Beryllium	4.79E-03	0.00	0.00	1.64E-06	3.28E-05
Chromium III	1.23E-02	0.00	0.00	0.00E+00	0.00E+00
HMX	1.58E-03	0.00	0.00	0.00E+00	0.00E+00
Lead	3.16E-03	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.13
Total Hazard Index-RME: 0.50
Total Cancer Risk-CT: 1.64E-06
Total Cancer Risk-RME: 3.29E-05

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 54
Exposure Scenario: Construction Worker Exposure to Subsurface Soil--Ingestion

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
2,4,6-Trinitrotoluene	3.87E+02	0.76	3.64	8.12E-08	1.56E-06
2,4-Dinitrotoluene	5.14E+00	0.00	0.01	0.00E+00	0.00E+00
HMX	1.65E+00	0.00	0.00	0.00E+00	0.00E+00
Lead	2.21E+03	0.00	0.00	0.00E+00	0.00E+00
Mercury	1.72E+01	0.06	0.27	0.00E+00	0.00E+00
RDX	9.43E-01	0.00	0.00	7.25E-10	1.39E-08

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.82
 Total Hazard Index-RME: 3.92
 Total Cancer Risk-CT: 8.20E-08
 Total Cancer Risk-RME: 1.57E-06

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 54
Exposure Scenario: Construction Worker Exposure to Subsurface Soil--Dermal

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
2,4,6-Trinitrotoluene	3.87E+02	1.20	1.55	1.28E-07	6.66E-07
2,4-Dinitrotoluene	5.14E+00	0.00	0.01	0.00E+00	0.00E+00
HMX	1.65E+00	0.00	0.00	0.00E+00	0.00E+00
Lead	2.21E+03	0.00	0.00	0.00E+00	0.00E+00
Mercury	1.72E+01	1.77	2.29	0.00E+00	0.00E+00
RDX	9.43E-01	0.00	0.00	1.15E-09	5.94E-09

Total Pathway Exposure Risks

Total Hazard Index-CT: 2.97
Total Hazard Index-RME: 3.85
Total Cancer Risk-CT: 1.29E-07
Total Cancer Risk-RME: 6.72E-07

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 54
Exposure Scenario: Construction Worker Exposure to Subsurface Soil--Inhalation of Particulates

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
2,4,6-Trinitrotoluene	3.87E+02	0.00	0.00	0.00E+00	0.00E+00
HMX	1.65E+00	0.00	0.00	0.00E+00	0.00E+00
Lead	2.21E+03	0.00	0.00	0.00E+00	0.00E+00
Mercury	1.72E+01	0.00	0.00	0.00E+00	0.00E+00
RDX	9.43E-01	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.00
Total Hazard Index-RME: 0.00
Total Cancer Risk-CT: 0.00E+00
Total Cancer Risk-RME: 0.00E+00

Facility Radford Army Ammunition Plant, VA
Site Name: SWMU 54
Exposure Scenario: Construction Worker Exposure to Subsurface Soil--Inhalation of Volatiles

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
2,4-Dinitrotoluene	5.14E+00	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.00
 Total Hazard Index-RME: 0.00
 Total Cancer Risk-CT: 0.00E+00
 Total Cancer Risk-RME: 0.00E+00

Facility Radford Army Ammunition Plant, VA
Site Name: STROUBLES CREEK
Exposure Scenario: Commercial Worker Exposure to SURFACE WATER--Ingestion

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Barium	4.60E-02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	2.08E-03	0.00	0.00	3.13E-08	3.13E-07
Chromium III	1.61E-02	0.00	0.00	0.00E+00	0.00E+00
HMX	5.30E-03	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.00
 Total Hazard Index-RME: 0.00
 Total Cancer Risk-CT: 3.13E-08
 Total Cancer Risk-RME: 3.13E-07

Facility Radford Army Ammunition Plant, VA
Site Name: STROUBLES CREEK
Exposure Scenario: Commercial Worker Exposure to SURFACE WATER--Dermal

CHEMICAL	EP CONCENTRATIONS	HAZARD INDEX-CT	HAZARD INDEX-RME	CANCER RISK-CT	CANCER RISK-RME
Barium	4.60E-02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	2.08E-03	0.00	0.00	7.88E-09	1.06E-07
Chromium III	1.61E-02	0.00	0.00	0.00E+00	0.00E+00
HMX	5.30E-03	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.00
Total Hazard Index-RME: 0.00
Total Cancer Risk-CT: 7.88E-09
Total Cancer Risk-RME: 1.06E-07

Facility Radford Army Ammunition Plant, VA
Site Name: STROUBLES CREEK
Exposure Scenario: Commercial Worker Exposure to SEDIMENT--Ingestion

CHEMICAL	EP CONCENTRATIONS	HAZARD INDEX-CT	HAZARD INDEX-RME	CANCER RISK-CT	CANCER RISK-RME
Arsenic	9.78E+00	0.00	0.01	5.13E-08	1.03E-06
Barium	1.84E+02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	1.41E+00	0.00	0.00	2.12E-08	4.25E-07
Chromium III	3.31E+01	0.00	0.00	0.00E+00	0.00E+00
Chrysene	6.60E-02	0.00	0.00	1.68E-12	3.37E-11
Di-n-butyl phthalate	2.50E+00	0.00	0.00	0.00E+00	0.00E+00
Fluoranthene	7.23E-02	0.00	0.00	0.00E+00	0.00E+00
Lead	3.59E+01	0.00	0.00	0.00E+00	0.00E+00
Nickel	2.97E+01	0.00	0.00	0.00E+00	0.00E+00
Phenanthrene	7.62E-02	0.00	0.00	0.00E+00	0.00E+00
Silver	7.47E-02	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.00
 Total Hazard Index-RME: 0.01
 Total Cancer Risk-CT: 7.25E-08
 Total Cancer Risk-RME: 1.45E-06

Facility Radford Army Ammunition Plant, VA
Site Name: STROUBLES CREEK
Exposure Scenario: Commercial Worker Exposure to SEDIMENT--Dermal

CHEMICAL	EP CONCENTRATIONS	HAZARD INDEX-CT	HAZARD INDEX-RME	CANCER RISK-CT	CANCER RISK-RME
Arsenic	9.78E+00	0.00	0.00	1.26E-08	1.69E-07
Barium	1.84E+02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	1.41E+00	0.00	0.00	3.57E-07	4.80E-06
Chromium III	3.31E+01	0.00	0.00	0.00E+00	0.00E+00
Chrysene	6.60E-02	0.00	0.00	4.71E-12	6.34E-11
Di-n-butyl phthalate	2.50E+00	0.00	0.00	0.00E+00	0.00E+00
Fluoranthene	7.23E-02	0.00	0.00	0.00E+00	0.00E+00
Lead	3.59E+01	0.00	0.00	0.00E+00	0.00E+00
Nickel	2.97E+01	0.00	0.00	0.00E+00	0.00E+00
Phenanthrene	7.62E-02	0.00	0.00	0.00E+00	0.00E+00
Silver	7.47E-02	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.00
Total Hazard Index-RME: 0.00
Total Cancer Risk-CT: 3.69E-07
Total Cancer Risk-RME: 4.97E-06

Facility Radford Army Ammunition Plant, VA
Site Name: STROUBLES CREEK
Exposure Scenario: Fisherman Exposure to SURFACE WATER--Dermal

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Barium	4.60E-02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	2.08E-03	0.00	0.01	4.55E-07	1.18E-04
Chromium III	1.61E-02	0.00	0.00	0.00E+00	0.00E+00
HMX	5.30E-03	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.00
Total Hazard Index-RME: 0.02
Total Cancer Risk-CT: 4.55E-07
Total Cancer Risk-RME: 1.18E-04

Facility Radford Army Ammunition Plant, VA
Site Name: STROUBLES CREEK
Exposure Scenario: Fisherman Exposure to SURFACE WATER--Ingestion

CHEMICAL	EP CONCENTRATIONS	HAZARD INDEX-CT	HAZARD INDEX-RME	CANCER RISK-CT	CANCER RISK-RME
Barium	4.60E-02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	2.08E-03	0.00	0.00	7.20E-10	1.80E-08
Chromium III	1.61E-02	0.00	0.00	0.00E+00	0.00E+00
HMX	5.30E-03	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.00
Total Hazard Index-RME: 0.00
Total Cancer Risk-CT: 7.20E-10
Total Cancer Risk-RME: 1.80E-08

Facility Radford Army Ammunition Plant, VA
Site Name: STROUBLES CREEK
Exposure Scenario: Recreational User Exposure to SURFACE WATER--Dermal

CHEMICAL	EP CONCENTRATIONS	HAZARD INDEX-CT	HAZARD INDEX-RME	CANCER RISK-CT	CANCER RISK-RME
Barium	4.60E-02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	2.08E-03	0.00	0.00	3.41E-09	2.63E-07
Chromium III	1.61E-02	0.00	0.00	0.00E+00	0.00E+00
HMX	5.30E-03	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.00
Total Hazard Index-RME: 0.00
Total Cancer Risk-CT: 3.41E-09
Total Cancer Risk-RME: 2.63E-07

Facility Radford Army Ammunition Plant, VA
Site Name: STROUBLES CREEK
Exposure Scenario: Recreational User Exposure to SURFACE WATER--Ingestion

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Barium	4.60E-02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	2.08E-03	0.00	0.00	6.75E-09	5.25E-08
Chromium III	1.61E-02	0.00	0.00	0.00E+00	0.00E+00
HMX	5.30E-03	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.00
Total Hazard Index-RME: 0.00
Total Cancer Risk-CT: 6.75E-09
Total Cancer Risk-RME: 5.25E-08

Facility Radford Army Ammunition Plant, VA
Site Name: STROUBLES CREEK
Exposure Scenario: Construction Worker Exposure to SURFACE WATER--Dermal

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Barium	4.60E-02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	2.08E-03	0.00	0.00	1.48E-08	1.54E-07
Chromium III	1.61E-02	0.00	0.00	0.00E+00	0.00E+00
HMX	5.30E-03	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.00
Total Hazard Index-RME: 0.00
Total Cancer Risk-CT: 1.48E-08
Total Cancer Risk-RME: 1.54E-07

Facility Radford Army Ammunition Plant, VA
Site Name: STROUBLES CREEK
Exposure Scenario: Construction Worker Exposure to SURFACE WATER--Ingestion

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Barium	4.60E-02	0.00	0.01	0.00E+00	0.00E+00
Beryllium	2.08E-03	0.00	0.00	3.13E-07	2.50E-06
Chromium III	1.61E-02	0.00	0.00	0.00E+00	0.00E+00
HMX	5.30E-03	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.01
Total Hazard Index-RME: 0.01
Total Cancer Risk-CT: 3.13E-07
Total Cancer Risk-RME: 2.50E-06

Facility Radford Army Ammunition Plant, VA
Site Name: NEW RIVER
Exposure Scenario: Commercial Worker Exposure to SURFACE WATER--Ingestion

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Barium	2.46E-02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	7.33E-04	0.00	0.00	1.10E-08	1.10E-07
Lead	5.93E-03	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.00
Total Hazard Index-RME: 0.00
Total Cancer Risk-CT: 1.10E-08
Total Cancer Risk-RME: 1.10E-07

Facility Radford Army Ammunition Plant, VA
Site Name: NEW RIVER
Exposure Scenario: Commercial Worker Exposure to SURFACE WATER--Dermal

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Barium	2.46E-02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	7.33E-04	0.00	0.00	2.77E-09	3.73E-08
Lead	5.93E-03	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.00
Total Hazard Index-RME: 0.00
Total Cancer Risk-CT: 2.77E-09
Total Cancer Risk-RME: 3.73E-08

Facility Radford Army Ammunition Plant, VA
Site Name: NEW RIVER
Exposure Scenario: Commercial Worker Exposure to SEDIMENT--Ingestion

CHEMICAL	EP CONCENTRATIONS	HAZARD INDEX-CT	HAZARD INDEX-RME	CANCER RISK-CT	CANCER RISK-RME
2,4,6-Trinitrotoluene	2.86E+01	0.00	0.01	2.99E-09	5.99E-08
Arsenic	1.74E+01	0.00	0.01	9.12E-08	1.82E-06
Barium	7.01E+02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	4.23E+00	0.00	0.00	6.36E-08	1.27E-06
bis (2-Ethyl hexyl) Phthalate	6.62E+00	0.00	0.00	3.24E-10	6.48E-09
Di-n-butyl phthalate	1.30E+01	0.00	0.00	0.00E+00	0.00E+00
Diethyl phthalate	6.23E+00	0.00	0.00	0.00E+00	0.00E+00
Dimethyl phthalate	8.31E+00	0.00	0.00	0.00E+00	0.00E+00
Lead	3.40E+03	0.00	0.00	0.00E+00	0.00E+00
Mercury	9.36E-02	0.00	0.00	0.00E+00	0.00E+00
n-Diphenylnitrosamine	2.60E+00	0.00	0.00	4.45E-11	8.90E-10
Silver	1.78E-01	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.01
 Total Hazard Index-RME: 0.02
 Total Cancer Risk-CT: 1.58E-07
 Total Cancer Risk-RME: 3.16E-06

Facility Radford Army Ammunition Plant, VA
Site Name: NEW RIVER
Exposure Scenario: Commercial Worker Exposure to SEDIMENT--Dermal

CHEMICAL	EP CONCENTRATIONS	HAZARD INDEX-CT	HAZARD INDEX-RME	CANCER RISK-CT	CANCER RISK-RME
2,4,6-Trinitrotoluene	2.86E+01	0.00	0.01	2.52E-09	3.38E-08
Arsenic	1.74E+01	0.00	0.00	2.23E-08	3.01E-07
Barium	7.01E+02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	4.23E+00	0.00	0.00	1.07E-06	1.44E-05
bis (2-Ethyl hexyl) Phthalate	6.62E+00	0.00	0.00	2.72E-09	3.66E-08
Di-n-butyl phthalate	1.30E+01	0.00	0.00	0.00E+00	0.00E+00
Diethyl phthalate	6.23E+00	0.00	0.00	0.00E+00	0.00E+00
Dimethyl phthalate	8.31E+00	0.00	0.00	0.00E+00	0.00E+00
Lead	3.40E+03	0.00	0.00	0.00E+00	0.00E+00
Mercury	9.36E-02	0.00	0.00	0.00E+00	0.00E+00
n-Diphenylnitrosamine	2.60E+00	0.00	0.00	0.00E+00	0.00E+00
Silver	1.78E-01	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.01
Total Hazard Index-RME: 0.02
Total Cancer Risk-CT: 1.10E-06
Total Cancer Risk-RME: 1.47E-05

Facility Radford Army Ammunition Plant, VA
Site Name: NEW RIVER
Exposure Scenario: Fisherman Exposure to SURFACE WATER--Ingestion

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Barium	2.46E-02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	7.33E-04	0.00	0.00	2.54E-10	5.07E-08
Lead	5.93E-03	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.00

Total Hazard Index-RME: 0.00

Total Cancer Risk-CT: 2.54E-10

Total Cancer Risk-RME: 5.07E-08

Facility Radford Army Ammunition Plant, VA
Site Name: NEW RIVER
Exposure Scenario: Fisherman Exposure to SURFACE WATER--Dermal

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Barium	2.46E-02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	7.33E-04	0.00	0.00	1.60E-07	4.16E-05
Lead	5.93E-03	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.00
Total Hazard Index-RME: 0.01
Total Cancer Risk-CT: 1.60E-07
Total Cancer Risk-RME: 4.16E-05

Facility Radford Army Ammunition Plant, VA
Site Name: NEW RIVER
Exposure Scenario: Construction Worker Exposure to SURFACE WATER--Ingestion

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Barium	2.46E-02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	7.33E-04	0.00	0.00	5.50E-09	4.40E-08
Lead	5.93E-03	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.00
Total Hazard Index-RME: 0.00
Total Cancer Risk-CT: 5.50E-09
Total Cancer Risk-RME: 4.40E-08

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Facility Radford Army Ammunition Plant, VA
Site Name: NEW RIVER
Exposure Scenario: Construction Worker Exposure to SURFACE WATER--Dermal

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Barium	2.46E-02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	7.33E-04	0.00	0.00	1.04E-08	5.42E-08
Lead	5.93E-03	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks
Total Hazard Index-CT: 0.00
Total Hazard Index-RME: 0.00
Total Cancer Risk-CT: 1.04E-08
Total Cancer Risk-RME: 5.42E-08

Facility Radford Army Ammunition Plant, VA
Site Name: NEW RIVER
Exposure Scenario: Recreational User Exposure to SURFACE WATER--Ingestion

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Barium	2.46E-02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	7.33E-04	0.00	0.00	3.09E-11	2.03E-09
Lead	5.93E-03	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.00
 Total Hazard Index-RME: 0.00
 Total Cancer Risk-CT: 3.09E-11
 Total Cancer Risk-RME: 2.03E-09

Facility Radford Army Ammunition Plant, VA
Site Name: NEW RIVER
Exposure Scenario: Recreational User Exposure to SURFACE WATER--Dermal

<u>CHEMICAL</u>	<u>EP CONCENTRATIONS</u>	<u>HAZARD INDEX-CT</u>	<u>HAZARD INDEX-RME</u>	<u>CANCER RISK-CT</u>	<u>CANCER RISK-RME</u>
Barium	2.46E-02	0.00	0.00	0.00E+00	0.00E+00
Beryllium	7.33E-04	0.00	0.00	1.20E-09	9.28E-08
Lead	5.93E-03	0.00	0.00	0.00E+00	0.00E+00

Total Pathway Exposure Risks

Total Hazard Index-CT: 0.00
Total Hazard Index-RME: 0.00
Total Cancer Risk-CT: 1.20E-09
Total Cancer Risk-RME: 9.28E-08